



CIVIL/STRUCTURAL ENGINEERING DEPARTMENT

**STRUCTURAL CALCULATIONS  
STEIGERWALT RESIDENCE  
ROOF IMPROVEMENTS AT PV PANELS**

5424 Se 64th Ave  
Portland, Oregon

January 9, 2024



**DESIGN PARAMETERS:**

**2022 Oregon Structural Specialty Code**

<b>Supervising Engineer:</b>	<b>Trevor Jones, PE</b>	<b>(208)-994-1680</b>
<b>Structural Project Manager:</b>	<b>Troy Custodio</b>	<b>(208)-994-1680</b>

ROOF DEAD LOAD.....	7 psf
SOLAR DEAD LOAD.....	2.53 psf
LIVE (SNOW) LOAD.....	20 psf (non-reducible)

**CONTENTS:**

	Pages
Project Notes & Loading.....	2
RISA Roof Analysis.....	3 - 17
Collar Tie Analysis.....	18
Heel Connection Analysis.....	19 - 20

5715 Bedford Street • Pasco, WA 99301 • [www.solgenpower.com](http://www.solgenpower.com)



CIVIL/STRUCTURAL ENGINEERING DEPARTMENT

Subject: STEIGERWALT RESIDENCE ROOF 1  
 Engineer: TAJ Eng. Tech: Troy Custodio  
 Date: 12/28/2023

## Project Notes

\* Point load locations and tributary areas have been measured by hand from the plans. Although multiple loading conditions exist, the one that has been selected for analysis is believed to be the most conservative, based on engineering judgement, considering point load locations, quantity, and magnitudes, and location of intermediate supports (if any).

## Distributed Loading

### Existing Dead Load - Rafter/TC

Asphalt Shingles	3	psf
1/2" Plywood	1.5	psf
Framing	--	psf*
M,E, & Misc	0.5	psf
<b>Total Existing Dead Load - TC*</b>	<b>5</b>	<b>psf</b>

\* - framing accounted for with member self-weight in RISA, not included in this calc.

### Existing Dead Load - Joist/BC

1/2" Gypsum	1.5	psf
Blown-In Insulation	0.5	psf
Framing	--	psf*
<b>Total Existing Dead Load - BC*</b>	<b>2</b>	<b>psf</b>
<b>Solar Panel Dead Load</b>	<b>2.53</b>	<b>psf</b>

### Snow Load

Sloped Roof Snow Load	20.0	psf
-----------------------	------	-----

**Note:** Roof Live Load will not govern over snow loads, and is therefore not treated in this analysis. ( $p_{snow} = p_{RLL}$ , but  $C_{d,snow} < C_{d,RLL}$ . Also, RLL may be removed where panels are located per the IBC, while snow loads are non-reducible.)

## Line and Point Loading

### Line Loads

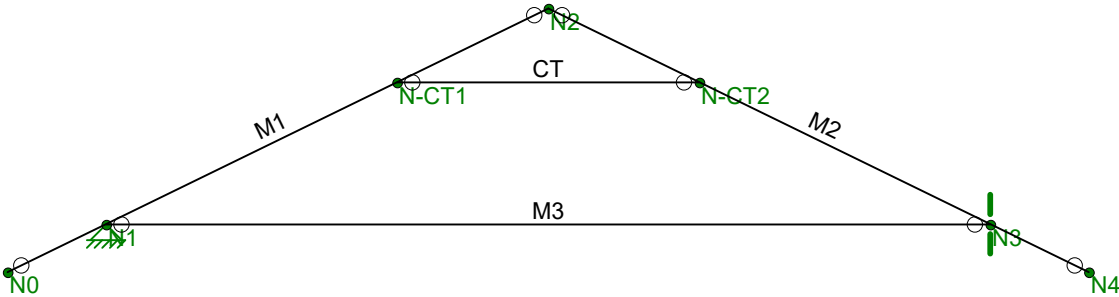
Tributary Width	2	ft
<b>Dead Load - TC</b>	<b>10</b>	<b>plf</b>
<b>Dead Load - BC</b>	<b>4</b>	<b>plf</b>
<b>Snow Load</b>	<b>40</b>	<b>plf</b>

	Start Loc	End Loc	
Snow Shade Locations on Left Roof	0.80	7.60	ft from rafter end
Snow Shade Locations on Right Roof	3.00	12.15	ft from ridge

### Point Loads

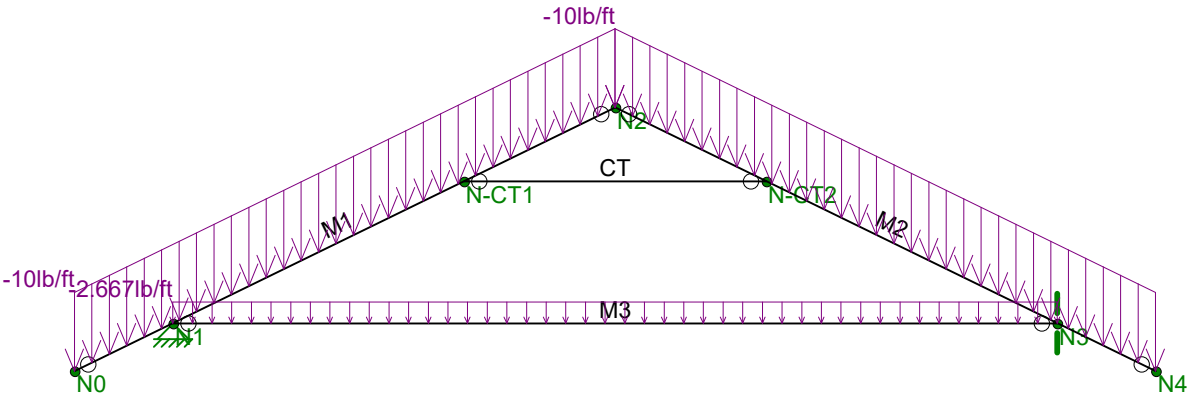
	Trib area (ft <sup>2</sup> )	Location (ft)	Solar pt load	Snow pt load	
Right Roof Load #1	11.5	7.25	29.095	230	lbs
Right Roof Load #2	7	11.15	17.71	140	lbs

Right Roof Load #1	11.5	4.5	29.095	230	lbs
Right Roof Load #2	7	9.75	17.71	140	lbs



Envelope Only Solution

Solgen Power	Steigerwalt Roof 1	SK - 1
TAJ		Dec 28, 2023 at 2:33 AM
		Matthew Steigerwalt - RISA.r2d



Loads: BLC 1, DL  
Envelope Only Solution

Solgen Power

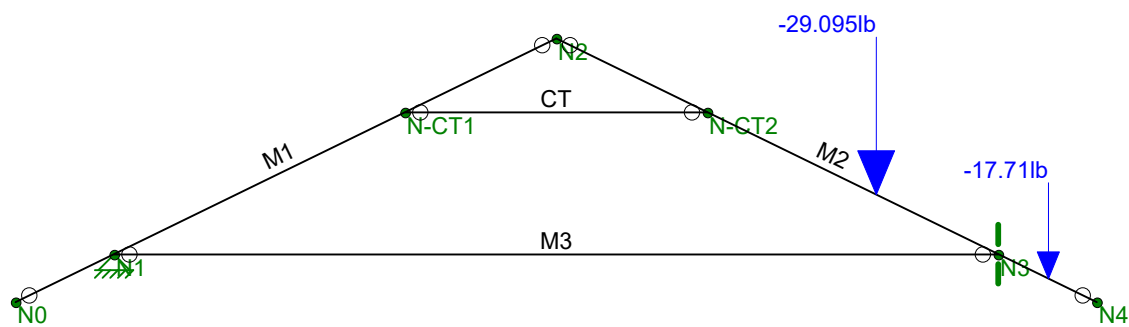
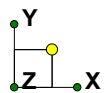
TAJ

Steigerwalt Roof 1

SK - 2

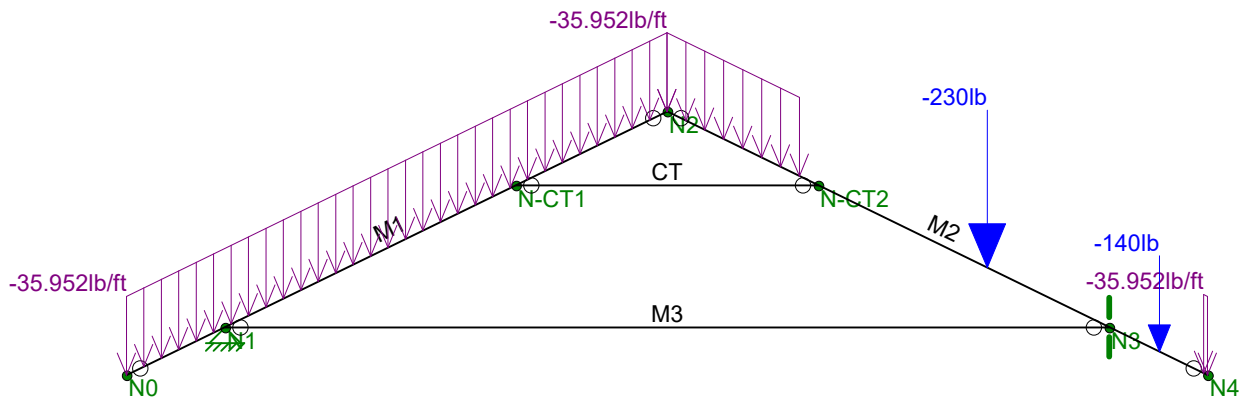
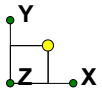
Dec 28, 2023 at 2:34 AM

Matthew Steigerwalt - RISA.r2d



Loads: BLC 2, DL - Solar  
Envelope Only Solution

Solgen Power	Steigerwalt Roof 1	SK - 3
TAJ		Dec 28, 2023 at 2:34 AM
		Matthew Steigerwalt - RISA.r2d

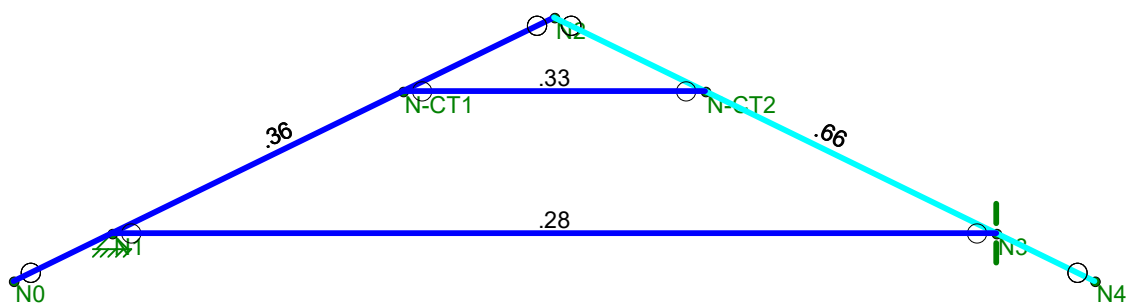


Loads: BLC 3, SL  
Envelope Only Solution

Solgen Power	Steigerwalt Roof 1	SK - 4
TAJ		Dec 28, 2023 at 2:34 AM
		Matthew Steigerwalt - RISA.r2d

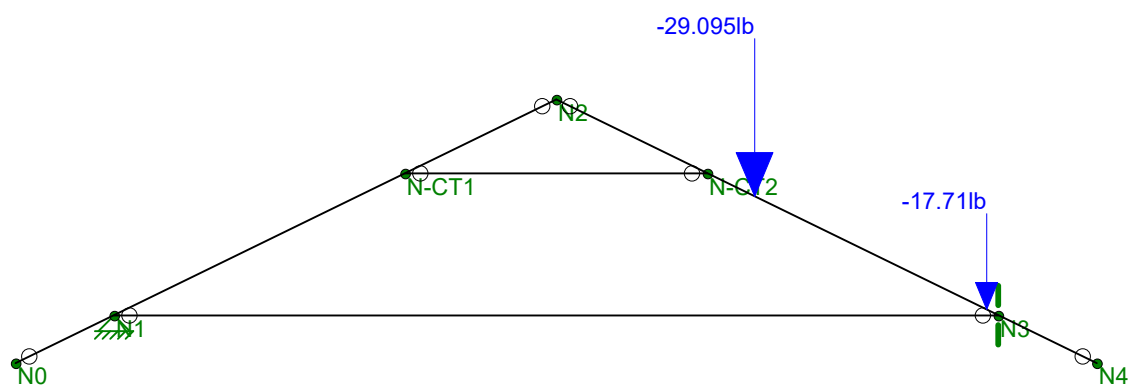
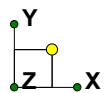


Code Check ( Env )	
<span style="background-color: black; color: black;"> </span>	No Calc
<span style="background-color: red; color: red;"> </span>	> 1.0
<span style="background-color: magenta; color: magenta;"> </span>	.90-1.0
<span style="background-color: green; color: green;"> </span>	.75-.90
<span style="background-color: cyan; color: cyan;"> </span>	.50-.75
<span style="background-color: blue; color: blue;"> </span>	0-.50



Member Code Checks Displayed (Enveloped)  
Envelope Only Solution

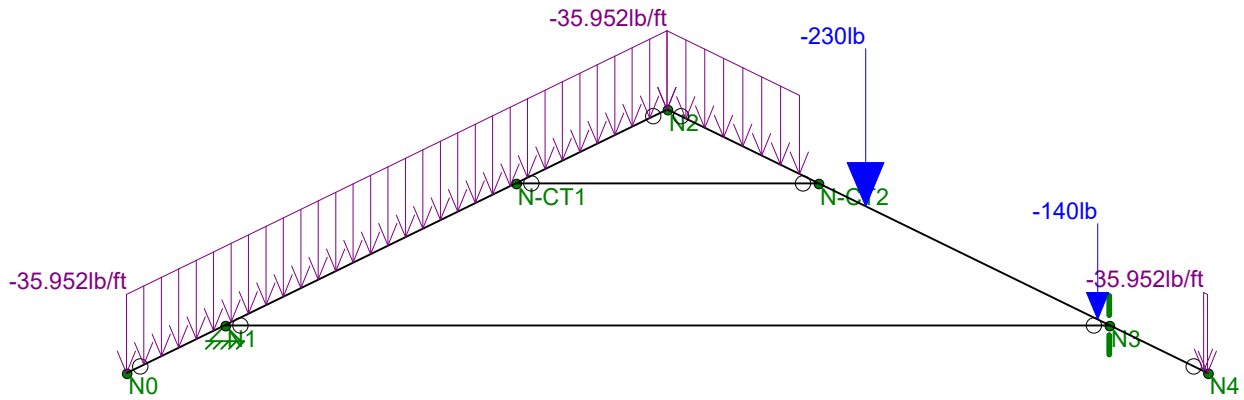
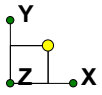
Solgen Power	Steigerwalt Roof 1	SK - 5
TAJ		Dec 28, 2023 at 2:34 AM
		Matthew Steigerwalt - RISA.r2d



Loads: BLC 2, DL - Solar  
Envelope Only Solution

Solgen Power	Steigerwalt Roof 1	SK - 6
TAJ		Jan 10, 2024 at 3:38 AM
		Matthew Steigerwalt - RISA.r2d



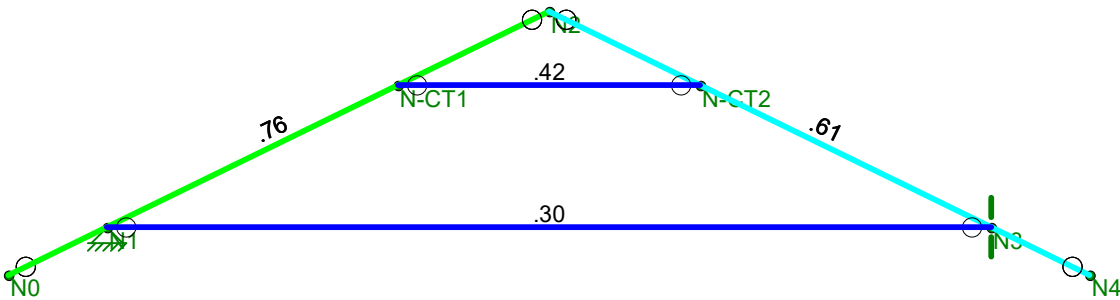


Loads: BLC 3, SL  
Envelope Only Solution

Solgen Power	Steigerwalt Roof 1	SK - 7
TAJ		Jan 10, 2024 at 3:38 AM
		Matthew Steigerwalt - RISA.r2d



Code Check ( Env )	
<div></div>	No Calc
<div></div>	> 1.0
<div></div>	.90-1.0
<div></div>	.75-.90
<div></div>	.50-.75
<div></div>	0-.50



Member Code Checks Displayed (Enveloped)  
Loads: BLC 4,  
Envelope Only Solution

Solgen Power	Steigerwalt Roof 1	SK - 8
TAJ		Jan 10, 2024 at 3:38 AM
		Matthew Steigerwalt - RISA.r2d

### (Global) Model Settings

Display Sections for Member Calcs	5
Max Internal Sections for Member Calcs	97
Include Shear Deformation?	Yes
Increase Nailing Capacity for Wind?	Yes
Merge Tolerance (in)	0.12
P-Delta Analysis Tolerance	0.50%
Include P-Delta for Walls?	Yes
Automatically Iterate Stiffness for Walls?	Yes
Max Iterations for Wall Stiffness	3
Gravity Acceleration (ft/sec^2)	32.2
Wall Mesh Size (in)	12
Eigensolution Convergence Tol. (1.E-)	4
Dynamic Solver	Accelerated Solver

Hot Rolled Steel Code	AISC 15th (360-16): ASD
Adjust Stiffness?	Yes(Iterative)
Cold Formed Steel Code	AISI S100-16: ASD
Wood Code	AWC NDS-18: ASD
Wood Temperature	< 100F
Concrete Code	ACI 318-19
Masonry Code	TMS 402-16: ASD
Aluminum Code	AA ADM1-15: ASD - Building
Number of Shear Regions	4
Region Spacing Increment (in)	4
Concrete Stress Block	Rectangular
Use Cracked Sections?	Yes
Bad Framing Warnings?	No
Unused Force Warnings?	Yes
Min 1 Bar Diam. Spacing?	No
Concrete Rebar Set	REBAR SET ASTMA615
Min % Steel for Column	1
Max % Steel for Column	8

### Wood Material Properties

	Label	Type	Database	Species	Grade	Cm	Ci	Emod	Nu	Therm (/...	Dens[k/ft...
1	DF	Solid Sa...	Visually ...	Douglas F...	No.2			1	0.3	0.3	0.035
2	SP	Solid Sa...	Visually ...	Southern ...	No.1			1	0.3	0.3	0.035
3	HF	Solid Sa...	Visually ...	Hem-Fir	No.1			1	0.3	0.3	0.035
4	SPF	Solid Sa...	Visually ...	Spruce-Pi...	No.1			1	0.3	0.3	0.035
5	24F-1.8E DF Bala...	Glulam	NDS Ta...	24F-1.8E...	na			1	0.3	0.3	0.035
6	24F-1.8E DF Unba...	Glulam	NDS Ta...	24F-1.8E...	na			1	0.3	0.3	0.035
7	24F-1.8E SP Bala...	Glulam	NDS Ta...	24F-1.8E...	na			1	0.3	0.3	0.035
8	24F-1.8E SP Unba...	Glulam	NDS Ta...	24F-1.8E...	na			1	0.3	0.3	0.035
9	1.3E-1600F_VERS...	SCL	Boise Ca...	1.3E-160...	na			1	0.3	0.3	0.035
10	1.35E LSL_SolidSt...	SCL	Louisian...	1.35E LS...	na			1	0.3	0.3	0.035
11	1.3E_RIGIDLAM L...	SCL	SCL	1.3E_RIG...	na			1	0.3	0.3	0.035
12	2.0E_DF Parallam ...	SCL	TrusJoist	2.0E_DF ...	na			1	0.3	0.3	0.035
13	LVL_PRL_1.5E_2...	Custom	N/A	LVL_PRL...	na			1	0.3	0.3	0.035
14	LVL_Microlam_1.9...	Custom	N/A	LVL_Micr...	na			1	0.3	0.3	0.035
15	PSL_Parallam_2.0...	Custom	N/A	PSL_Para...	na			1	0.3	0.3	0.035
16	LSL_TimberStrand...	Custom	N/A	LSL_Timb...	na			1	0.3	0.3	0.035

### Joint Coordinates and Temperatures

	Label	X [ft]	Y [ft]	Temp [F]
1	N0	-2	-0.975465	0
2	N1	0	0	0
3	N2	9	4.389593	0
4	N3	18	0	0
5	N4	20	-0.975465	0
6	N-CT1	5.924544	2.889593	0
7	N-CT2	12.075456	2.889593	0

### Basic Load Cases

	BLC Description	Category	X Gravity	Y Gravity	Joint	Point	Distributed
1	DL	DL		-1			3
2	DL - Solar	DL				2	
3	SL	SL				2	3

### Load Combinations

	Description	Solve	PDelta	S...	BLC Fac...	BLC Fac...	BLC Fac...	BLC Fac...	BLC Fac...	BLC Fac...	BLC Fac...	BLC Fac...	BLC Fac...	BLC Fac...	BLC Fac...	BLC Fac...
1	DL	Yes	Y		DL	1										
2	DL + SL	Yes	Y		DL	1	SL	1								

### Member Primary Data

	Label	I Joint	J Joint	Rotate(deg)	Section/Shape	Type	Design List	Material	Design Rules
1	M1	N0	N2		Rafter / TC	None	None	DF	Typical
2	M2	N2	N4		Rafter / TC	None	None	DF	Typical
3	M3	N1	N3		Joist / BC	None	None	DF	Typical
4	CT	N-CT1	N-CT2		Collar Tie	None	None	DF	Typical

### Wood Design Parameters

	Label	Shape	Length[ft]	Le-out[ft]	Le-in[ft]	le-bend to...	le-bend bo...	K-out	K-in	CV	Cr	Out sway	In sway
1	M1	Rafter / TC	12.239	1	Segment	Lb out	Segment						
2	M2	Rafter / TC	12.239	1	Segment	Lb out	Segment						
3	M3	Joist / BC	18	1		Lb out							
4	CT	Collar Tie	6.151			Lb out							

### Wood Section Sets

	Label	Shape	Type	Design List	Material	Design Rules	A [in <sup>2</sup> ]	I (90,270) [i...]	I (0,180) [in <sup>4</sup> ]
1	Rafter / TC	2x4	None	None	DF	Typical	5.25	0.984	5.359
2	Joist / BC	2x6	None	None	DF	Typical	8.25	1.547	20.797
3	Sister	2x4	None	None	DF	Typical	5.25	0.984	5.359
4	Brace/post/k...	2x4	None	None	DF	Typical	5.25	0.984	5.359
5	Collar Tie	2x6	None	None	DF	Typical	8.25	1.547	20.797
6	Webbing	2x4	None	None	DF	Typical	5.25	0.984	5.359

### Envelope Member End Reactions

	Member	Membe...		Axial[lb]	LC	Shear[lb]	LC	Moment[lb-ft]	LC
1	M1	I	max	0	2	0.001	1	0	1
2			min	0	1	-0.056	2	0	1
3		J	max	54.998	2	-3.554	1	0	1

### Envelope Member End Reactions (Continued)

	Member	Membe...		Axial[lb]	LC	Shear[lb]	LC	Moment[lb-ft]	LC
4			min	14.408	1	-42.282	2	0	1
5	M2	I	max	67.108	2	17.277	2	0	1
6			min	11.681	1	9.17	1	0	1
7		J	max	0	2	0.025	2	0	1
8			min	0	1	0.01	1	0	1
9	M3	I	max	-181.684	1	42.047	1	0	1
10			min	-636.736	2	42.047	1	0	1
11		J	max	-181.684	1	-42.047	1	0	1
12			min	-636.736	2	-42.047	1	0	1
13	CT	I	max	568.809	2	6.167	1	0	1
14			min	167.171	1	6.167	1	0	1
15		J	max	568.809	2	-6.167	1	0	1
16			min	167.171	1	-6.167	1	0	1

### Envelope Wood Code Checks

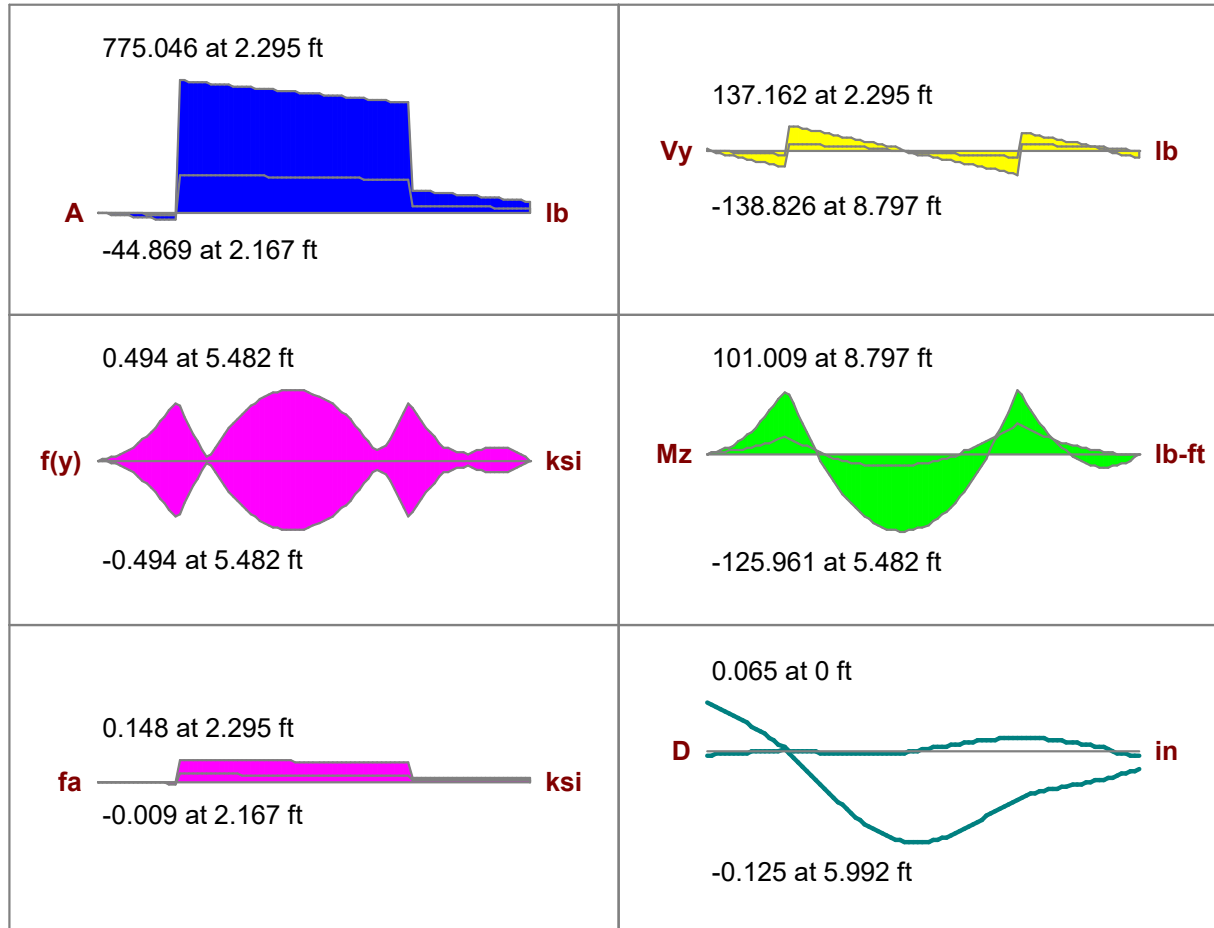
	Member	Shape	Code Check	Loc[ft]	LC	Shear ...	Loc[ft]	LC	Fc' [k...Ft' [ksi]	Fb' [k...Fv' [k...	RB	CL	CP	Eqn		
1	M1	2x4	0.356	5.482	2	0.192	8.797	2	0.865	1.164	1.721	0.207	4.32	0.998	0.436	3.9-3
2	M2	2x4	0.657	7.267	2	0.233	9.944	2	0.865	1.164	1.721	0.207	4.32	0.998	0.436	3.9-3
3	M3	2x6	0.277	9	2	0.042	18	1	0.318	1.009	1.49	0.18	5.416	0.997	0.168	3.9-1
4	CT	2x6	0.335	6.151	2	0.006	6.151	1	0.206	1.009	1.455	0.18	13.432	0.974	0.108	3.6.3

Member: **M1**Shape: **2x4**Material: **DF**Length: **12.239 ft**I Joint: **N0**J Joint: **N2**

Envelope

Code Check: **0.356 (LC 2)**

Report Based On 97 Sections

**AWC NDS-18: ASD Code Check**Max Bending Check **0.356 (LC 2)**Location **5.482 ft**Equation **3.9-3**CD **1.15** RB **4.32**Cr **1** Cfu **1**Max Shear Check **0.192 (LC 2)**Location **8.797 ft**Max Defl Ratio **L/994**CL **0.998**CP **0.436**

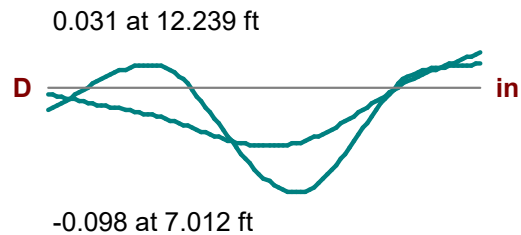
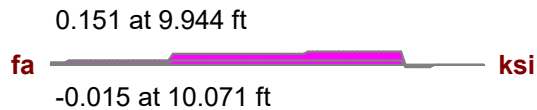
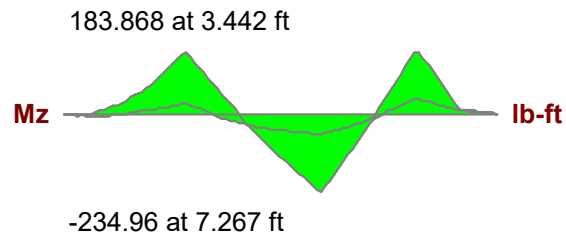
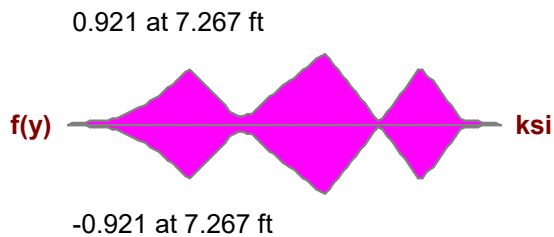
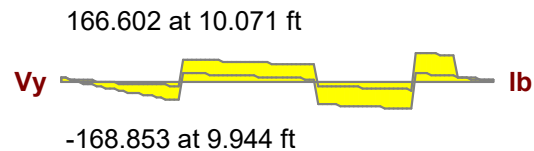
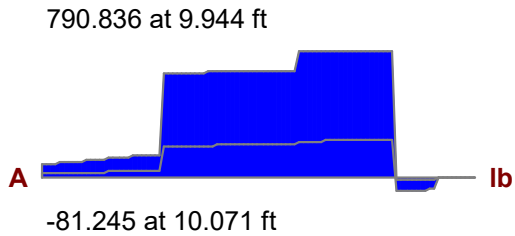
	(ksi)	Cm	Ct	CF	Ci		Out	In
Fc'	<b>0.865</b>	<b>1</b>	<b>1</b>	<b>1.15</b>	<b>1</b>	Lb	<b>1 ft</b>	<b>6.592 ft</b>
Ft'	<b>1.164</b>	<b>1</b>	<b>1</b>	<b>1.5</b>	<b>1</b>	le/d	<b>8</b>	<b>22.6</b>
Fb'	<b>1.721</b>	<b>1</b>	<b>1</b>	<b>1.5</b>	<b>1</b>	Sway	<b>No</b>	<b>No</b>
Fv'	<b>0.207</b>	<b>1</b>	<b>1</b>		<b>1</b>	Le-Bending Top	<b>1 ft</b>	
E'	<b>1700</b>	<b>1</b>	<b>1</b>		<b>1</b>	Le-Bending Bot	<b>6.592 ft</b>	

Member: **M2**Shape: **2x4**Material: **DF**Length: **12.239 ft**I Joint: **N2**J Joint: **N4**

Envelope

Code Check: **0.657 (LC 2)**

Report Based On 97 Sections

**AWC NDS-18: ASD Code Check**Max Bending Check **0.657 (LC 2)**Location **7.267 ft**Equation **3.9-3**CD **1.15** RB **4.32**Cr **1** Cfu **1**Max Shear Check **0.233 (LC 2)**Location **9.944 ft**Max Defl Ratio **L/1456**CL **0.998**CP **0.436**

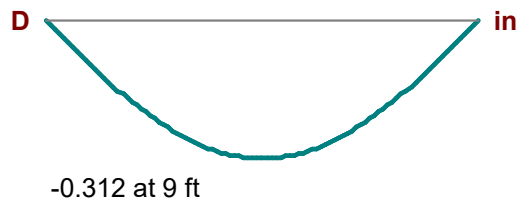
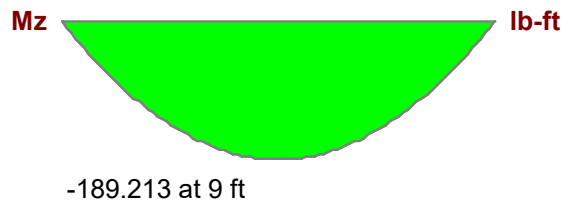
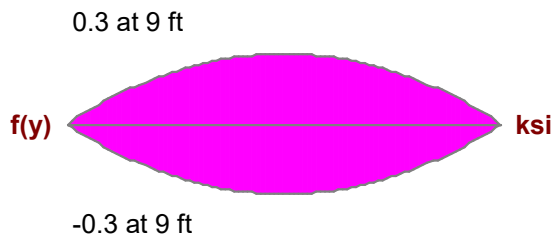
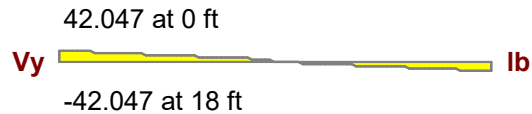
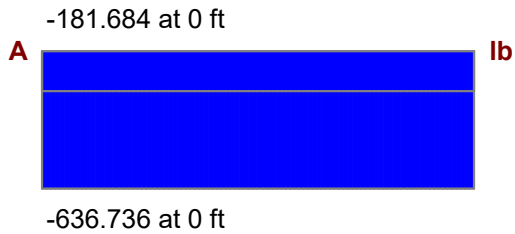
	(ksi)	Cm	Ct	CF	Ci		Out	In
Fc'	<b>0.865</b>	<b>1</b>	<b>1</b>	<b>1.15</b>	<b>1</b>	Lb	<b>1 ft</b>	<b>6.592 ft</b>
Ft'	<b>1.164</b>	<b>1</b>	<b>1</b>	<b>1.5</b>	<b>1</b>	le/d	<b>8</b>	<b>22.6</b>
Fb'	<b>1.721</b>	<b>1</b>	<b>1</b>	<b>1.5</b>	<b>1</b>	Sway	<b>No</b>	<b>No</b>
Fv'	<b>0.207</b>	<b>1</b>	<b>1</b>		<b>1</b>	Le-Bending Top	<b>1 ft</b>	
E'	<b>1700</b>	<b>1</b>	<b>1</b>		<b>1</b>	Le-Bending Bot		<b>6.592 ft</b>

Member: **M3**Shape: **2x6**Material: **DF**Length: **18 ft**I Joint: **N1**J Joint: **N3**

Envelope

Code Check: **0.277 (LC 2)**

Report Based On 97 Sections

**AWC NDS-18: ASD Code Check**Max Bending Check **0.277 (LC 2)**Location **9 ft**Equation **3.9-1**CD **1.15** RB **5.416**Cr **1** Cfu **1**Max Shear Check **0.042 (LC 1)**Location **18 ft**Max Defl Ratio **L/692**CL **0.997**CP **0.168**

	(ksi)	Cm	Ct	CF	Ci		Out	In
Fc'	<b>0.318</b>	<b>1</b>	<b>1</b>	<b>1.1</b>	<b>1</b>	Lb	<b>1 ft</b>	<b>18 ft</b>
Ft'	<b>1.009</b>	<b>1</b>	<b>1</b>	<b>1.3</b>	<b>1</b>	le/d	<b>8</b>	<b>39.273</b>
Fb'	<b>1.49</b>	<b>1</b>	<b>1</b>	<b>1.3</b>	<b>1</b>	Sway	<b>No</b>	<b>No</b>
Fv'	<b>0.18</b>	<b>1</b>	<b>1</b>		<b>1</b>	Le-Bending Top	<b>1 ft</b>	
E'	<b>1700</b>	<b>1</b>	<b>1</b>		<b>1</b>	Le-Bending Bot	<b>18 ft</b>	

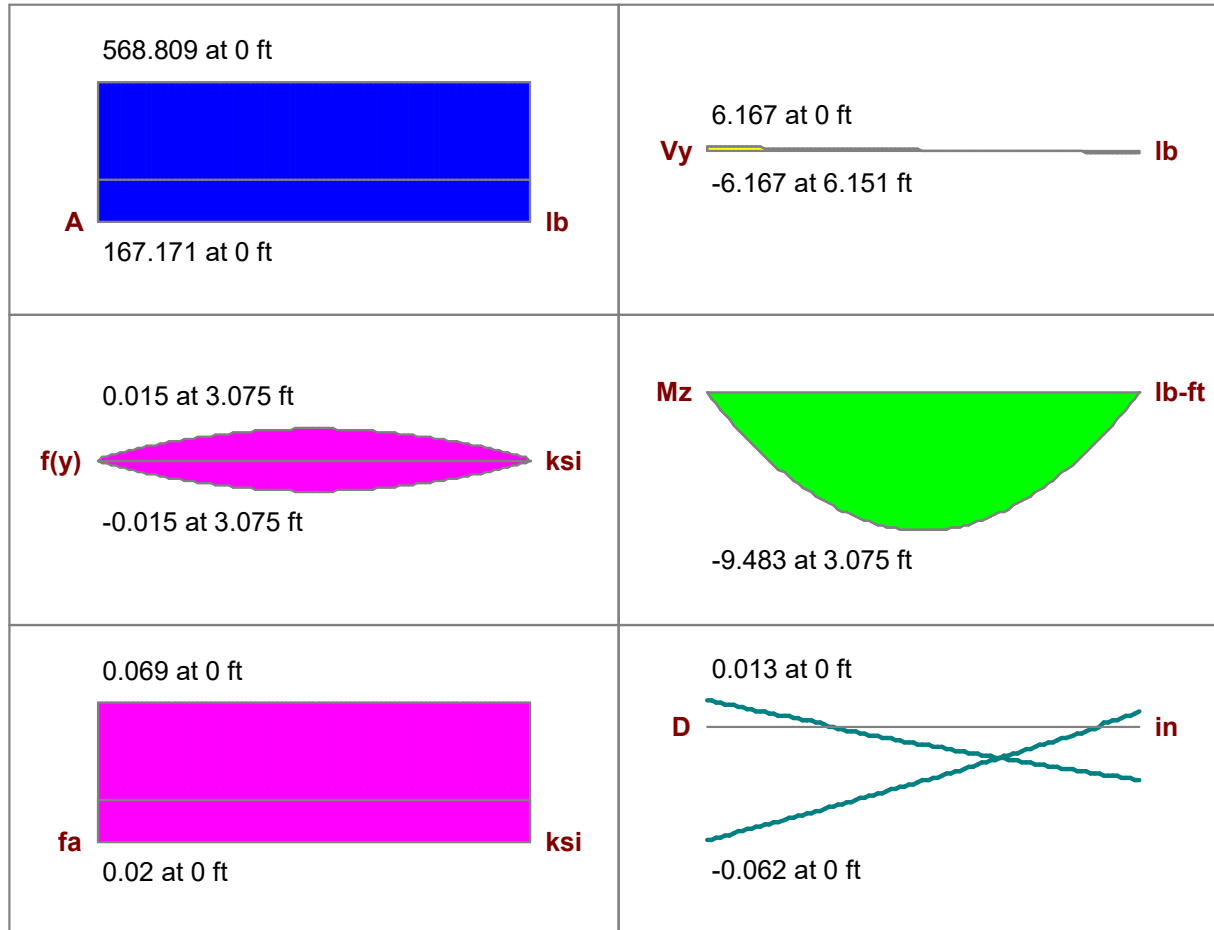


Member: **CT**Shape: **2x6**Material: **DF**Length: **6.151 ft**I Joint: **N-CT1**J Joint: **N-CT2**

Envelope

Code Check: **0.335 (LC 2)**

Report Based On 97 Sections

**AWC NDS-18: ASD Code Check**Max Bending Check **0.335 (LC 2)**Location **6.151 ft**Equation **3.6.3**CD **1.15** RB **13.432**Cr **1** Cfu **1**Max Shear Check **0.006 (LC 1)**Location **6.151 ft**Max Defl Ratio **L/10000**CL **0.974**CP **0.108**

	(ksi)	Cm	Ct	CF	Ci		Out	In
Fc'	<b>0.206</b>	<b>1</b>	<b>1</b>	<b>1.1</b>	<b>1</b>	Lb	<b>6.151 ft</b>	<b>6.151 ft</b>
Ft'	<b>1.009</b>	<b>1</b>	<b>1</b>	<b>1.3</b>	<b>1</b>	le/d	<b>49.207</b>	<b>13.42</b>
Fb'	<b>1.455</b>	<b>1</b>	<b>1</b>	<b>1.3</b>	<b>1</b>	Sway	<b>No</b>	<b>No</b>
Fv'	<b>0.18</b>	<b>1</b>	<b>1</b>		<b>1</b>	Le-Bending Top	<b>6.151 ft</b>	
E'	<b>1700</b>	<b>1</b>	<b>1</b>		<b>1</b>	Le-Bending Bot	<b>6.151 ft</b>	



Subject:  
Date:  
Engineer:

STEIGERWALT RESIDENCE ROOF 1

01/10/2024

TAJ

Eng. Tech:

Troy Custodio

CIVIL/STRUCTURAL ENGINEERING DEPARTMENT

## Connection Analysis

The purpose of this calculation is to verify the connections - either existing or as retrofit - are adequate for the required design loads.

### NEW COLLAR TIE CONNECTION

Connection Demand\*\*

779

lbs

\*\* - from RISA analysis. Tension in joist/bottom chord at member ends.

### Proposed Nail Connection

# of connectors

3

(assumed)

Connector Size &amp; Type

16d Common Wire Nail

(assumed)

Proposed Nail Connection Capacity

486

lbs (Note: nail capacity = 162 lbs)

### Proposed A34 Connection

# of connectors

1

(top and bottom)

Connector Size &amp; Type

A34, w/ #9 x 1 1/2" SDS Screws

Base Capacity (F1, Cd = 1.15\*)

640

lbs

Cr, repetitive member factor

1.15

Proposed A34 Connection Capacity

736

lbs

Total Connection Capacity

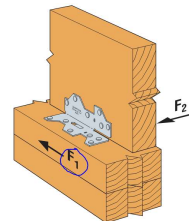
1222

lbs

OK

\* - linear interpolation between 1.00 and 1.25 values, below:

Model No.	Type of Connection	Fasteners (in.)	Direction of Load	DF/SP Allowable Loads		
				Floor (100)	Roof (125)	(160)
A34	1	(8) 0.131 x 1 1/2	F <sub>1</sub>	395	480	545
			F <sub>2</sub>	395	430	430
	1	(8) #9 x 1 1/2 SD	F <sub>1</sub>	640	640	640
			F <sub>2</sub>	495	495	495
			Uplift	240	240	240





Subject:  
Date:  
Engineer:

STEIGERWALT RESIDENCE ROOF 1

12/28/2023

TAJ

Eng. Tech:

Troy Custodio

CIVIL/STRUCTURAL ENGINEERING DEPARTMENT

## **Connection Analysis**

The purpose of this calculation is to verify the connections - either existing or as retrofit - are adequate for the required design loads.

### **HEEL CONNECTION**

Connection Demand\*\*

637

lbs

\*\* - from RISA analysis. Tension in joist/bottom chord at member ends.

### **Existing Connection**

# of connectors

4

(assumed)

Connector Size & Type

16d Common Wire Nail

(assumed)

Existing Connection Capacity

648

lbs (Note: nail capacity = 162 lbs per next page)

**OK**

7/27/2021

## Connection Calculator

<b>Design Method</b>	Allowable Stress Design (ASD)	▼
<b>Connection Type</b>	Lateral loading	▼
<b>Fastener Type</b>	Nail	▼
<b>Loading Scenario</b>	Single Shear	▼

<b>Main Member Type</b>	Douglas Fir-Larch	▼
<b>Main Member Thickness</b>	1.5 in.	▼
<b>Side Member Type</b>	Douglas Fir-Larch	▼
<b>Side Member Thickness</b>	1.5 in.	▼
<b>Nail Type</b>	Common Wire	▼
<b>Nail Size</b>	16d (D = 0.162 in.; L = 3.5 in.)	▼
<b>Load Duration Factor</b>	C <sub>D</sub> = 1.15	▼
<b>Wet Service Factor</b>	C <sub>M</sub> = 1.0	▼
<b>End Grain Factor</b>	C <sub>eg</sub> = 1.0	▼
<b>Temperature Factor</b>	C <sub>t</sub> = 1.0	▼
<b>Diaphragm Factor</b>	C <sub>di</sub> = 1.0	▼

## Connection Yield Modes

Im	591 lbs.
Is	591 lbs.
II	245 lbs.
III <sub>m</sub>	219 lbs.
III <sub>s</sub>	219 lbs.
IV	162 lbs.

<b>Adjusted ASD Capacity</b>	<b>162 lbs.</b>
Fastener length exceeds total connection thickness	

- Nail bending yield strength of 90000 psi is assumed.
- The Adjusted ASD Capacity does not apply for toe-nails installed in wood members.
- Length of tapered tip is assumed to be two times the nail diameter for calculating dowel bearing length in the main member.
- The Adjusted ASD Capacity only applies for nails that have been driven flush with the side member surface. It does not apply for nails that have been overdriven into the side member.

While every effort has been made to insure the accuracy of the information presented, and special effort has been made to assure that the information reflects the state-of-the-art, neither the American Wood Council nor its members assume any responsibility for any particular design prepared from this on-line Connection Calculator. Those using this on-line Connection Calculator assume all liability from its use.

The Connection Calculator was designed and created by Cameron Knudson, Michael Dodson and David Pollock at Washington State University. Support for development of the Connection Calculator was provided by [American Wood Council](#).

**NAIL CAPACITY CALCULATION,  
PER AWC'S ONLINE CALCULATOR**



CIVIL/STRUCTURAL ENGINEERING DEPARTMENT

**STRUCTURAL CALCULATIONS  
STEIGERWALT RESIDENCE  
ROOF IMPROVEMENTS AT PV PANELS**

5424 Se 64th Ave  
Portland, Oregon

October 24, 2023



**DESIGN PARAMETERS:**

**2022 Oregon Structural Specialty Code**

<b>Supervising Engineer:</b>	<b>Trevor Jones, PE</b>	<b>(208)-994-1680</b>
<b>Structural Project Manager:</b>	<b>Troy Custodio</b>	<b>(208)-994-1680</b>

ROOF DEAD LOAD.....	9 psf
SOLAR DEAD LOAD.....	2.53 psf
LIVE (SNOW) LOAD.....	20 psf (non-reducible)

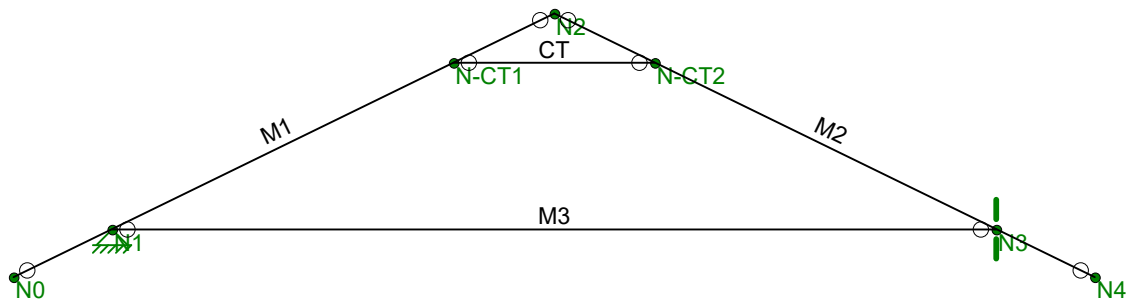
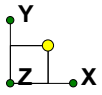
**CONTENTS:**

	Pages
Project Notes & Loading.....	2
RISA Roof Analysis.....	3 - 10

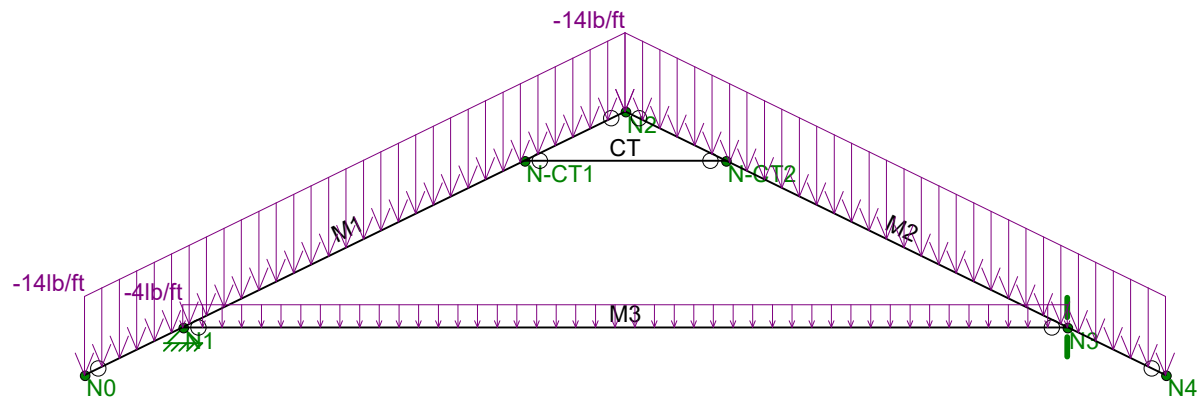
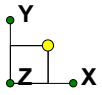
CIVIL/STRUCTURAL ENGINEERING DEPARTMENT

\* Point load locations and tributary areas have been measured by hand from the plans. Although multiple loading conditions exist, the one that has been selected for analysis is believed to be the most conservative, based on engineering judgement, considering point load locations, quantity, and magnitudes, and location of intermediate supports (if any).

[illegible]



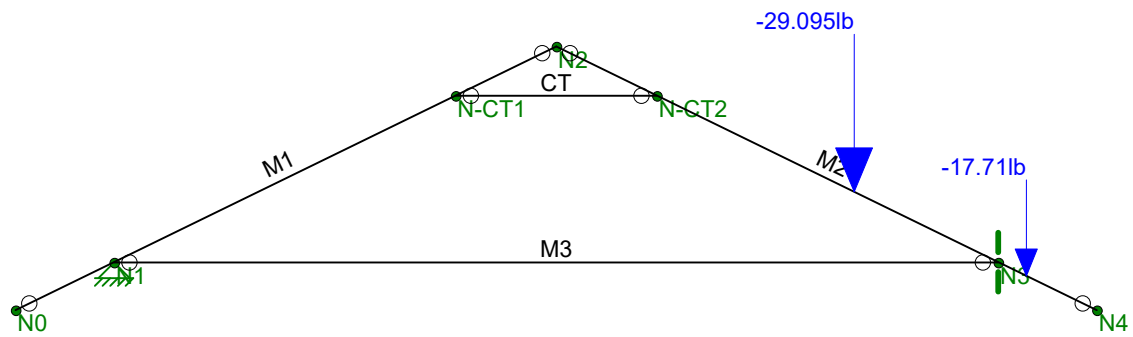
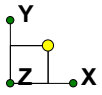
Solgen Power	Steigerwalt Roof 1	SK - 1
TAJ		Oct 25, 2023 at 5:51 AM
		Matthew Steigerwalt - RISA.r2d



Loads: BLC 1, DL

Solgen Power	Steigerwalt Roof 1	SK - 2
TAJ		Oct 25, 2023 at 5:51 AM
		Matthew Steigerwalt - RISA.r2d





Loads: BLC 2, DL - Solar

Solgen Power

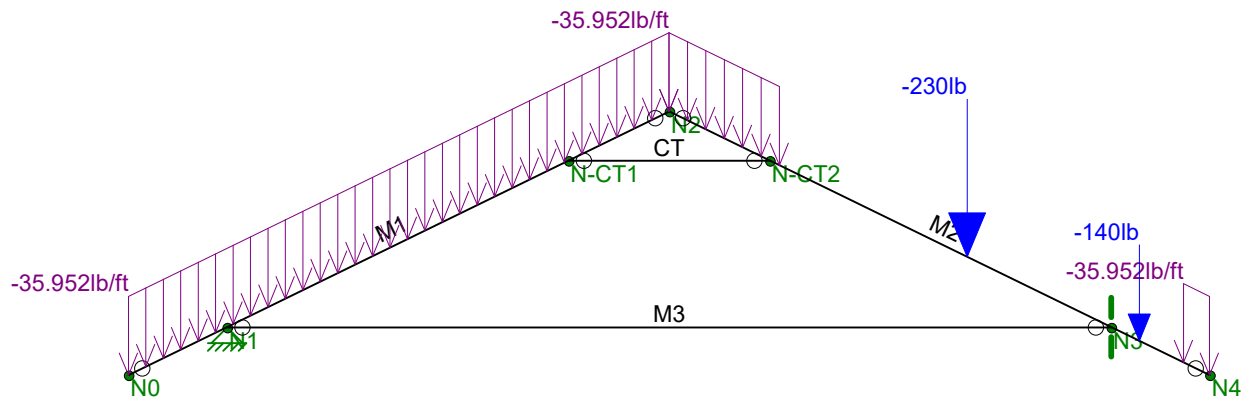
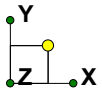
TAJ

Steigerwalt Roof 1

SK - 3

Oct 25, 2023 at 5:51 AM

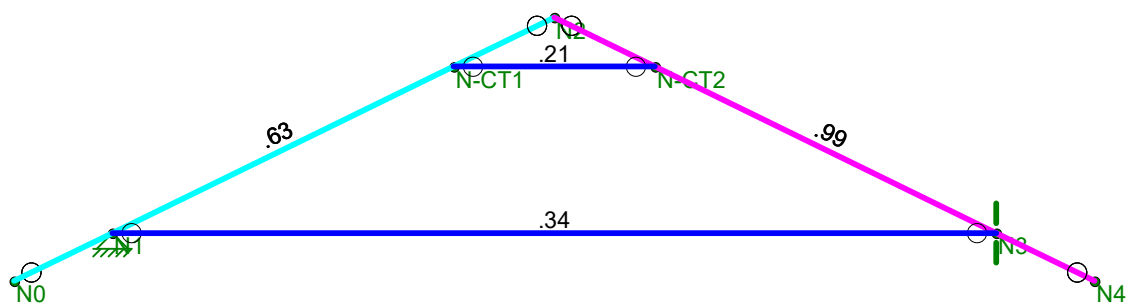
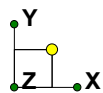
Matthew Steigerwalt - RISA.r2d



Loads: BLC 3, SL

Solgen Power	Steigerwalt Roof 1	SK - 4
TAJ		Oct 25, 2023 at 5:51 AM
		Matthew Steigerwalt - RISA.r2d

Code Check ( Env )	
<span style="background-color: black; color: black;"> </span>	No Calc
<span style="background-color: red; color: red;"> </span>	> 1.0
<span style="background-color: magenta; color: magenta;"> </span>	.90-1.0
<span style="background-color: green; color: green;"> </span>	.75-.90
<span style="background-color: cyan; color: cyan;"> </span>	.50-.75
<span style="background-color: blue; color: blue;"> </span>	0-.50



Member Code Checks Displayed (Enveloped)  
 Loads: BLC 4,  
 Envelope Only Solution

Solgen Power	Steigerwalt Roof 1	SK - 5
TAJ		Oct 25, 2023 at 5:52 AM
		Matthew Steigerwalt - RISA.r2d

### (Global) Model Settings

Display Sections for Member Calcs	5
Max Internal Sections for Member Calcs	97
Include Shear Deformation?	Yes
Increase Nailing Capacity for Wind?	Yes
Merge Tolerance (in)	0.12
P-Delta Analysis Tolerance	0.50%
Include P-Delta for Walls?	Yes
Automatically Iterate Stiffness for Walls?	Yes
Max Iterations for Wall Stiffness	3
Gravity Acceleration (ft/sec^2)	32.2
Wall Mesh Size (in)	12
Eigensolution Convergence Tol. (1.E-)	4
Dynamic Solver	Accelerated Solver

Hot Rolled Steel Code	AISC 15th (360-16): ASD
Adjust Stiffness?	Yes(Iterative)
Cold Formed Steel Code	AISI S100-16: ASD
Wood Code	AWC NDS-18: ASD
Wood Temperature	< 100F
Concrete Code	ACI 318-19
Masonry Code	TMS 402-16: ASD
Aluminum Code	AA ADM1-15: ASD - Building
Number of Shear Regions	4
Region Spacing Increment (in)	4
Concrete Stress Block	Rectangular
Use Cracked Sections?	Yes
Bad Framing Warnings?	No
Unused Force Warnings?	Yes
Min 1 Bar Diam. Spacing?	No
Concrete Rebar Set	REBAR SET ASTMA615
Min % Steel for Column	1
Max % Steel for Column	8

### Wood Material Properties

	Label	Type	Database	Species	Grade	Cm	Ci	Emod	Nu	Therm (/1...	Dens[k/ft...
1	DF	Solid Sawn	Visually ...	Douglas Fir-Larch	No.2			1	0.3	0.3	0.035
2	SP	Solid Sawn	Visually ...	Southern Pine	No.1			1	0.3	0.3	0.035
3	HF	Solid Sawn	Visually ...	Hem-Fir	No.1			1	0.3	0.3	0.035
4	SPF	Solid Sawn	Visually ...	Spruce-Pine-fir	No.1			1	0.3	0.3	0.035
5	24F-1.8E DF...	Glulam	NDS Tabl...	24F-1.8E DF BAL	na			1	0.3	0.3	0.035
6	24F-1.8E DF...	Glulam	NDS Tabl...	24F-1.8E_DF_UNBAL	na			1	0.3	0.3	0.035
7	24F-1.8E SP...	Glulam	NDS Tabl...	24F-1.8E SP BAL	na			1	0.3	0.3	0.035
8	24F-1.8E SP...	Glulam	NDS Tabl...	24F-1.8E_SP_UNBAL	na			1	0.3	0.3	0.035
9	1.3E-1600F_...	SCL	Boise Ca...	1.3E-1600F_VERSAL...	na			1	0.3	0.3	0.035
10	1.35E LSL_S...	SCL	Louisiana...	1.35E LSL_SolidStart	na			1	0.3	0.3	0.035
11	1.3E RIGIDL...	SCL	Roseburg...	1.3E RIGIDLAM LVL	na			1	0.3	0.3	0.035
12	2.0E_DF Par...	SCL	TrusJoist	2.0E_DF Parallam PSL	na			1	0.3	0.3	0.035
13	LVL_PRL_1...	Custom	N/A	LVL_PRL_1.5E 2250F	na			1	0.3	0.3	0.035
14	LVL_MicroLa...	Custom	N/A	LVL_Microllam_1.9E...	na			1	0.3	0.3	0.035
15	PSL_Paralla...	Custom	N/A	PSL_Parallam_2.0E_...	na			1	0.3	0.3	0.035
16	LSL_Timber...	Custom	N/A	LSL_TimberStrand_1...	na			1	0.3	0.3	0.035

### Joint Coordinates and Temperatures

	Label	X [ft]	Y [ft]	Temp [F]
1	N0	-2	-0.975465	0
2	N1	0	0	0
3	N2	9	4.389593	0
4	N3	18	0	0
5	N4	20	-0.975465	0
6	N-CT1	6.949696	3.389593	0
7	N-CT2	11.050304	3.389593	0

### Basic Load Cases

	BLC Description	Category	X Gravity	Y Gravity	Joint	Point	Distributed
1	DL	DL		-1			3
2	DL - Solar	DL				2	
3	SL	SL				2	3

### Load Combinations

	Description So...	PDelta	S...	BLC Fac...	BLC Fac...	BLC Fac...	BLC Fac...	BLC Fac...	BLC Fac...	BLC Fac...	BLC Fac...	BLC Fac...	BLC Fac...	BLC Fac...	BLC Fac...	BLC Fac...
1	DL	Yes	Y	DL	1											
2	DL + SL	Yes	Y	DL	1	SL	1									

### Member Primary Data

	Label	I Joint	J Joint	Rotate(deg)	Section/Shape	Type	Design List	Material	Design Rules
1	M1	N0	N2		Rafter / TC	None	None	DF	Typical
2	M2	N2	N4		Rafter / TC	None	None	DF	Typical
3	M3	N1	N3		Joist / BC	None	None	DF	Typical
4	CT	N-CT1	N-CT2		Collar Tie	None	None	DF	Typical

### Wood Design Parameters

	Label	Shape	Length[ft]	Le-out[ft]	Le-in[ft]	le-bend to...	le-bend bo...	K-out	K-in	CV	Cr	Out sway	In sway
1	M1	Rafter / TC	12.239	1	Segment	Lb out	Segment						
2	M2	Rafter / TC	12.239	1	Segment	Lb out	Segment						
3	M3	Joist / BC	18	1		Lb out							
4	CT	Collar Tie	4.101			Lb out							

### Wood Section Sets

	Label	Shape	Type	Design List	Material	Design Rules	A [in <sup>2</sup> ]	I (90,270) [i...]	I (0,180) [in <sup>4</sup> ]
1	Rafter / TC	2x4	None	None	DF	Typical	5.25	0.984	5.359
2	Joist / BC	2x6	None	None	DF	Typical	8.25	1.547	20.797
3	Sister	2x4	None	None	DF	Typical	5.25	0.984	5.359
4	Brace/post/kn...	2x4	None	None	DF	Typical	5.25	0.984	5.359
5	Collar Tie	2x6	None	None	DF	Typical	8.25	1.547	20.797
6	Webbing	2x4	None	None	DF	Typical	5.25	0.984	5.359

### Envelope Member End Reactions

	Member	Membe...		Axial[lb]	LC	Shear[lb]	LC	Moment[lb-ft]	LC
1	M1	I	max	0	2	-0.005	1	0	1
2			min	0	1	-0.109	2	0	1
3		J	max	-34.733	1	41.532	2	0	1

### Envelope Member End Reactions (Continued)

Member	Member...		Axial[lb]	LC	Shear[lb]	LC	Moment[lb-ft]	LC
4		min	-110.71	2	21.821	1	0	1
5	M2	I	max	1	-13.95	1	0	1
6		min	-100.866	2	-61.683	2	0	1
7		J	max	2	0.26	2	0	1
8		min	0	1	0.029	1	0	1
9	M3	I	max	1	54.047	1	0	1
10		min	-661.601	2	54.047	1	0	1
11		J	max	1	-54.047	1	0	1
12		min	-661.601	2	-54.047	1	0	1
13	CT	I	max	2	4.111	1	0	1
14		min	265.454	1	4.111	2	0	1
15		J	max	2	-4.111	1	0	1
16		min	265.454	1	-4.111	2	0	1

### Envelope Wood Code Checks

	Member	Shape	Code ...	Loc[ft]	LC	Shear ...	Loc[ft]	LC	Fc' [ksi]	Ft' [ksi]	Fb' [ksi]	Fv' [ksi]	RB	CL	CP	Eqn
1	M1	2x4	0.628	9.944	2	0.263	9.944	2	0.66	1.164	1.684	0.207	12.014	0.976	0.333	3.9-3
2	M2	2x4	0.987	6.757	2	0.263	10.071	2	0.66	1.164	1.721	0.207	4.32	0.998	0.333	3.9-3
3	M3	2x6	0.338	9	2	0.055	18	1	0.318	1.009	1.49	0.18	5.416	0.997	0.168	3.9-1
4	CT	2x6	0.211	4.101	2	0.004	4.101	1	0.447	1.009	1.472	0.18	10.967	0.985	0.235	3.6.3