### **BARUN CORP**

May 30, 2025

RE: CERTIFICATION LETTER

Project Address: SEAN JULIUS

4204 SE 91ST AVE. PORTLAND, OR 97266

#### **Design Criteria:**

- Applicable Codes = 2023 ORSC, 2021 IEBC/IBC, 2021 IRC, ASCE 7-16 and 2018 NDS
- Risk Category = II
- Wind Speed = 98 mph, Exposure Category B, Partially/Fully Enclosed Method
- Ground Snow Load = 25 psf
- Roof 1 & Roof 2: 2 x 6 @ 24" OC, Roof DL = 7 psf, Roof LL/SL = 25 psf (Non-PV), Roof LL/SL = 25 psf (PV)

To Whom It May Concern,

A structural evaluation of loading was conducted for the above address based on the design criteria listed above.

Existing roof structural framing has been reviewed for additional loading due to installation of Solar PV System on the roof. The structural review applies to the sections of roof that is directly supporting the Solar PV System.

Based on this evaluation, I certify that the alteration to the existing structure by installation of the Solar PV System meets the prescriptive compliance requirements of the applicable existing building and/or new building provisions adopted/referenced above.

Additionally, the Solar PV System assembly (including attachment hardware) has been reviewed to be in accordance with the manufacturer's specifications and to meet and/or exceed the requirements set forth by the referenced codes.

Sincerely,



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#### **RESULTS SUMMARY**

SEAN JULIUS, 4204 SE 91ST AVE., PORTLAND, OR 97266

MOUNTING PLANE STRUCTURAL EVALUATION							
MOUNTING PLANE ROOF PITCH RESULT GOVERNING ANALYSIS							
Roof 1 & Roof 2	34°	OK	MEMBER ANALYSIS				

STANDOFF HARDWARE EVALUATION FOR WIND UPLIFT					
MOUNTING PLANE WIND UPLIFT DCR					
Roof 1 & Roof 2	37.2%				

#### Limits of Scope of Work and Liability:

The existing structure has been reviewed based on the assumption that it has been originally designed and constructed per appropriate codes. The structural analysis of the subject property is based on the provided site survey data. The calculations produced for this structure's assessment are only for the roof framing supporting the proposed PV installation referenced in the stamped planset and were made according to generally recognized structural analysis standards and procedures. All PV modules, racking and attachment components shall be designed and installed per manufacturer's approved guidelines and specifications. These plans are not stamped for water leakage or existing damage to the structural component that was not accessed during the site survey. Prior to commencement of work, the PV system installer should verify that the existing roof and connections are in suitable condition and inspect framing noted on the certification letter and inform the Engineer of Record of any discrepancies prior to installation. The installer should also check for any damages such as water damage, cracked framing, etc. and inform the Engineer of Record of existing deficiencies which are unknown and/or were not observable during the time of survey and have not been included in this scope of work. Any change in the scope of the work shall not be accepted unless such change, addition, or deletion is approved in advance and in writing by the Engineer of Record. The Engineer of Record and Barun Corp claim no responsibility for misuse and improper installation.

# BARUN CORP LOAD CALCULATION Roof 1 & Roof 2 SEAN JULIUS, 4204 SE 91ST AVE., PORTLAND, OR 97266

PV PANELS DEAD LOAD (PV-DL)			
PV Panels Weight = 2.50 psf			
Hardware Assembly Weight	= 0.50 psf		
Total PV Panels Weight	PV-DL = 3.00 psf		

ROOF DEAD LOAD (R-DL)						
Existing Roofing Material Weight	= 2.50 psf					
Underlayment Weight			= 0.50 psf			
Plywood/OSB Sheathing Weight	= 1.50 psf					
Framing Weight	= 1.15 psf					
No Vaulted Ceiling			= 0.00 psf			
Miscellaneous	= 1.50 psf					
Total Roof Dead Load	R-DL = 7.10 psf					

REDUCED ROOF LIVE LOAD (Lr)				
Roof Live Load	Lo = 20.00 psf			
Member Tributary Area	$At < 200 \text{ ft}^2$			
Roof 1 & Roof 2 Pitch	34° or 8/12			
Tributary Area Reduction Factor	R1 = 1.00			
Roof Slope Reduction Factor	R2 = 0.80			
Reduced Roof Live Load, Lr = Lo (R1) (R2)	Lr = 16.00 psf			

SNOW LOAD				
Ground Snow Load	pg = 25.00 psf			
Effective Roof Slope	34°			
Snow Importance Factor	Is = 1.00			
Snow Exposure Factor	Ce = 1.00			
Snow Thermal Factor	Ct = 1.10			
Minimum Flat Roof Snow Load	pf-min = 25.00 psf			
Flat Roof Snow Load	pf = 25.00 psf			

SLOPED ROOF SNOW LOAD ON ROOF (Non-Slippery Surfaces)				
oof Slope Factor Cs-roof = 1.00				
Sloped Roof Snow Load on Roof	ps-roof = 25.00 psf			

SLOPED ROOF SNOW LOAD ON PV PANELS (Unobstructed Slippery Surfaces)			
Roof Slope Factor Cs-PV = 1.00			
Sloped Roof Snow Load on PV Panels	ps-PV = 25.00 psf		

#### Lateral Capacity check for Ecofasten Rockit Smart slide attachments.

Attachment type = Ecofasten RockIT Smart Slide Number of rows in Array = 4
Attachment Max. X-spacing = 4.00 ft Array Lateral Capacity factor = 1.25

Attachment Max. Y-spacing = 3.72 ft
Lateral load on each attachment = 232.98 lbs

Lateral capacity of the attachment = 251.25 lbs (Based on hardware manufacturer)

Pass. Provided spacing is Okay.

## BARUN CORP

#### WIND UPLIFT CALCULATION

#### Roof 1 & Roof 2

SEAN JULIUS, 4204 SE 91ST AVE., PORTLAND, OR 97266

SITE INFORMATION					
Ultimate Wind Speed =	98.00 mph	Roof Pitch =	34°		
Risk Category =	II	Roof Type =	Gable		
Exposure Category =	В	Velocity Pressure Exposure Coefficient, Kz =	0.57		
Mean Roof Height =	15.00 ft	Topographic Factor, Kzt =	1.00		
Solar Array Dead Load =	3.00 psf	Wind Directionality Factor, Kd =	0.85		
a =	3.00 ft	Ground Elevation Factor, Ke =	1.00		

	DESIGN CALCULATIONS						
	Wind Velo	ocity Pressure, qh =	12.01 psf	(0.00256*Kz*Kzt*Kd*Ke*(V^2))			
Solar	Array Pressure Equa	lization Factor, γa =	0.60				
	Hardware Type =	Ecofasten RockIt Co	omp Slide				
	Allowable Load =	751.36 lbs	D. Fir - L, #12 Wood	Screw x 2, 2" Embedment			
Arra	ay Edge Factor, γE =	1.50	<b>Exposed Condition</b>				
Max. X - Spa	Max. X - Spacing (Zone 1 - 2r) =		Effective Wind Area				
Max. Y - Spa	Max. Y - Spacing (Zone 1 - 2r) =		22.60 ft²				
Max. X - Spaci	ng (Zone 2n & 3r) =	4.00 ft	Effective Wind Area				
Max. Y - Spaci	ng (Zone 2n & 3r) =	5.65 ft	22.60 ft <sup>2</sup>				
Max. X -	Spacing (Zone 3e) =	4.00 ft	Effective Wind Area				
Max. Y -	Spacing (Zone 3e) =	5.65 ft	22.60 ft²				
ROOF ZONE	GCp (-) UPLIFT	UPLIFT PRESSURE		PULLOUT FORCE			
1 - 2r	-1.45	-7.88 psf		178.20 lbs			
2n & 3r	-1.73	-9.71 psf		219.52 lbs			
3e	-2.14	-12.36 psf		279.25 lbs			

#### NOTE:

• Wind calculation is based on ASCE 7-16, 29.4 - C&C, LC #7: 0.6DL + 0.6WL is used.



**COMPANY** 

**PROJECT** 

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Roof1&Roof2

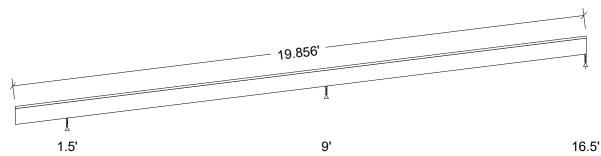
#### **Design Check Calculation Sheet**

WoodWorks Sizer

#### Loads:

Load	Type	Distribution	Pat-	Locatio	on [ft]	Magnitude	Unit
			tern	Start	End	Start End	
DL	Dead	Full Area	No			7.10(24.0")	psf
PV-DL	Dead	Partial Area	No	2.36	11.73	3.00(24.0")	psf
PV-SL	Snow	Partial Area	Yes	2.36	11.73	25.00(24.0")	psf
RF-SL1	Snow	Partial Area	Yes	0.00	2.36	25.00(24.0")	psf
RF-SL2	Snow	Partial Area	Yes	11.73	16.50	25.00(24.0")	psf
RF-LL1	Live	Partial Area	Yes	0.00	2.36	16.00(24.0")	psf
RF-LL2	Live	Partial Area	Yes	11.73	16.50	16.00(24.0")	psf

#### Maximum Reactions (lbs), Bearing Capacities (lbs) and Bearing Lengths (in):



Unfactored:			
Dead	99	196	54
Live	78	64	98
Snow	245	436	164
Factored:			
Total	343	633	251
Bearing:			
F'theta	776	776	776
Capacity			
Joist	1019	1065	582
Support	586	633	586
Des ratio			
Joist	0.34	0.59	0.43
Support	0.59	1.00	0.43
Load comb	#14	#17	#23
Length	0.50*	0.54	0.50*
Min req'd	0.50*	0.54**	0.50*
Cb	1.75	1.69	1.00
Cb min	1.75	1.69	1.00
Cb support	1.25	1.25	1.25
Fcp sup	625	625	625

<sup>\*</sup>Minimum bearing length setting used: 1/2" for end supports and 1/2" for interior supports

#### Lumber-soft, D.Fir-L, No.2, 2x6 (1-1/2"x5-1/2")

Supports: All - Timber-soft Beam, D.Fir-L No.2

Roof joist spaced at 24.0" c/c; Total length: 20.19'; Clear span(horz): 1.5', 7.438', 7.438'; Volume = 1.2 cu.ft.; Pitch: 8/12 Lateral support: top = continuous, bottom = at end supports; Repetitive factor: applied where permitted (refer to online help);

This section PASSES the design code check.

<sup>\*\*</sup>Minimum bearing length governed by the required width of the supporting member.

#### WoodWorks® Sizer

#### SOFTWARE FOR WOOD DESIGN

#### Roof1&Roof2

#### WoodWorks® Sizer

WARNING: Member length exceeds typical stock length of 18.0 ft

#### Analysis vs. Allowable Stress and Deflection using NDS 2018:

Criterion	Analysis Value	Design Value	Unit	Analysis/Design
Shear	fv = 47	Fv' = 207	psi	fv/Fv' = 0.23
Bending(+)	fb = 558	Fb' = 1547	psi	fb/Fb' = 0.36
Bending(-)	fb = 783	Fb' = 822	psi	fb/Fb' = 0.95
Deflection:			_	
Interior Live	0.11 = < L/999	0.60 = L/180	in	0.18
Total	0.14 = L/779	0.90 = L/120	in	0.15
Cantil. Live	-0.05 = L/402	0.24 = L/90	in	0.22
Total	-0.08 = L/257	0.36 = L/60	in	0.23

#### **Additional Data:**

```
CF
FACTORS: F/E(psi) CD
                                              Cfu
                                                                Ci
                                                                      LC#
                      CM
                            Ct
                                  CL
                                                    Cr
                                                         Cfrt
              1.15 1.00 1.00
                                                         1.00
                                                               1.00
Fv'
         180
                                                                      17
Fb'+
          900
                1.15 1.00 1.00 1.000 1.300
                                                    1.15
                                                         1.00
                                                               1.00
                                                                      23
Fb'-
          900
                                                    1.15 1.00
                1.15 1.00 1.00 0.531 1.300
                                                               1.00
                                                                      17
         625
                                                               1.00
Fcp'
                      1.00 1.00
                                                         1.00
         1.6 million 1.00 1.00
                                                               1.00
                                                                      13
Ε'
                                                         1.00
Emin' 0.58 million 1.00 1.00
                                                         1.00
                                                               1.00
                                                                      13
```

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CRITICAL LOAD COMBINATIONS:
          : LC #17 = D + S (pattern: sSS)
 Bending(+): LC \#23 = D + 0.75(L + S) (pattern: XsX)
 Bending(-): LC #17 = D + S (pattern: sSS)
 Deflection: LC #13 =
                        (live)
             LC #13 =
                        (total)
Bearing
           : Support 1 - LC \#14 = D + S (pattern: SSs)
             Support 2 - LC #17 = D + S (pattern: sSS)
             Support 3 - LC \#23 = D + 0.75(L + S) (pattern: XsX)
Load Types: D=dead L=live S=snow
Load Patterns: s=S/2, X=L+S or L+Lr,
                                         =no pattern load in this span
 Load combinations: ASD Basic from ASCE 7-16 2.4; all LC's listed in the Analysis report
CALCULATIONS:
V \max = 281, V \text{ design} = 256 \text{ (NDS } 3.4.3.1(a)) lbs
M(+) = 352 lbs-ft; M(-) = 493 lbs-ft
EI = 33.27e06 lb-in^2
 "Live" deflection is due to all non-dead loads (live, wind, snow ...)
 Total deflection = 1.50 permanent + "live"
Bearing: Allowable bearing at an angle F'theta calculated for each support
 as per NDS 3.10.3
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#### **Design Notes:**

1. Analysis and design are in accordance with the ICC International Building Code (IBC 2021) and the National Design Specification (NDS 2018), using Allowable Stress Design (ASD). Design values are from the NDS Supplement.

Lateral stability(-): Lu = 18.00' Le = 27.31' RB = 28.3; Lu based on full span

- 2. Please verify that the default deflection limits are appropriate for your application.
- 3. Continuous or Cantilevered Beams: NDS Clause 4.2.5.5 requires that normal grading provisions be extended to the middle 2/3 of 2 span beams and to the full length of cantilevers and other spans.
- 4. Sawn lumber bending members shall be laterally supported according to the provisions of NDS Clause 4.4.1.
- 5. SLOPED BEAMS: level bearing is required for all sloped beams.