

# Development Services

## From Concept to Construction

Phone: 503-823-7300 Email: [bds@portlandoregon.gov](mailto:bds@portlandoregon.gov) 1900 SW 4th Ave, Portland, OR 97201

More Contact Info (<http://www.portlandoregon.gov/bds/article/519984>)



### APPEAL SUMMARY

**Status:** Hold for Additional Information - Held over from ID 20220 (4/10/19) for more information

**Appeal ID:** 20395

**Project Address:** 1410 NW Johnson St

**Hearing Date:** 5/15/19

**Appellant Name:** Barry R Smith PC Architect

**Case No.:** B-006

**Appellant Phone:** 503-295-6261

**Appeal Type:** Building

**Plans Examiner/Inspector:** Preliminary

**Project Type:** commercial

**Stories:** 4 **Occupancy:** F-2 **Construction Type:** III-B

**Building/Business Name:**

**Fire Sprinklers:** Yes - NFPA 13 (Improvements Req'd)

**Appeal Involves:** Alteration of an existing structure, Reconsideration of appeal

**LUR or Permit Application No.:**

**Plan Submitted Option:** pdf [File 1] [File 2] [File 3] [File 4] [File 5]

**Proposed use:** Factory Industry - Low Hazard

### APPEAL INFORMATION SHEET

#### Appeal item 1

##### Code Section

Section 1022 Interior Exit Stairways and Ramps, 1022.3.1 Extension

##### Requires

Where interior exit stairways and ramps are extended to an exit discharge or a public way by an exit passageway, the interior exit stairway and ramp shall be separated from the exit passageway by a fire barrier constructed in accordance with Section 707 or a horizontal assembly constructed in accordance with Section 711, or both. The fire-resistance rating shall be at least equal to that required for the interior exit stairway and ramp. A fire door assembly complying with Section 716.5 shall be installed in the fire barrier to provide a means of egress from the interior exit stairway and ramp to the exit passageway. Openings in the fire barrier other than the fire door assembly are prohibited. Penetrations of the fire barrier are prohibited.

##### Proposed Design

This factory building was granted occupancy December 30, 1908 and little or no improvements have been made since the original construction. The current owner [Seller] has occupied the building since the 1950's using it as an office building and print shop.

Circulation and egress are constricted in the current configuration. Occupants have to travel through adjoin occupied spaces or through an enclosed stair to access tenant spaces. Door swing in the wrong direction and are redundant.

The new Owner [Purchaser] wishes to simplify the enclosed stair to act both as vertical circulation and means of egress as it now functions. The improvements are to secure the required two-hour fire resistive protection around the stairwell, correct the door swing and maneuvering distance condition and separate tenant access spaces by extending the stairwell footprint. (Fire Protection Engineer letters included for protection of existing heavy timber).

Per Section 1022.2, the fire-resistive rating of the Interior Exit Stairway is required to be 2 hour as the stair is connecting four stories.

Building is equipped with an automatic sprinkler system and needs upgrading to current NFPA 13 standards.

There are no combustible concealed attic spaces.

Where non-rated interior glass relite and doors are used, a 2HR rated fire curtain is provided (Tyco Model WS – 2HR Fire Barrier).

Stairwell protection will be extended to the basement.

RESPONSE: A Building Code appeal is required for substituting 2HR fire curtains in lieu of two-hour fire resistive construction.

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**Reason for alternative** The alternate gives the Owner flexibility to visually identify tenant access from egress components.

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APPEAL DECISION

**Extension of stair enclosures: Hold for Additional Information.**  
**Appellant may contact Corey Stanley (971 291-8919) with questions.**

1410 NW JOHNSON STREET

GENERAL NOTES:

1. CONSTRUCTION SHALL COMPLY WITH ALL CODES AS ADMINISTERED BY THE AUTHORITIES HAVING JURISDICTION. ALL WORK SHALL CONFORM TO ORDINANCES OR REGULATIONS RELATING TO ENVIRONMENTAL POLLUTION AND PRESERVATION OF NATURAL RESOURCES.
2. THE CONTRACTOR SHALL BE RESPONSIBLE FOR MAINTAINING ALL BURIED SERVICES IN UNDAMAGED CONDITION DURING CONSTRUCTION. CONTRACTOR SHALL VERIFY UTILITY LOCATIONS AND CONNECTIONS.
3. CONTRACTOR SHALL INSURE ALL SCAFFOLDING, TEMPORARY FLOORS, ETC., FURNISHED BY HIMSELF OR SUBCONTRACTORS FOR INSTALLATION OF WORK TO BE BUILT AND MAINTAINED TO SAFELY SUPPORT REQUIRED LOADS. COMPLY WITH ALL APPLICABLE LOCAL SAFETY CODES AND SPECIFICALLY THE OCCUPATIONAL SAFETY AND HEALTH ACT FOR THE CONSTRUCTION INDUSTRY.
4. PERFORM ALL WORK IN A FIRE-SAFE MANNER AND SUPPLY AND MAINTAIN ADEQUATE FIRST-AID AND FIRE FIGHTING EQUIPMENT CAPABLE OF EXTINGUISHING INCIPIENT FIRES. COMPLY WITH LOCAL AND STATE FIRE PREVENTION REGULATIONS.
5. PROVIDE ADEQUATE SAFETY AND PROTECTIVE DEVICES FOR WORKMEN DURING EXCAVATION AND CLEARING. REVIEW LOCATION OF EXISTING SERVICES AND UTILITY LINES. PROVIDE PROTECTIONS NECESSARY TO PREVENT DAMAGE TO EXISTING IMPROVEMENTS AND SURVEY MARKERS. PROVIDE EROSION CONTROL PER BUILDING DEPARTMENT REQUIREMENTS.
6. PROVIDE SHORING, SHEETING AND BRACING WHEREVER NECESSARY TO PREVENT CAVING DURING EXCAVATION OR TO PROTECT ADJACENT IMPROVEMENTS, PROPERTY, WORKMEN AND THE PUBLIC.
7. SOILS ENGINEER SHALL INSPECT AND APPROVE CUT-OUT FOR FOUNDATION AND FOUNDATION PLAN.
8. CONCRETE TESTING SHALL BE REQUIRED SEE STRUCTURAL GENERAL NOTES FOR TESTING REQUIREMENTS.
9. FURNISH AND PLACE HOLDDOWNS AND DEFORMED STEEL AS INDICATED BY THE STRUCTURAL ENGINEER. STRUCTURAL ENGINEER SHALL INSPECT ALL HOLDDOWNS AND STEEL FOR CONFORMANCE. CONTRACTOR SHALL PROVIDE UL RATINGS FOR RATED STEEL PROTECTION, SEE DRAWINGS FOR RATED REQUIREMENTS.
10. RAPIDLY HANDLE CONCRETE FROM MIXER TO FORMS AND DEPOSIT AS NEAR AS POSSIBLE TO ITS FINAL POSITION TO AVOID SEGREGATION DUE TO HANDLING. SEE STRUCTURAL FOR ADDITIONAL REQUIREMENTS.
11. EXAMINE DRAWINGS FOR REQUIRED ROUGH CARPENTRY MATERIALS INCLUDING PLATES, STUDS, FIRE-STOPS, SOLID BLOCKING, BRIDGING, POSTS, BLOCKS, SUB-FLOORING AND SHEATHING. LUMBER SHALL BE DOUGLAS-FIR (STANDARD), TREATED LUMBER WITH A NET RETENTION OF 0.25 PCF. GYPSUM BOARD SHALL BE AS NOTED ON DRAWINGS. USE EXTERIOR GYPSUM BOARD FOR SOFFITS AND PORCH CEILINGS AND WATERPROOF IN BATHROOMS. PROVIDE ALL GLUE LAMINATED MEMBERS AS INDICATED BY STRUCTURAL. BUILDING PAPER SHALL BE NO. 15 LB. ASPHALT SATURATED ROOFING FELT. ALL HANGERS AND HOLDDOWNS SHALL BE HOT DIPPED GALVANIZED. USE KRAFT FACE FIBERGLASS INSULATION; SEE ENERGY CODE COMPLIANCE. I-JOISTS BY TRUSS JOIST CORPORATION SHALL HAVE HOLES KNOCKED OUT AT FACTORY. INSTALL WITH HOLES UP. SIZE AND DETAILS OF JOISTS SHALL FIT DIMENSIONS AND LOADS AS INDICATED ON DRAWINGS.
12. ALL MANUFACTURED MATERIALS, COMPONENTS, FASTENERS, ASSEMBLIES, ECT., SHALL BE HANDLED AND INSTALLED IN ACCORDANCE WITH THE MANUFACTURER'S INSTRUCTIONS AND PROVISIONS OF APPLICABLE ICBO RESEARCH RECOMMENDATIONS.
13. PROVIDE SHOP DRAWINGS FOR ALL PRE-ENGINEERED PRODUCTS (I-JOISTS, ROOF TRUSSES, ETC.) FOR STRUCTURAL REVIEW.
14. IMMEDIATELY NOTIFY ARCHITECT IN WRITING OF ANY DISREPINCIES BETWEEN CONSTRUCTION DOCUMENTS AND ACTUAL CONDITIONS. CORRECTIONS SHALL BE THE RESPONSIBILITY OF THE OWNER/CONTRACTOR.
15. MECHANICAL AND ELECTRICAL SYSTEMS SHALL BE BIDDER DESIGNED AND UNDER SEPARATE PERMIT. CONTRACTOR SHALL PROVIDE ALL REQUISITE SYSTEM DESIGN DOCUMENTS, LOAD CALCULATIONS AND SHOP DRAWINGS REQUIRED FOR REVIEW.

PROJECT DESCRIPTION

THE PROJECT IS TO HARDEN THE EXISTING EXIT STAIR SYSTEM WHILE EXPANDING THE FIRST FLOOR LOBBY AREA FOR TENANT ACCESS. HARDENING TO SOME EXTENT OCCURS ON ALL FLOORS. ADD ADA BATHROOMS TO UPPER THIRD FLOOR. BRING EXISTING AUTOMATIC SPRINKLER SYSTEM UP TO NFPA13 STANDARDS. PAINT AND REPAIR EXISTING EXTERIOR FIRE ESCAPE AND ASSOCIATED ELEMENTS.

PROPERTY:

SITE ADDRESS:

1410 NW JOHNSON STREET  
PORTLAND, OREGON 97209

PROPERTY ID:

R140740

STATE ID:

1N1E33AD 2000

NEW STATE ID:

1N1E33AD -02000

ALT ACCOUNT #:

R180211050

MAP #:

2928 OLD

OWNER/DEVELOPER:

GANN BUILDING LLC  
1410 NW JOHNSON STREET  
PORTLAND OREGON 97209  
contact: MARTIN KEHOE

PH: 503.244.3838  
FAX: N/A  
EM: mkehoe03@gmail.com

BARRY R. SMITH, PC, ARCHITECT  
715 SW MORRISON STREET, SUITE 909  
PORTLAND, OREGON 97205-3105  
contact: BARRY SMITH

PH: 503.295.6261  
FAX: N/A  
EM: barry@barryrsmith.com

SEPARATE PERMITS REQUIRED

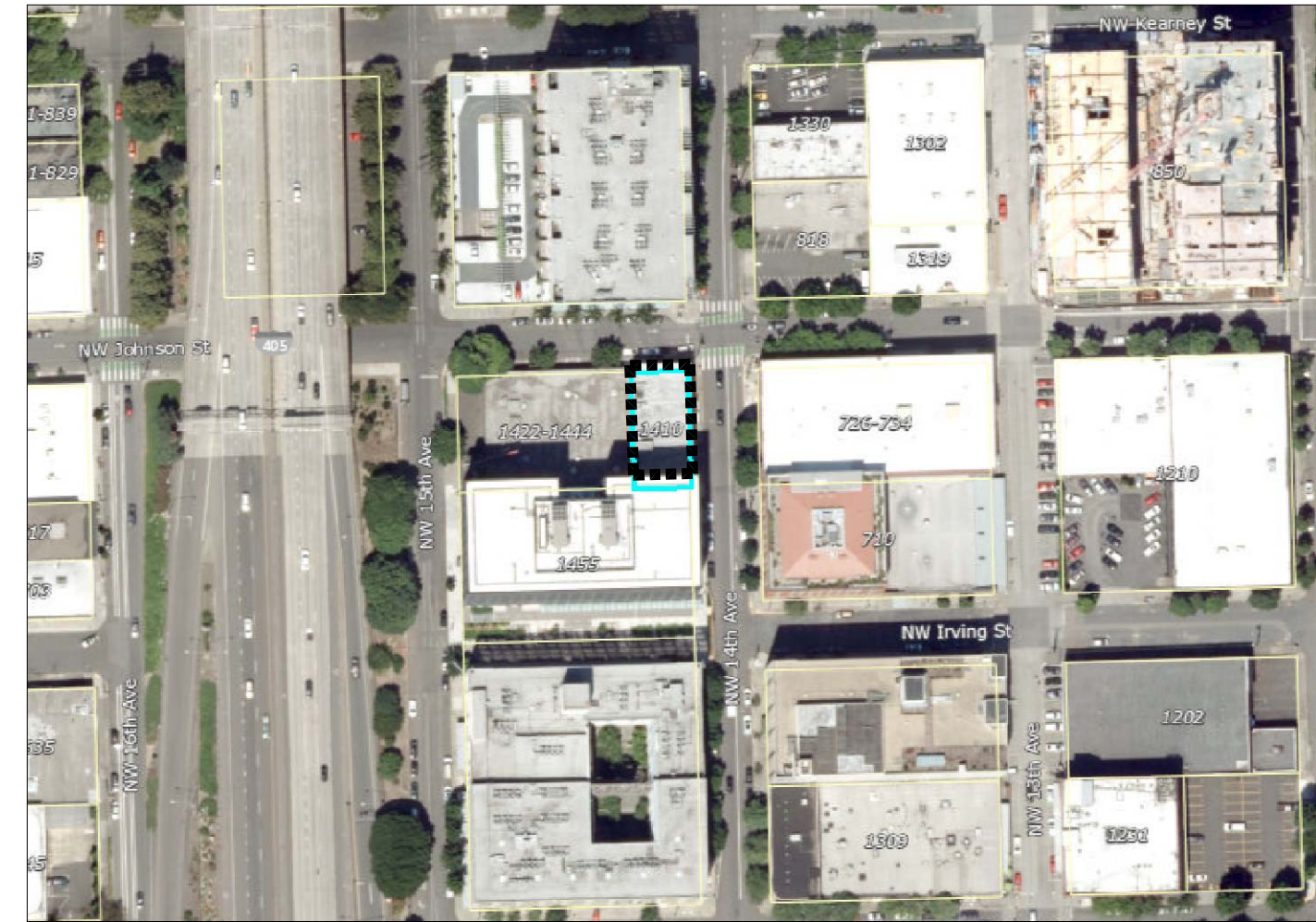
1. MECHANICAL PLANS
2. ELECTRICAL PLANS
3. PLUMBING PLANS

CODE APPEALS

PENDING - ID#18949

DRAWING INDEX:

- ARCHITECTURAL
- A0.0 TITLE SHEET + SITE PLAN
- A0.1 BUILDING CODE ANALYSIS - SUMMARY
- A0.2 BUILDING CODE ANALYSIS - HARDENING PLANS
- A0.3 BUILDING CODE ANALYSIS - HARDENING PLANS
- A1.0 EXISTING CONDITION PLANS
- A2.0 DEMOLITION PLANS
- A3.0 HARDENING PLANS + DOOR SCHEDULE
- A3.1 ENLARGED HARDENING PLANS + RATED DETAILS
- A5.0 EXTERIOR ELEVATIONS
- STRUCTURAL
- S1 PLANS
- S2 DETAILS



76 SITE PLAN  
A0.0 SCALE: 1:10



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1410 NW JOHNSON STREET  
for GANN BUILDING LLC  
TITLE SHEET & SITE PLAN

PERMIT SET

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A0.0  
05.09.2019





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1410 NW JOHNSON STREET

for GANN BUILDING LLC

BUILDING CODE ANALYSIS - FLOOR PLANS

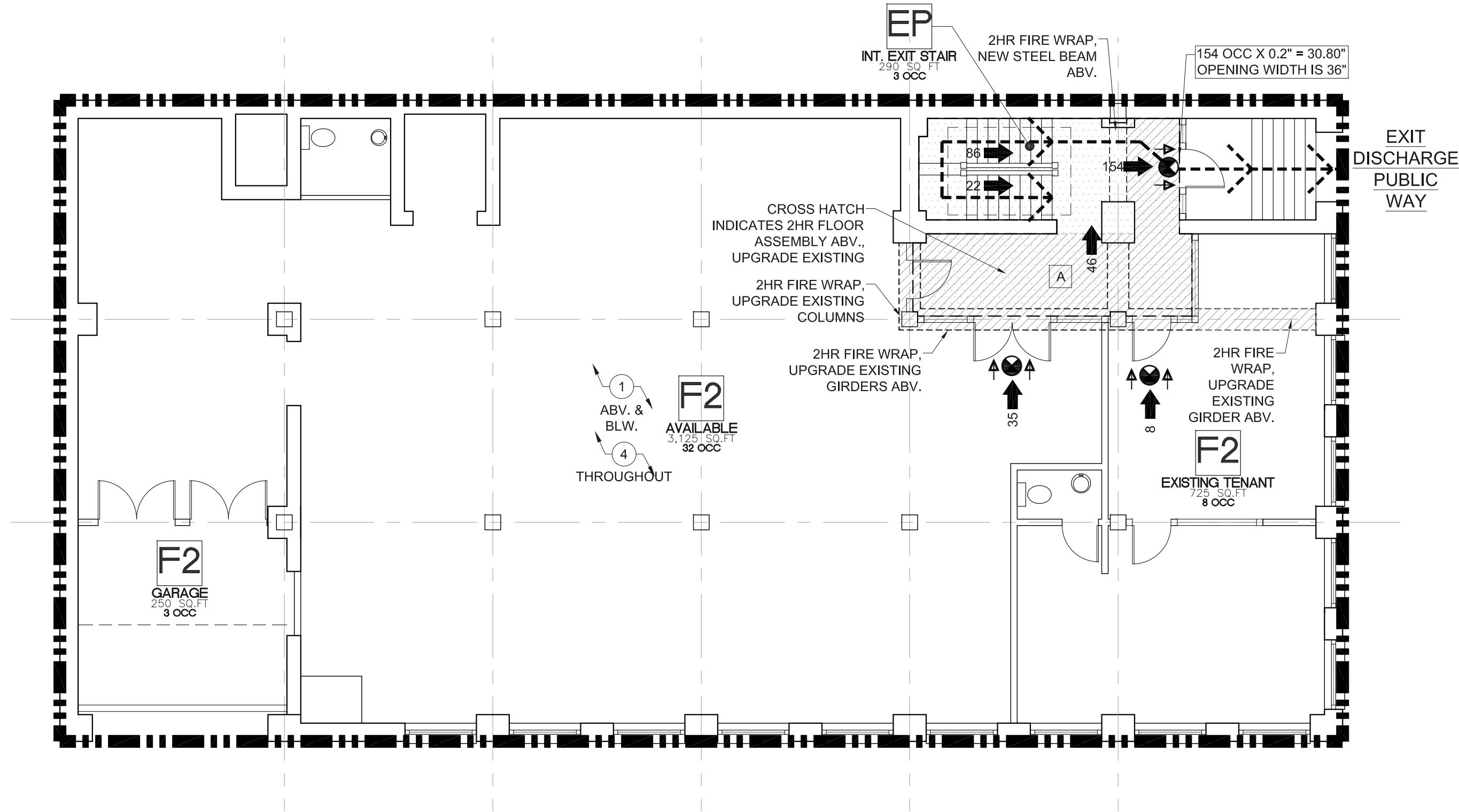
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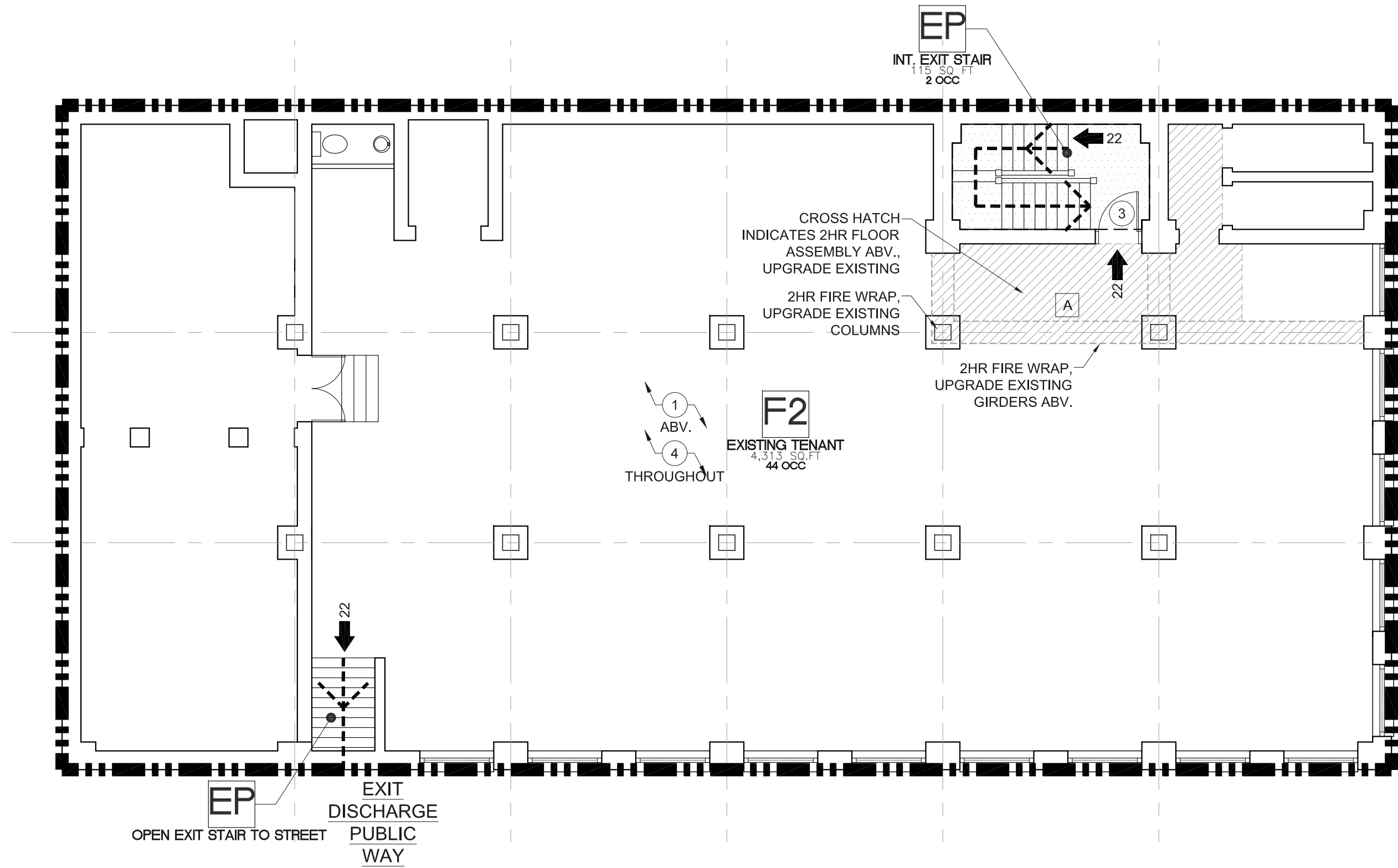
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OCCUPANCY SEPARATION	
FIRST FLOOR - 5,000 GROSS SQ. FT. 46 TOTAL OCCUPANT LOAD ALLOWED	
F2	4,100 SQ. FT. - 43 OCCUPANTS FACTORY OCCUPANIES INCLUDE THE USE OF A BUILDING OR STRUCTURE OR PORTION THEROF, FOR LOW-HAZARD FACTORY INDUSTRIAL 100 GROSS SF ALLOWANCE PER OCCUPANT.
EP	290 SQ. FT. - 3 OCCUPANTS EXIT STAIR ENCLOSURE OR EXIT PASSAGEWAY: BOTH WITH OPENING, DUCT, PENETRATION, AND JOINT PROTECTION. SEE WALL TYPES AND JOINT DETAILS, DOOR AND WINDOW SCHEDULES, PENETRATION DETAILS, AND MECHANICAL DRAWINGS. (PART OF FACTORY OCCUPANCY DESIGNATION AND CALCULATED AS PART OF IT FOR BUILDING AREA CALCULATION PURPOSES.) 100 GROSS SF ALLOWANCE PER OCCUPANT.



63  
A0.2  
BUILDING CODE ANALYSIS - FIRST FLOOR PLAN  
SCALE: 1/8" = 1'-0"  
SEE HARDENING PLANS ON A3.0 FOR FURTHER INFORMATION

OCCUPANCY SEPARATION	
BASEMENT FLOOR - 5,000 GROSS SQ. FT. 46 TOTAL OCCUPANT LOAD ALLOWED	
F2	4,313 SQ. FT. - 44 OCCUPANTS FACTORY OCCUPANIES INCLUDE THE USE OF A BUILDING OR STRUCTURE OR PORTION THEROF, FOR LOW-HAZARD FACTORY INDUSTRIAL 100 GROSS SF ALLOWANCE PER OCCUPANT.
EP	115 SQ. FT. - 2 OCCUPANTS EXIT STAIR ENCLOSURE OR EXIT PASSAGEWAY: BOTH WITH OPENING, DUCT, PENETRATION, AND JOINT PROTECTION. SEE WALL TYPES AND JOINT DETAILS, DOOR AND WINDOW SCHEDULES, PENETRATION DETAILS, AND MECHANICAL DRAWINGS. (PART OF FACTORY OCCUPANCY DESIGNATION AND CALCULATED AS PART OF IT FOR BUILDING AREA CALCULATION PURPOSES.) 100 GROSS SF ALLOWANCE PER OCCUPANT.



66  
A0.2  
BUILDING CODE ANALYSIS - BASEMENT FLOOR PLAN  
SCALE: 1/8" = 1'-0"  
SEE HARDENING PLANS ON A3.0 FOR FURTHER INFORMATION

BUILDING CODE ANALYSIS	
KEY NOTES	
<b>WALL ASSEMBLIES:</b> SEE LEGEND BELOW FOR FIRE-RATED WALLS.	
<b>FLOOR / ROOF ASSEMBLIES:</b>	
①	0-HOUR HORIZONTAL FLOOR/CEILING ASSEMBLY (TABLE 601)
②	0-HOUR ROOF ASSEMBLY (TABLE 601)
<b>OPENING PROTECTION:</b>	
③	90 MIN. DOOR @ 2-HR INTERIOR EXIT STAIRWAYS (TABLE 716.5)
<b>FIRE PROTECTION:</b>	
④	BUILDING IS EQUIPPED THROUGHOUT WITH AN AUTOMATIC SPRINKLER SYSTEM IN ACCORDANCE WITH NFPA 13. (903.3.1.1)
GENERAL NOTES	
<ul style="list-style-type: none"><li>THIS CODE ANALYSIS PLAN IS FOR REFERENCE ONLY. SEE ALL OTHER PLAN SHEETS FOR CONTRACT DOCUMENT INFORMATION. THIS CODE ANALYSIS IDENTIFIES SOME SPECIFIC BUILDING CODE REQUIREMENTS BUT IS NOT INTENDED TO LIST ALL BUILDING CODE REQUIREMENTS.</li><li>SEE OTHER PLANS AND DETAIL SHEETS FOR ACCESSIBILITY CONFORMANCE.</li></ul>	
LEGEND	
	INDICATES EMERGENCY EGRESS PATH @ A MINIMUM OF 1 FOOT-CANDLE. SEE SHEET LIGHTING PLANS FOR EXTERIOR LIGHTING REQUIREMENTS. LIGHTING LEVELS ARE PER ALL APPLICABLE FIRE/LIFE/SAFETY CODES.
	2-HOUR FIRE BARRIER & EXTERIOR WALL (705 & 707)
	NON-RATED WALL (TABLE 601)
	EXIT DISCHARGE
	NUMBER AND DIRECTION OF OCCUPANTS FROM THE SPACE.
APPEALS	
PENDING	



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PORTLAND, OR

1410 NW JOHNSON STREET

for GANN BUILDING LLC

BUILDING CODE ANALYSIS - FLOOR PLANS

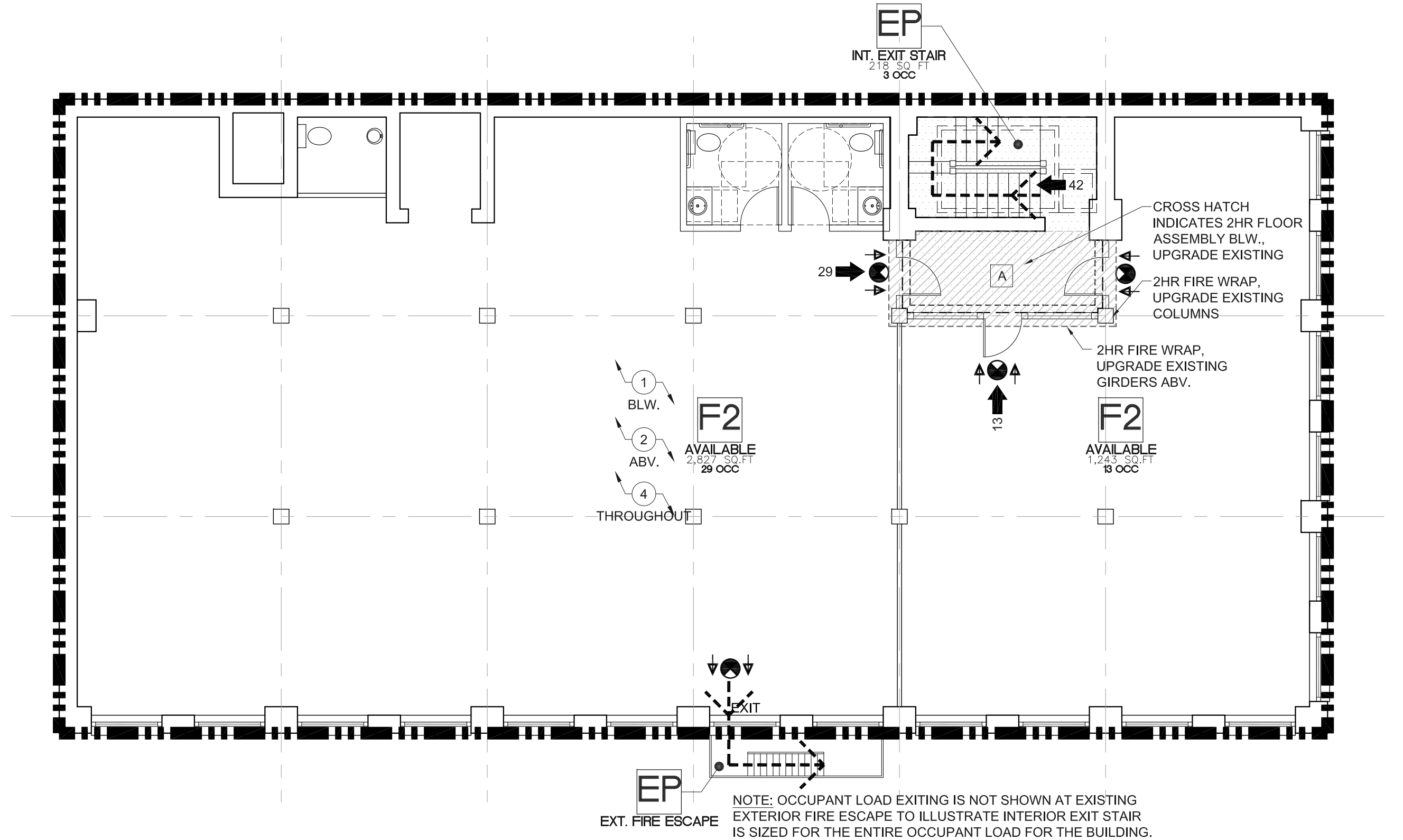
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OCCUPANCY SEPARATION	
THIRD FLOOR - 5,000 GROSS SQ. FT. 45 TOTAL OCCUPANT LOAD ALLOWED	
F2	4,103 SQ. FT. - 42 OCCUPANTS FACTORY OCCUPANCIES INCLUDE THE USE OF A BUILDING OR STRUCTURE OR PORTION THEREOF, FOR LOW-HAZARD FACTORY INDUSTRIAL 100 GROSS SF ALLOWANCE PER OCCUPANT.
EP	218 SQ. FT. - 3 OCCUPANTS EXIT STAIR ENCLOSURE OR EXIT PASSAGEWAY: BOTH WITH OPENING, DUCT, PENETRATION, AND JOINT PROTECTION. SEE WALL TYPES AND JOINT DETAILS, DOOR AND WINDOW SCHEDULES, PENETRATION DETAILS, AND MECHANICAL DRAWINGS. (PART OF FACTORY OCCUPANCY DESIGNATION AND CALCULATED AS PART OF IT FOR BUILDING AREA CALCULATION PURPOSES.) 100 GROSS SF ALLOWANCE PER OCCUPANT.



63  
A0.3

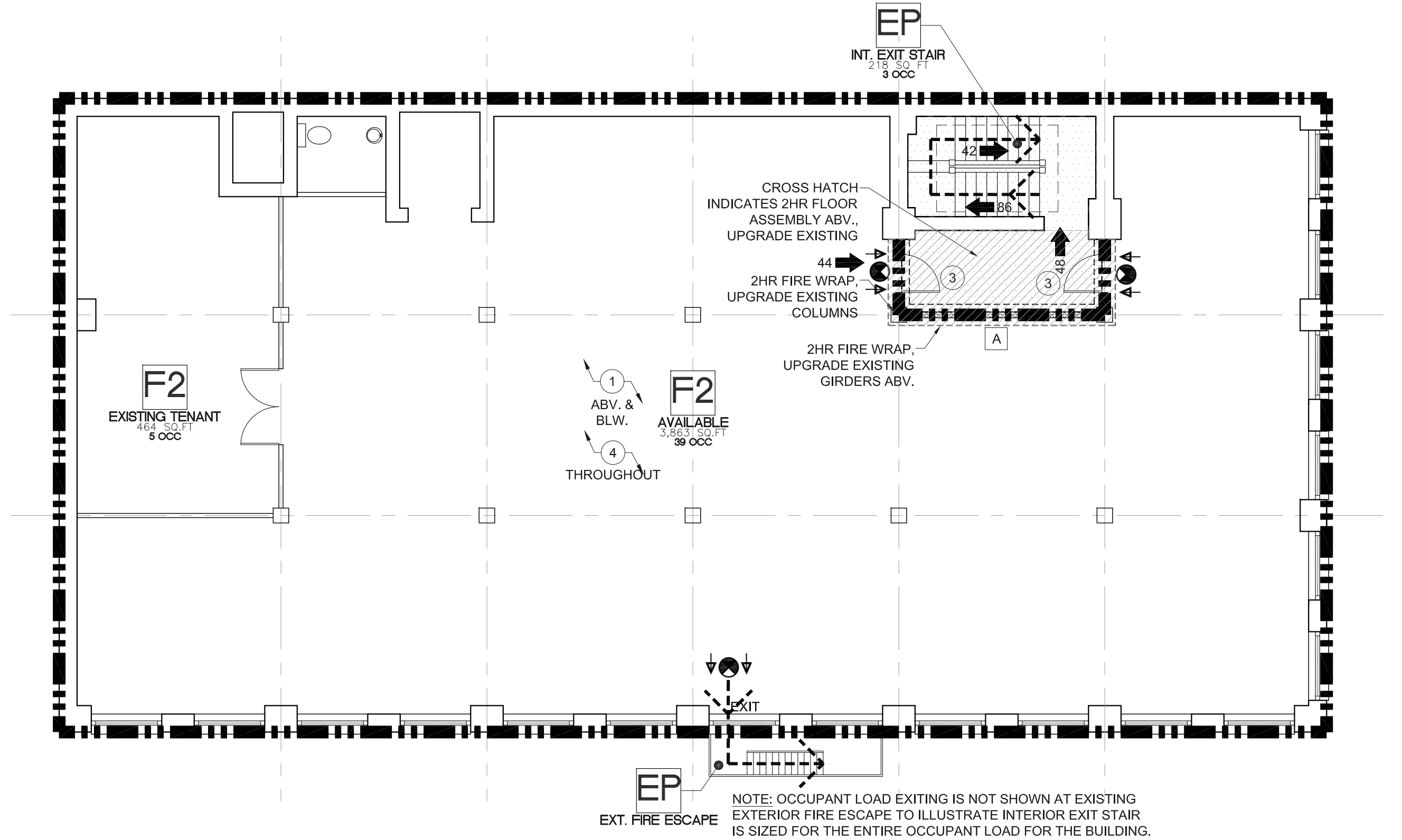
### BUILDING CODE ANALYSIS - THIRD FLOOR PLAN

SCALE: 1/8" = 1'-0"

SEE HARDENING PLANS ON A3.0 FOR FURTHER INFORMATION



OCCUPANCY SEPARATION	
SECOND FLOOR - 5,000 GROSS SQ. FT. 48 TOTAL OCCUPANT LOAD ALLOWED	
F2	4,358 SQ. FT. - 45 OCCUPANTS FACTORY OCCUPANCIES INCLUDE THE USE OF A BUILDING OR STRUCTURE OR PORTION THEREOF, FOR LOW-HAZARD FACTORY INDUSTRIAL 100 GROSS SF ALLOWANCE PER OCCUPANT.
EP	218 SQ. FT. - 3 OCCUPANTS EXIT STAIR ENCLOSURE OR EXIT PASSAGEWAY: BOTH WITH OPENING, DUCT, PENETRATION, AND JOINT PROTECTION. SEE WALL TYPES AND JOINT DETAILS, DOOR AND WINDOW SCHEDULES, PENETRATION DETAILS, AND MECHANICAL DRAWINGS. (PART OF FACTORY OCCUPANCY DESIGNATION AND CALCULATED AS PART OF IT FOR BUILDING AREA CALCULATION PURPOSES.) 100 GROSS SF ALLOWANCE PER OCCUPANT.



66  
A0.3

### BUILDING CODE ANALYSIS - SECOND FLOOR PLAN

SCALE: 1/8" = 1'-0"

SEE HARDENING PLANS ON A3.0 FOR FURTHER INFORMATION



BUILDING CODE ANALYSIS	
KEY NOTES	
<b>WALL ASSEMBLIES:</b> SEE LEGEND BELOW FOR FIRE-RATED WALLS.	
<b>FLOOR / ROOF ASSEMBLIES:</b> ① 0-HOUR HORIZONTAL FLOOR/CEILING ASSEMBLY (TABLE 601) ② 0-HOUR ROOF ASSEMBLY (TABLE 601)	
<b>OPENING PROTECTION:</b> ③ 90 MIN. DOOR @ 2-HR INTERIOR EXIT STAIRWAYS (TABLE 716.5)	
<b>FIRE PROTECTION:</b> ④ BUILDING IS EQUIPPED THROUGHOUT WITH AN AUTOMATIC SPRINKLER SYSTEM IN ACCORDANCE WITH NFPA 13. (903.3.1.1)	
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	2-HOUR FIRE BARRIER & EXTERIOR WALL (705 & 707)
	NON-RATED WALL (TABLE 601)
	EXIT DISCHARGE
	NUMBER AND DIRECTION OF OCCUPANTS FROM THE SPACE.
APPEALS	
PENDING	

80

70

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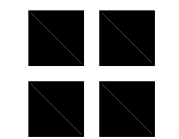
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PORTLAND, OR

1410 NW JOHNSON STREET  
for GANN BUILDING LLC  
EXISTING CONDITIONS PLANS

PERMIT SET

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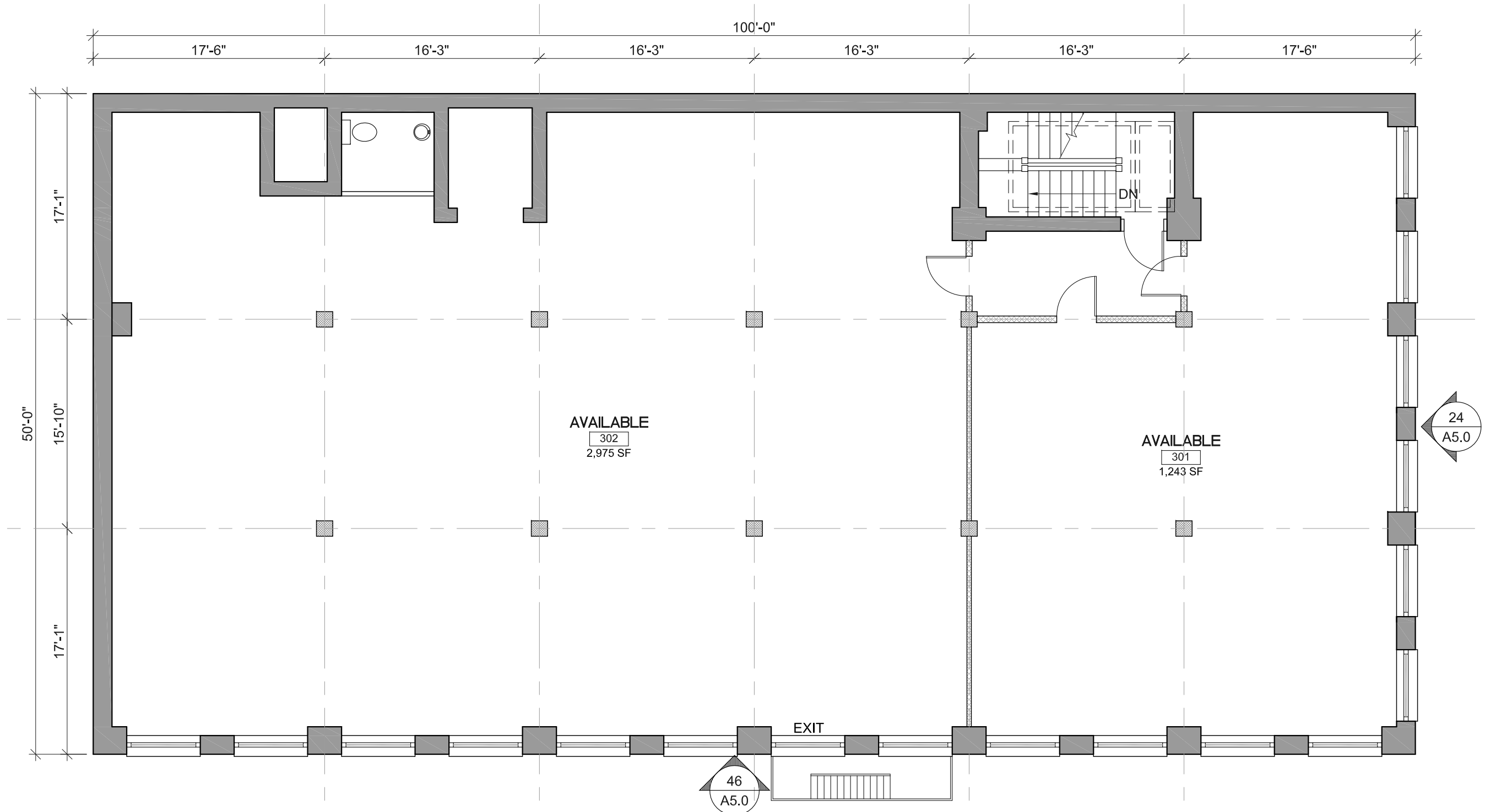
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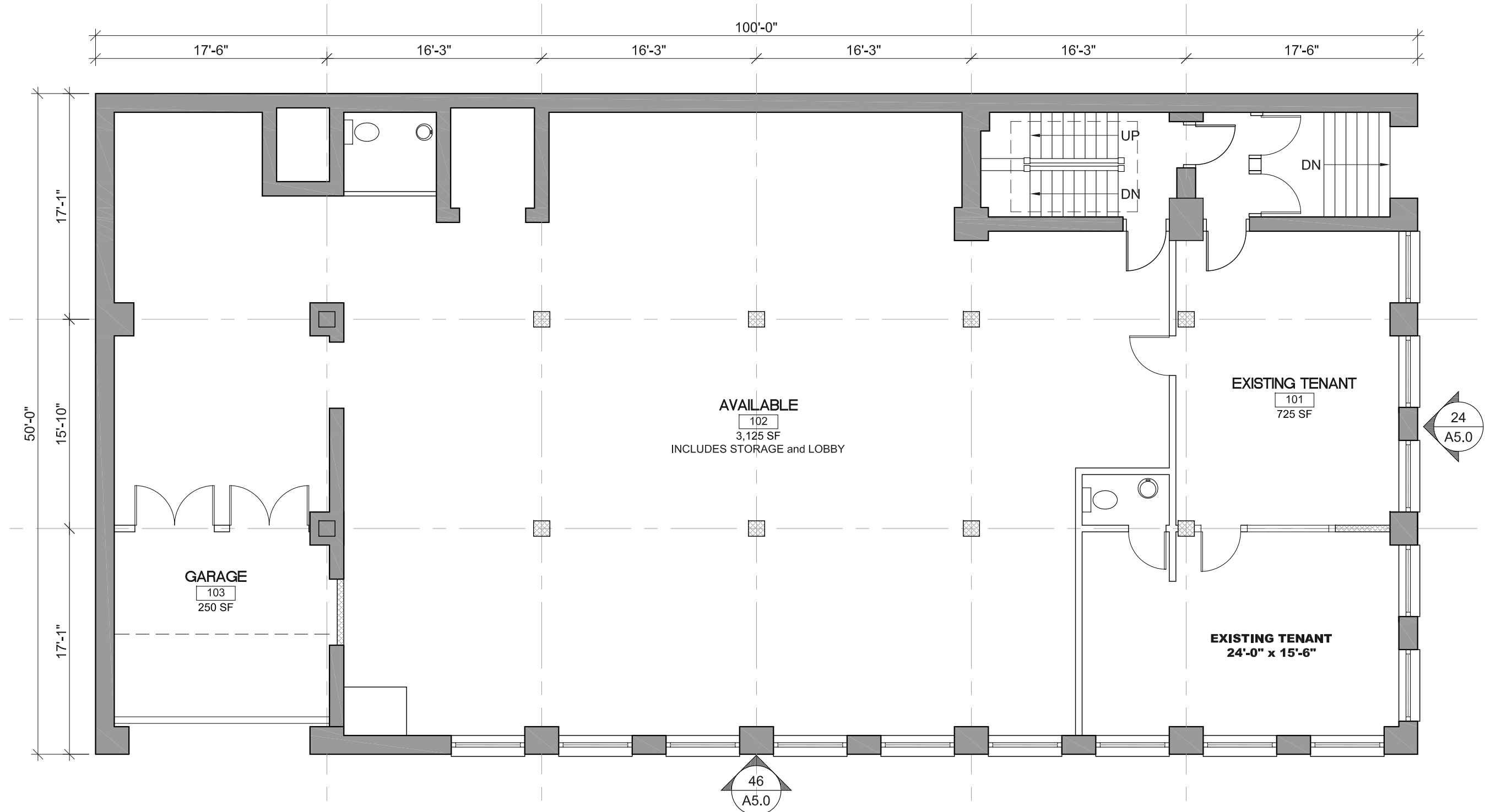
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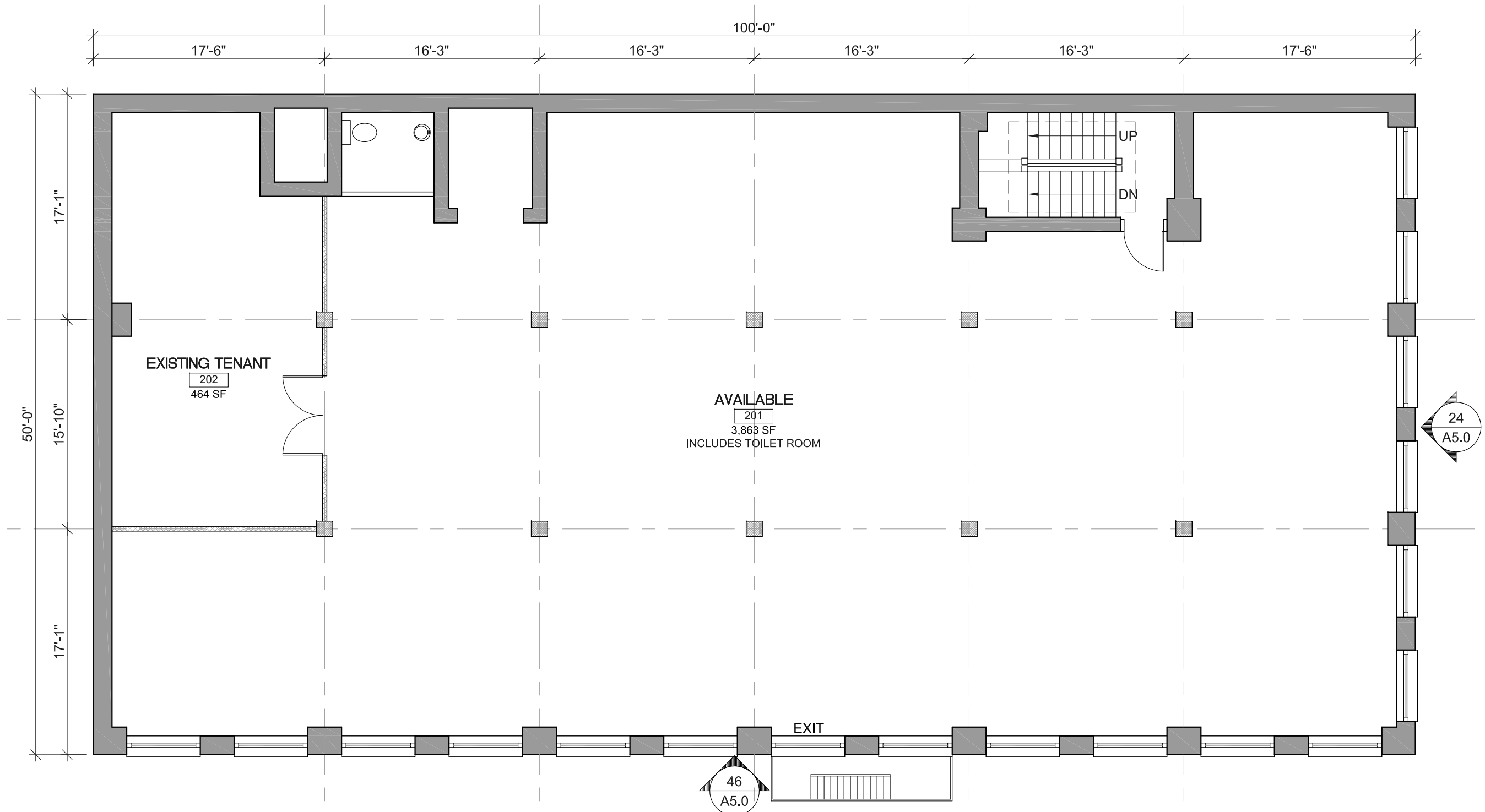
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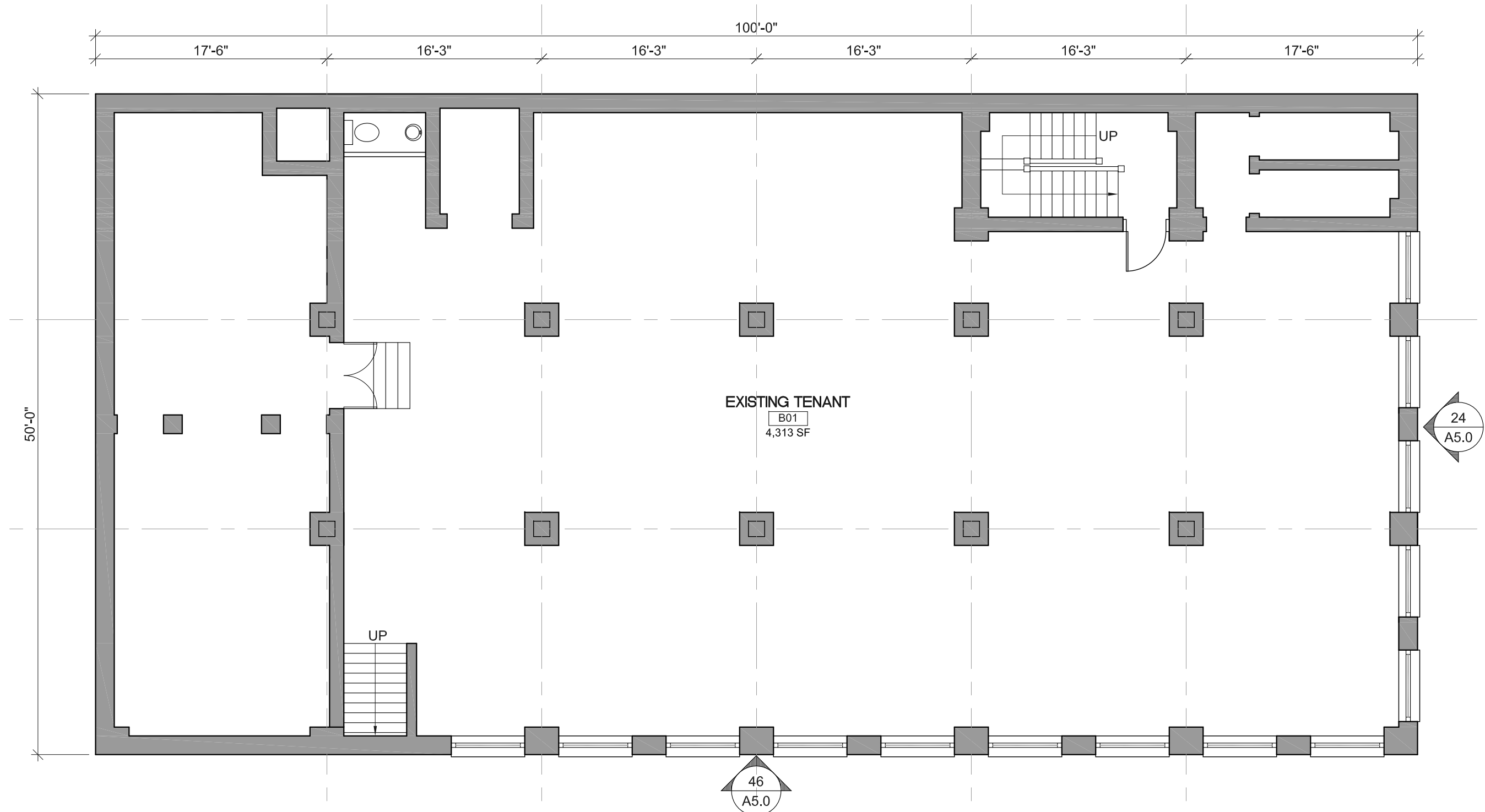
**84 THIRD FLOOR PLAN**  
SCALE: 1/8" = 1'-0" **5,000 SF GROSS** NORTH



**44 FIRST FLOOR PLAN**  
SCALE: 1/8" = 1'-0" **5,000 SF GROSS** NORTH



**86 SECOND FLOOR PLAN**  
SCALE: 1/8" = 1'-0" **5,000 SF GROSS** NORTH



**46 BASEMENT FLOOR PLAN**  
SCALE: 1/8" = 1'-0" **5,000 SF GROSS** NORTH

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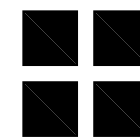
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PORTLAND OR 97205 503.295.6261 www.barryremith.com



PORTLAND, OR

1410 NW JOHNSON STREET

for GANN BUILDING LLC

DEMOLITION PLANS

PERMIT SET

PLL1410NWJ - 02

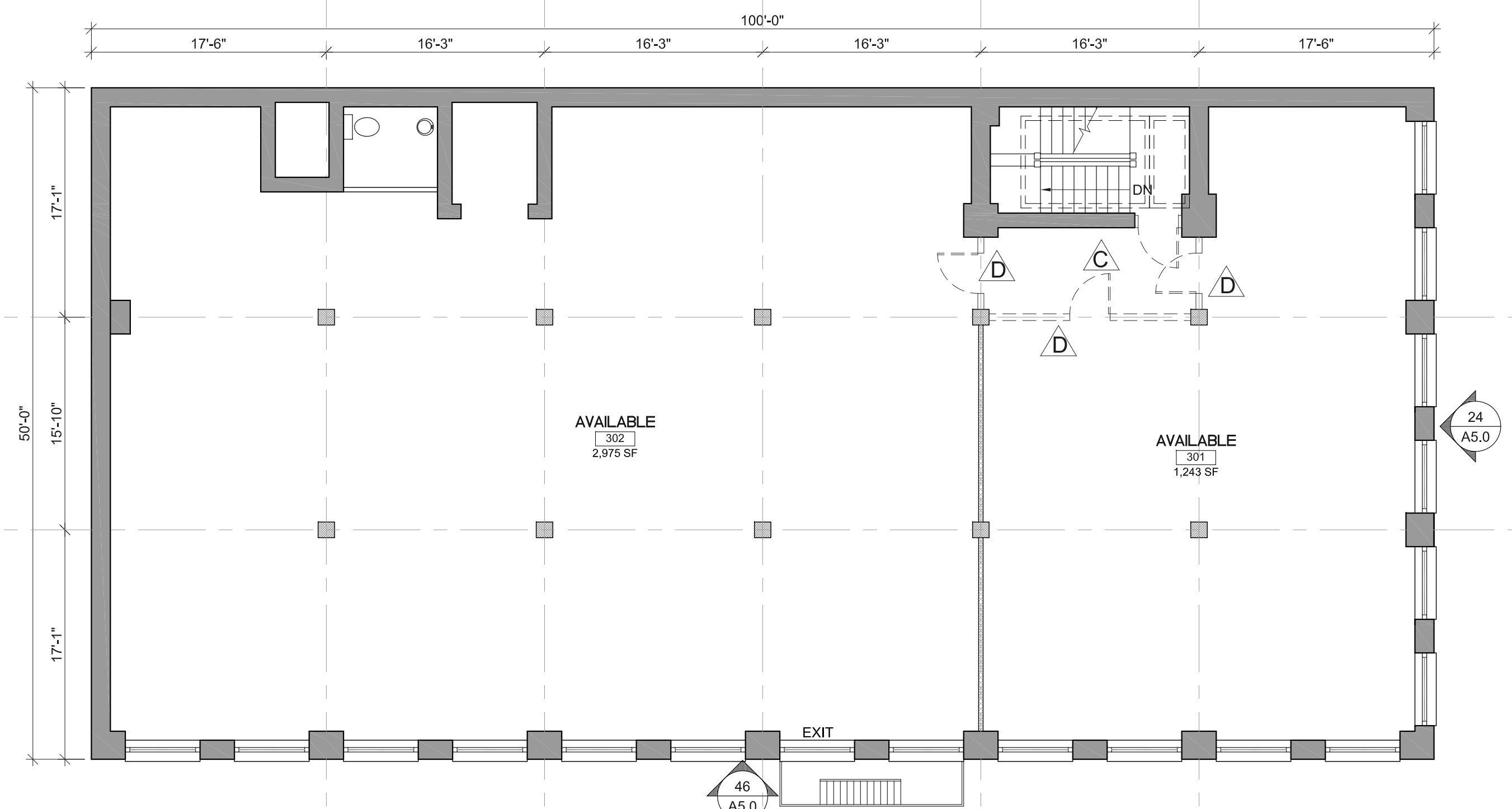
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DEMOLITION SCHEDULE

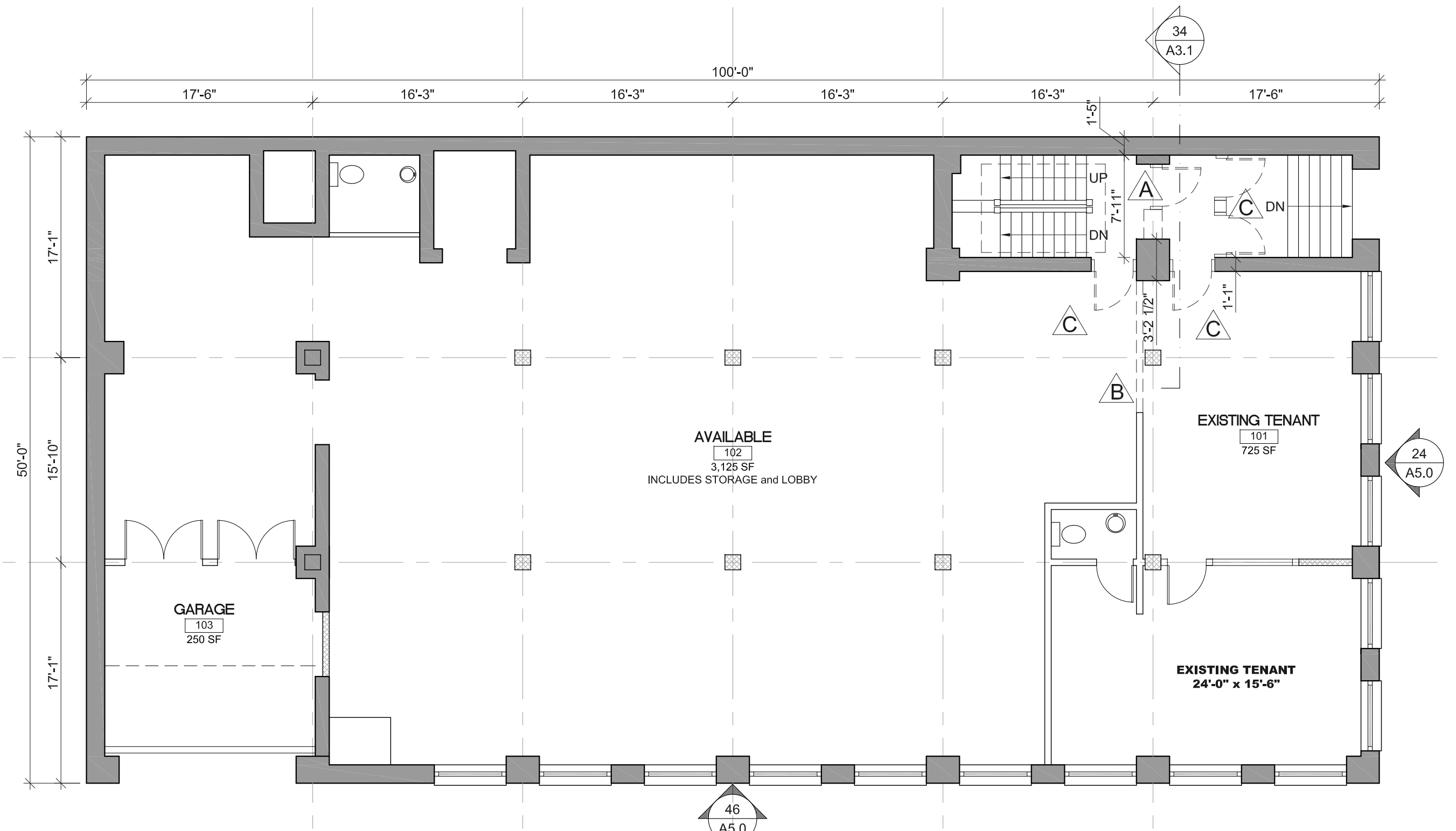
- A** REMOVE EXISTING DOORS AND BRICK STEM WALL.  
PROVIDE BRACING AS REQ'D BY STRUCTURAL.
- B** REMOVE PORTION OF NON-LOAD BEARING WOOD PARTITION.
- C** REMOVE EXISTING NON-RATED DOORS AND FRAMES.
- D** REMOVE EXISTING NON-RATED WOOD PARTITION WALLS.

- NOTES:
- DRAWINGS BASED ON ASBUILT PLANS.
  - CONTRACTOR TO FIELD VERIFY ALL DIMENSIONS.



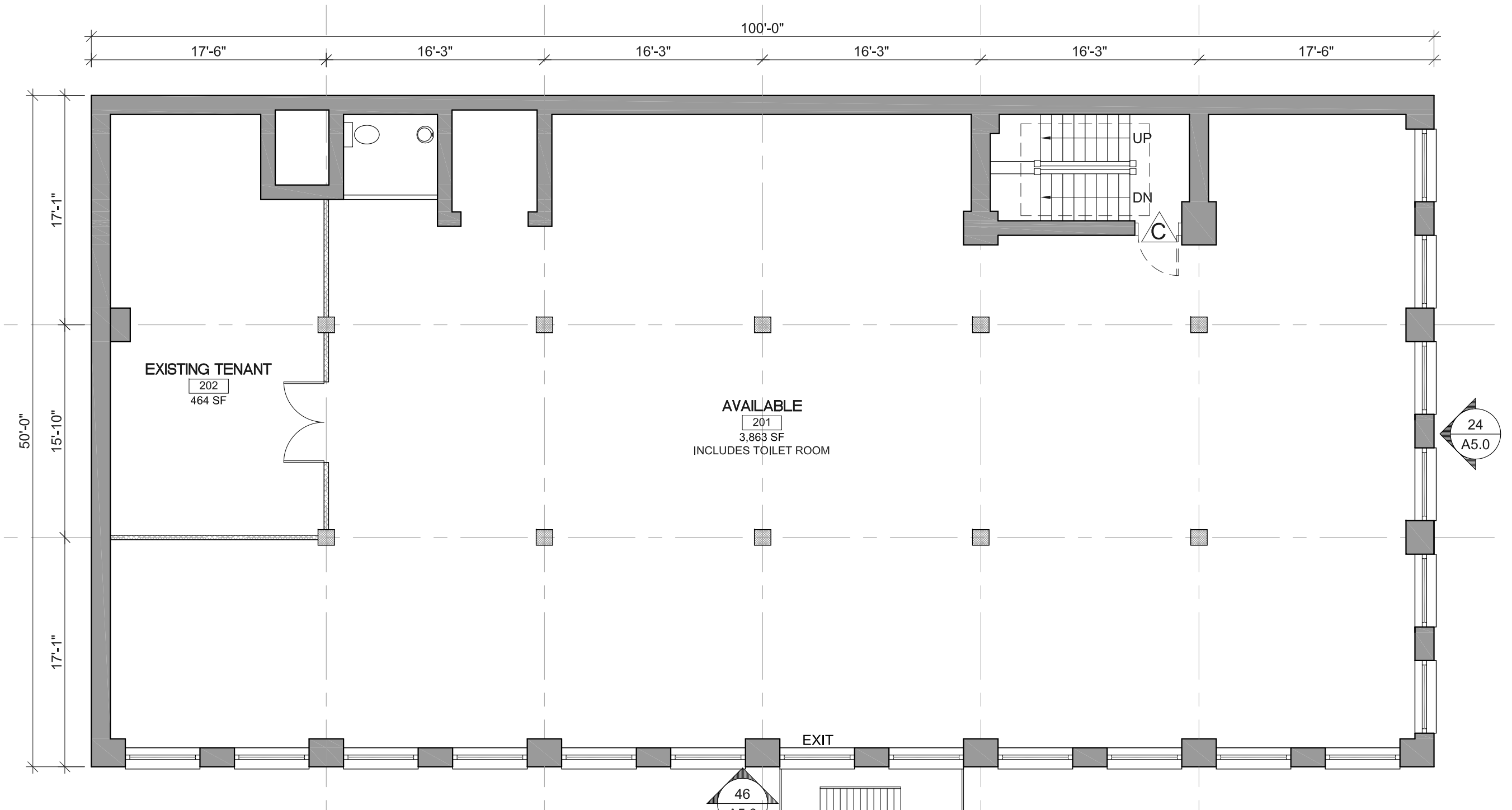
84 THIRD FLOOR DEMO PLAN

A2.0 SCALE: 1/8" = 1'-0"



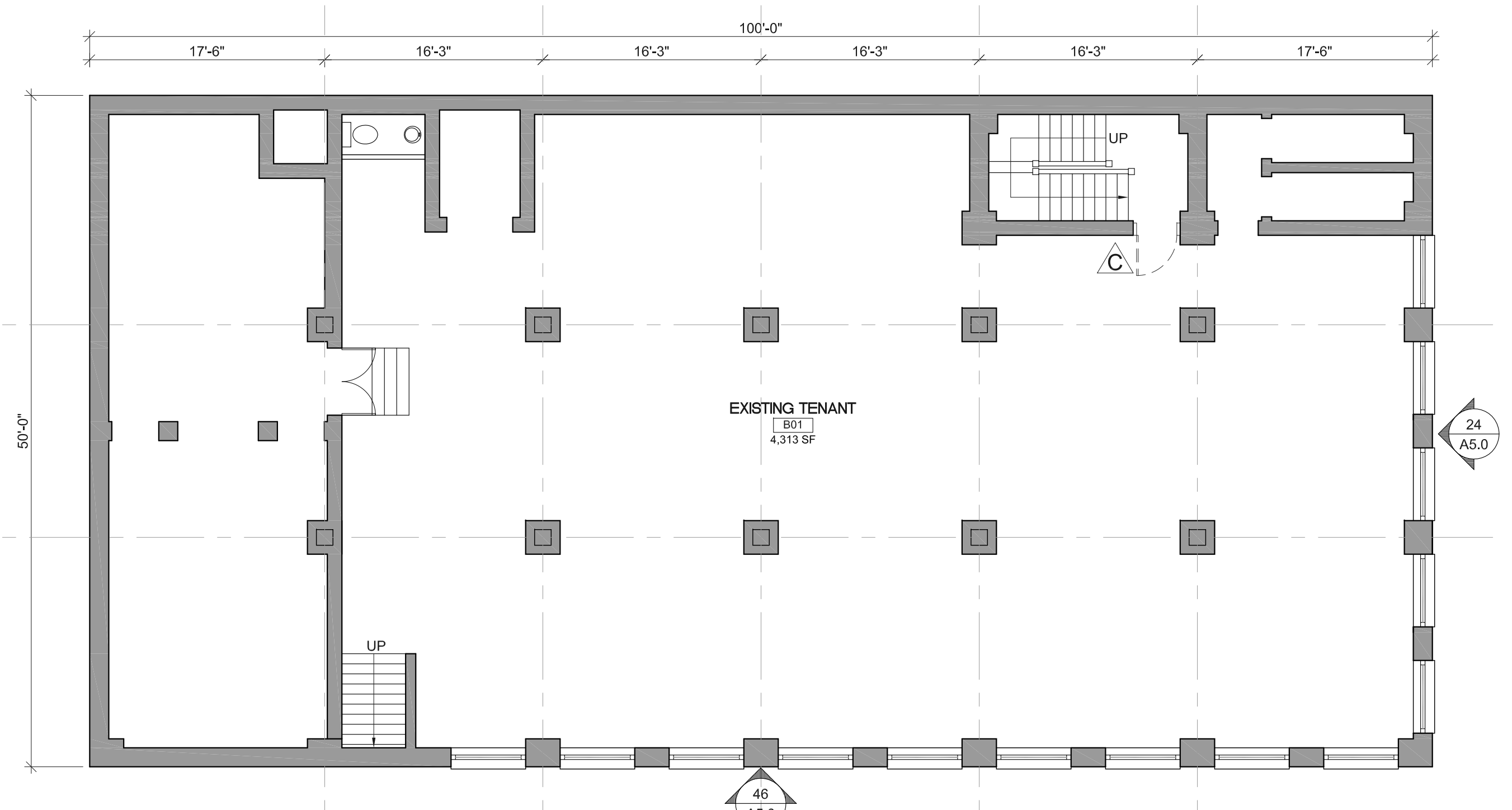
44 FIRST FLOOR DEMO PLAN

A2.0 SCALE: 1/8" = 1'-0"



86 SECOND FLOOR DEMO PLAN

A2.0 SCALE: 1/8" = 1'-0"

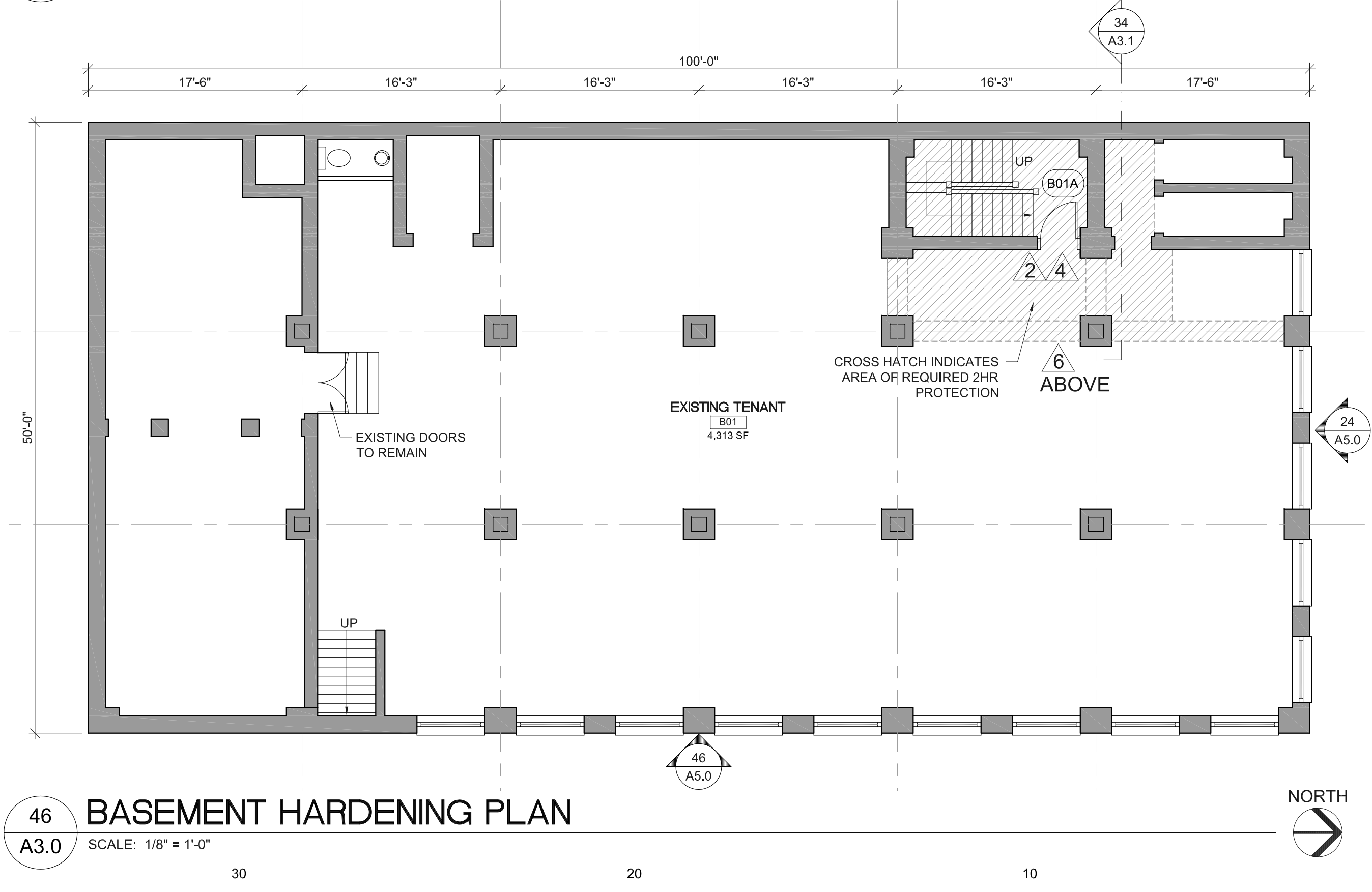
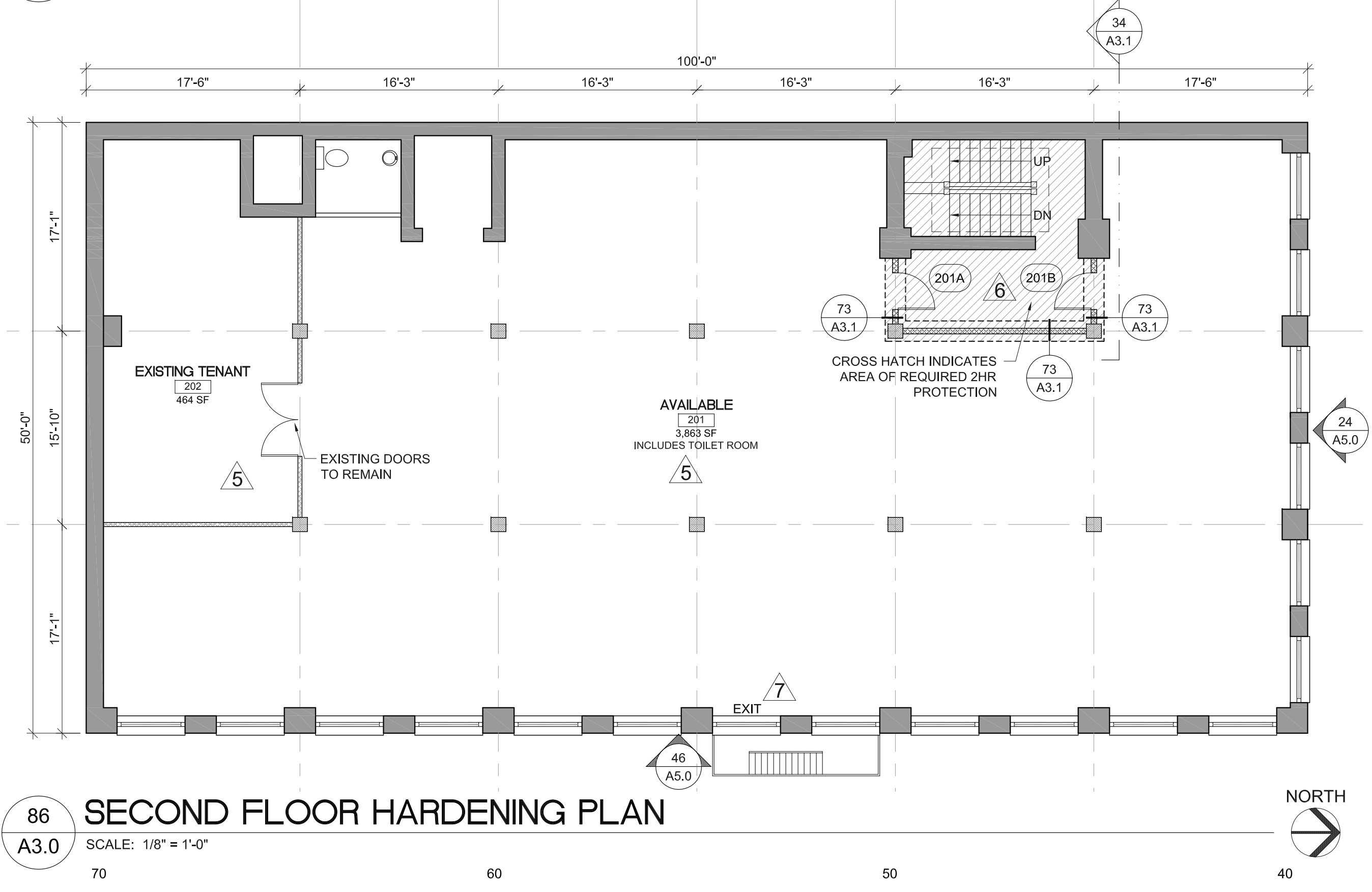
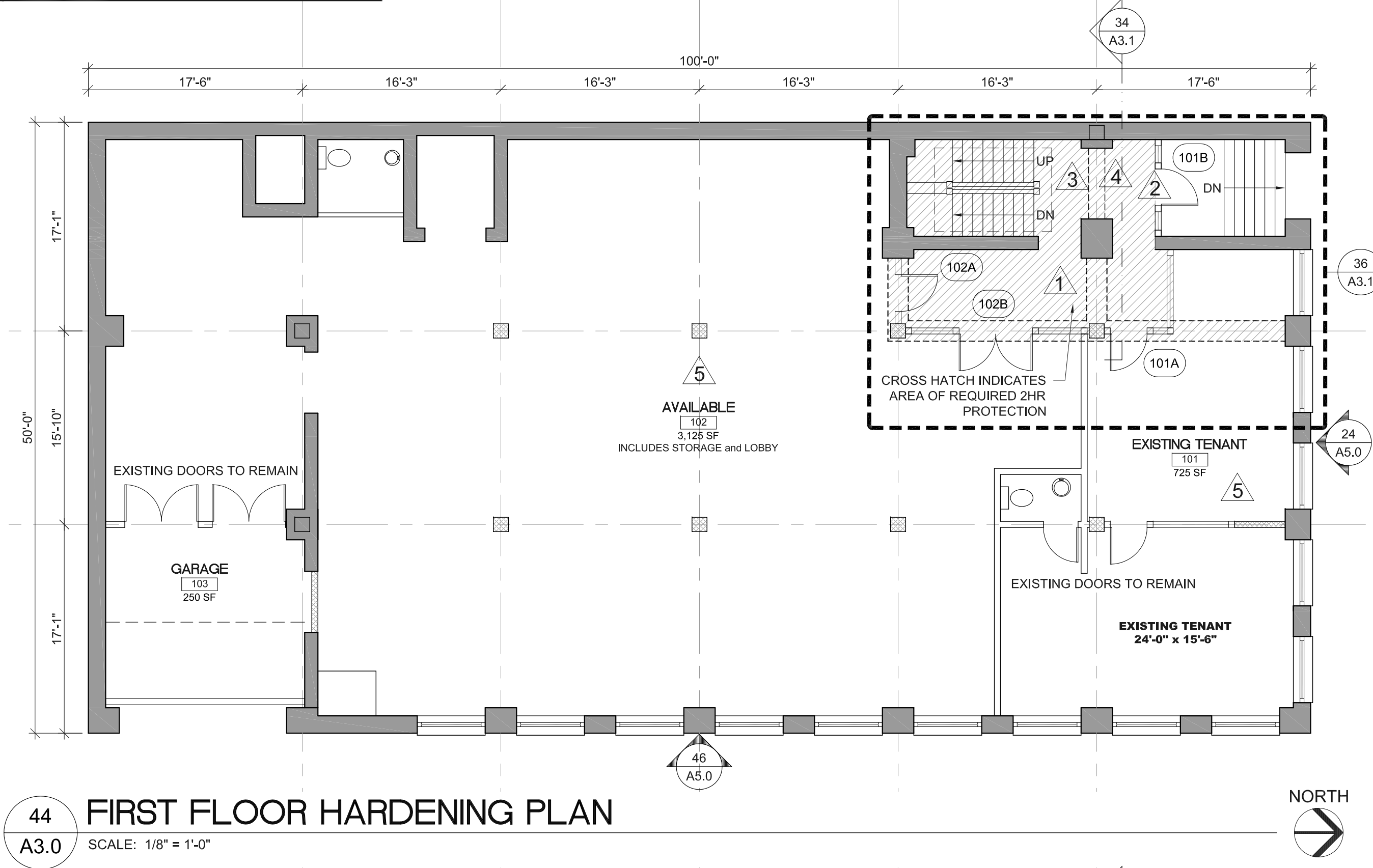
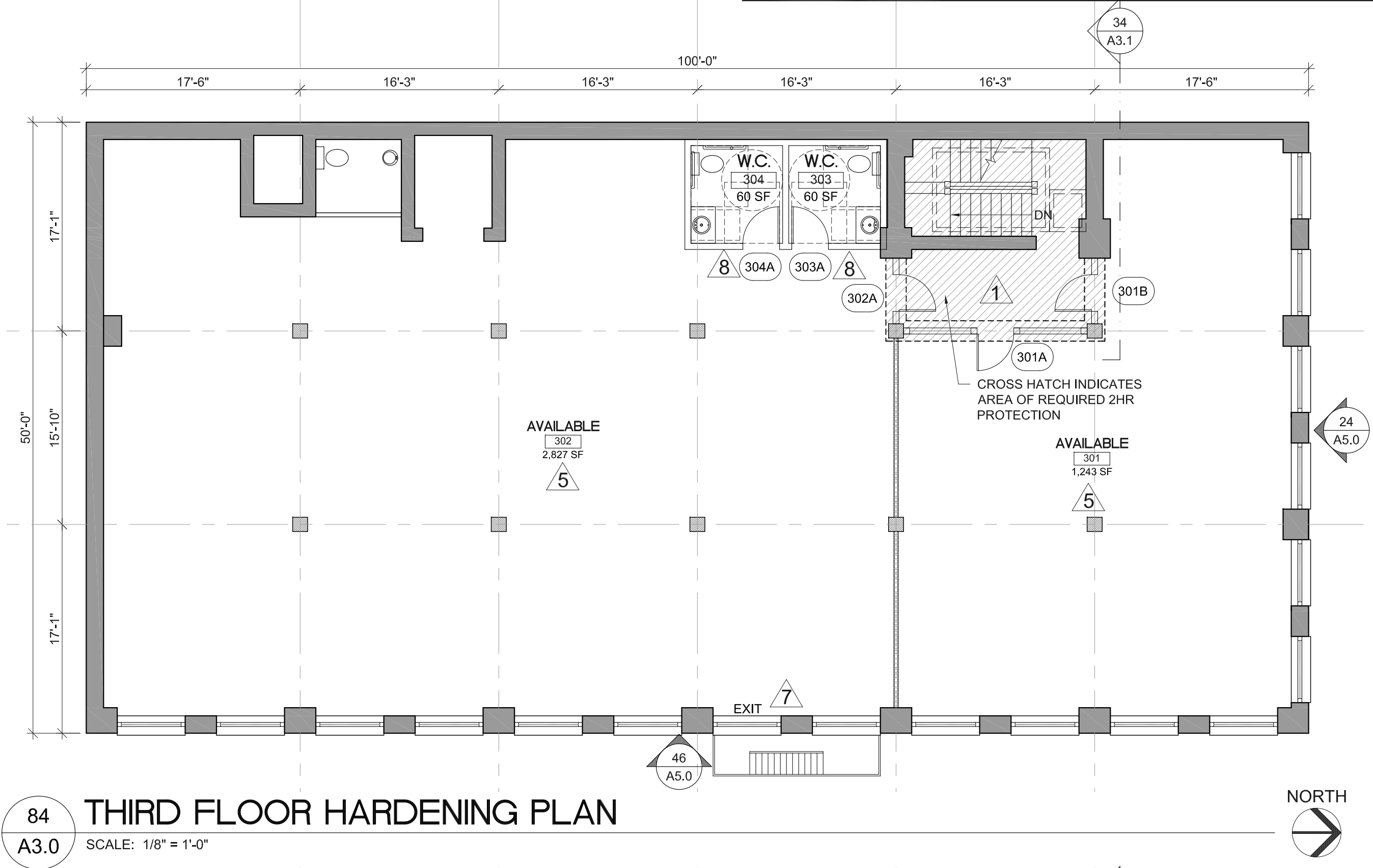


46 BASEMENT DEMO PLAN

A2.0 SCALE: 1/8" = 1'-0"

DOOR SCHEDULE									
NO.	SIZE	FRAME	DOOR			ACCESS	HDW FUNCTION	REMARKS	
	W. x HT. x THK.	MATERIAL / FINISH	MATERIAL / FINISH	LABEL	TEXTURE				
B01A	3'-0" x 7'-0" x 1 3/4"	HM, O.S. / PF.	HM, O.S. / PF.	90-MIN.	SMOOTH	PASSAGE	PB. & LATCH	FIRELIGHT - 100 SQ. IN. MAX. - EGRESS STAIRWAY	
101A	3'-0" x 7'-0" x 1 3/4"	STOREFRONT	STOREFRONT	N/R	GLAZE	KEYED	LEVER & LATCH	FULL-LITE DOOR PART OF STOREFRONT SYSTEM	
101B	3'-0" x 7'-0" x 1 3/4"	STOREFRONT, O.S.	STOREFRONT, O.S.	N/R	GLAZE	KEYED	LEVER & LATCH	EXT. ENTRANCE / EXIT - STOREFRONT SYSTEM	
102A	3'-0" x 7'-0" x 1 3/4"	STOREFRONT, O.S.	STOREFRONT, O.S.	N/R	GLAZE	KEYED	LEVER & LATCH	FULL-LITE DOOR PART OF STOREFRONT SYSTEM	
102B	6'-0" x 7'-0" x 1 3/4"	STOREFRONT	STOREFRONT	N/R	GLAZE	KEYED	LEVER & LATCH	DBL. FULL-LITE - PART OF STOREFRONT SYSTEM	
201A	3'-0" x 7'-0" x 1 3/4"	HM, O.S. / PF.	HM, O.S. / PF.	90-MIN.	SMOOTH	PASSAGE	PB. & LATCH	FIRELIGHT - 100 SQ. IN. MAX. - EGRESS STAIRWAY	
201B	3'-0" x 7'-0" x 1 3/4"	HM, O.S. / PF.	HM, O.S. / PF.	90-MIN.	SMOOTH	PASSAGE	PB. & LATCH	FIRELIGHT - 100 SQ. IN. MAX. - EGRESS STAIRWAY	
301A	3'-0" x 7'-0" x 1 3/4"	STOREFRONT	STOREFRONT	N/R	GLAZE	KEYED	LEVER & LATCH	FULL-LITE DOOR PART OF STOREFRONT SYSTEM	
301B	3'-0" x 7'-0" x 1 3/4"	STOREFRONT, O.S.	STOREFRONT, O.S.	N/R	GLAZE	KEYED	LEVER & LATCH	FULL-LITE DOOR PART OF STOREFRONT SYSTEM	
302A	3'-0" x 7'-0" x 1 3/4"	STOREFRONT, O.S.	STOREFRONT, O.S.	N/R	GLAZE	KEYED	LEVER & LATCH	FULL-LITE DOOR PART OF STOREFRONT SYSTEM	
303A	3'-0" x 7'-0" x 1 3/4"	HM. / PF.	HM. / PF.	N/R	SMOOTH	LOCKABLE	LEVER & LATCH	-	
304A	3'-0" x 7'-0" x 1 3/4"	HM. / PF.	HM. / PF.	N/R	SMOOTH	LOCKABLE	LEVER & LATCH	-	
NOTE: ALL DOORS TO BE SELF- OR AUTOMATIC CLOSING WITH LATCH. ALL RATED DOORS & DOORS PART OF THE EXIT SYSTEM TO HAVE SMOKE SEALS.									
NOTES:						ABBREVIATIONS:			
• ALL INTERIOR EXIT STAIR DOORS SHALL BE MARKED WITH AN "S" LABEL.						DBL. - DOUBLE			
• ALL STOREFRONT DOORS PART OF THE EXIT STAIR SYSTEM SHALL BE UNLOCKED ON THE EGRESS SIDE TO ALLOW PASSAGE AT ALL TIMES.						EXT. - EXTERIOR			
						HM. - HOLLOW METAL			
						N/R - NON-RATED			
						O.S. - OUTSWING			
						PB. - PANIC BAR			
						PF. - PREFINISHED			

HARDENING SCHEDULE	
1	EXPAND EXISTING ENCLOSED STAIR AND EXIT LOBBY. PROVIDE 2HR FIRE CURTAIN AT NON-RATED ASSEMBLIES REQUIRING 2HR FIRE RESISTANCE WITH "TYCO MODEL WS - 2HR FIRE BARRIER" ASSEMBLY.
2	REPLACE NON RATED EXIT DOORS WITH PANIC EGRESS PASSAGE.
3	REPAIR EXISTING WOOD STAIR.
4	NEW BRACING PER STRUCTURAL. PROTECT STRUCTURAL ELEMENTS TO MEET 2HR FIRE REISISTIVE REQUIREMENTS.
5	ALL AREAS NOT A PART OF THE EXIT STAIR SYSTEM SHALL BE PROTECTED WITH A MINIMUM NFPA 13 FIRE SPRINKLER SYSTEM THROUGHOUT.
6	EXPAND 2HR RATED STAIR ENCLOSURE. USE 2HR RATED WALL AND 1.5 HR DOOR ASSEMBLIES. PROVIDE 2HR FIRE RESISTIVE CONSTRUCTION FOR LOAD BEARING STRUCTURAL ELEMENTS. EXTEND PROTECTION TO NEXT VERTICAL SUPPORT(S) CONTINUOUS TO FOUNDATION.
7	REPAIR EXISTING WINDOW, FRAME AND WEIGHTS. PAINT AND REPAIR EXISTING FIRE ESCAPE.
8	ADD ACCESSIBLE TOILET ROOMS.
NOTES:	
• DRAWINGS BASED ON ASBUILT PLANS.	
• CONTRACTOR TO FIELD VERIFY ALL DIMENSIONS.	



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1410 NW JOHNSON STREET  
for GANN BUILDING LLC  
HARDENING PLANS

PERMIT SET

PLL1410NWJ - 03

A3.0

05.09.2019



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PORTLAND, OR

1410 NW JOHNSON STREET

for GANN BUILDING LLC

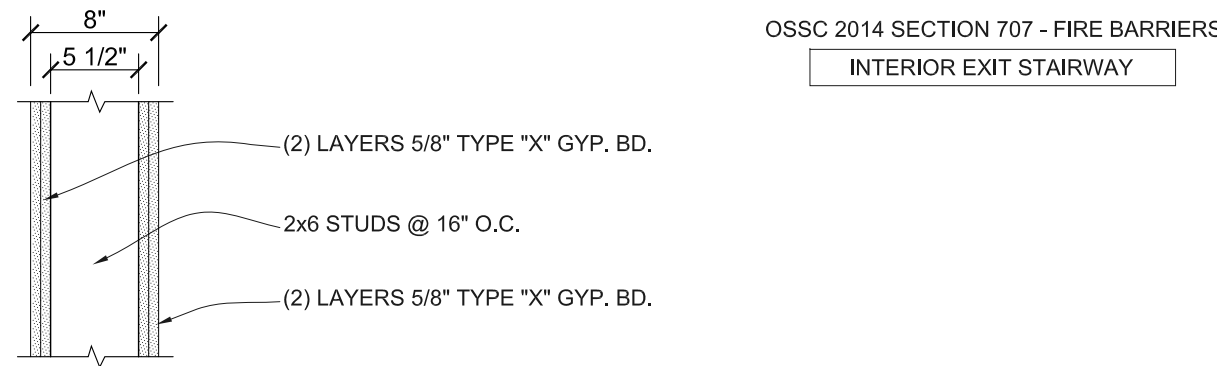
HARDENING PLANS - ENLARGED

PERMIT SET

PLL1410NWJ - 03

A3.1

05.09.2019



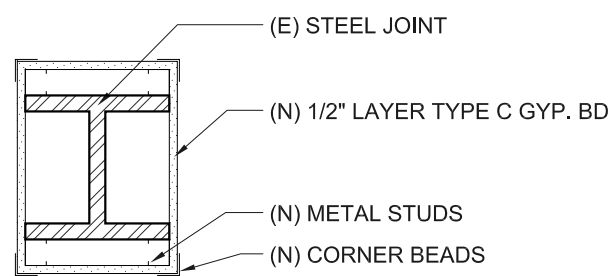
CONSTRUCTION  
BASE LAYER 5/8" TYPE X GYPSUM WALLBOARD OR VENEER BASE APPLIED PARALLEL OR AT RIGHT ANGLES TO EACH SIDE OF 2X6 STUDS 16" O.C. WITH 1-1/4" TYPE W DRYWALL SCREWS 12" O.C.. FACE LAYER 5/8" TYPE X GYPSUM WALLBOARD OR VENEER BASE APPLIED PARALLEL OR AT RIGHT ANGLES TO EACH SIDE WITH 1-7/8" TYPE W DRYWALL SCREWS 12" O.C. AND OFFSET 6" FROM SCREWS IN BASE LAYER.

JOINTS STAGGERED 16" EACH LAYER AND SIDE. (LOAD BEARING)

FIRE TEST: SWRI 01-5920-614, 12-5-94

SOUND TEST: SEE WP 4135 (NGC 2363, 4-1-70)

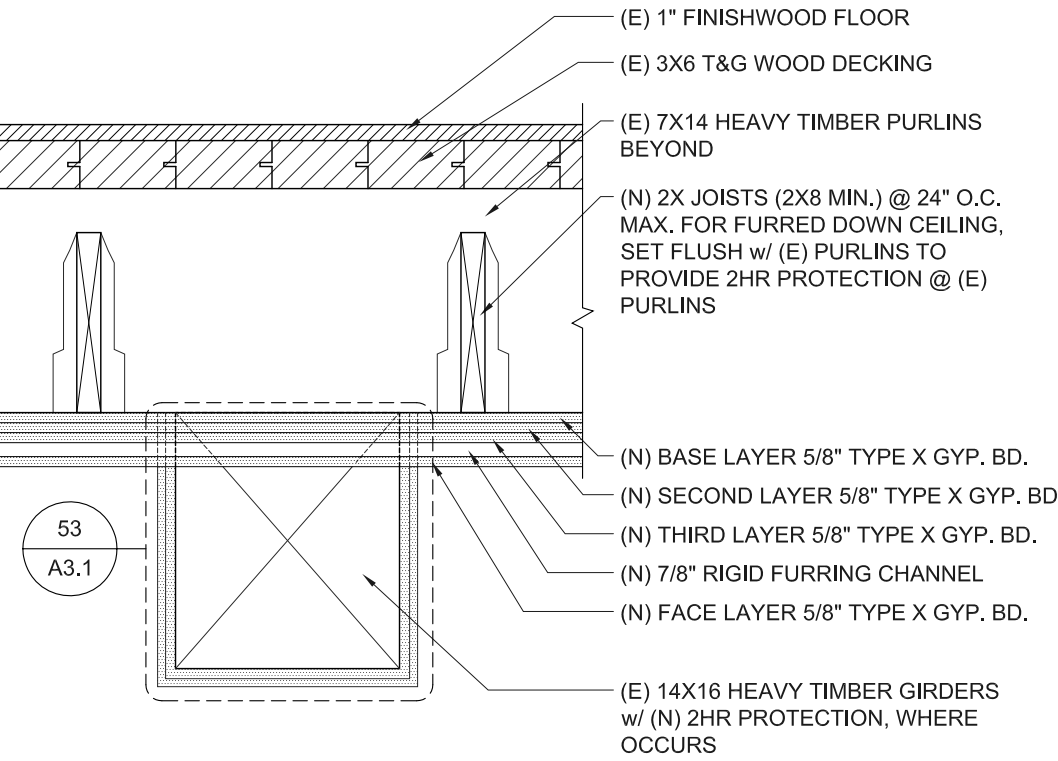
**73 2 HR. INT. 5 1/2" WOOD**  
A3.1 SCALE: 1" = 1' - 0" GA FILE No.: WP 4136



1/2" LAYER NOM. 3/32" THICK GYPSUM TYPE C GYPSUM BOARD ATTACHED WITH 1" LONG SELF-DRILLING, SELF-TAPPING STEEL SCREWS, SPACED VERTICALLY 12" O.C. TO STEEL STUDS 1-5/8" WIDE WITH LEG DIMENSIONS OF 1-5/16" AND 1-7/16" WITH A 1/4" FOLDED FLANGE IN LEGS FABRICATED FROM 25 MSG GALV STEEL. 3/4" BY 1-3/4" RECTANGULAR CUTOUTS PUNCHED 8" AND 16" FROM THE ENDS. STEEL STUD CUT 1/2" LESS IN LENGTH THAN ASSEMBLY HEIGHT. CORNER BEADS NO. 28 MSG GALV STEEL. 1-1/4" LEGS ATTACHED TO GYPSUM BOARD BY CRIMPING SPACED 6" O.C..

FIRE TEST: UL X520 AND CITY OF PORTLAND BUILDING CODE APPEAL APPROVAL.

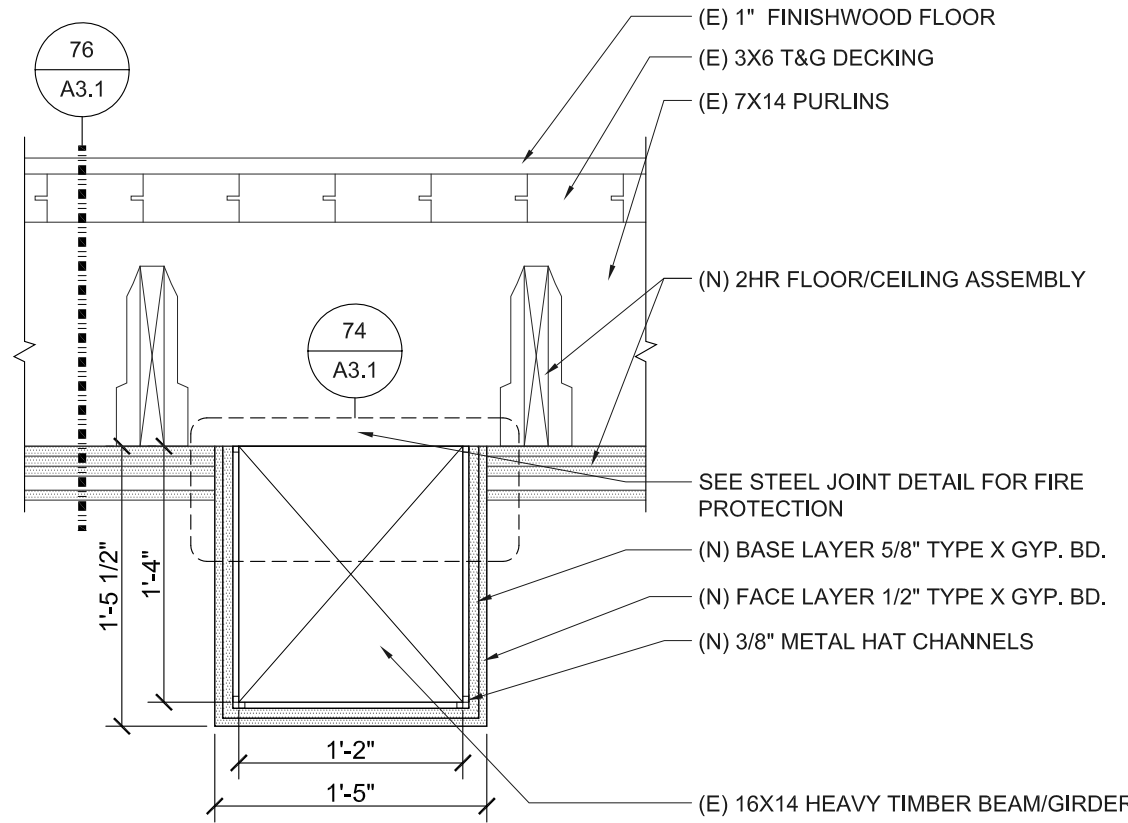
**74 2-HR FIRE-RATED STEEL JOINT DETAIL**  
A3.1 SCALE: 1" = 1' - 0" CITY OF PORTLAND BUILDING CODE APPEAL IDXXXX



BASE LAYER - 5/8" TYPE X GYPSUM WALLBOARD APPLIED AT RIGHT ANGLES TO 2X8 WOOD JOISTS 24" O.C. WITH 1-1/4" TYPE W DRYWALL SCREWS 12" O.C. SECOND LAYER - 5/8" TYPE X GYPSUM WALLBOARD APPLIED AT RIGHT ANGLES TO JOISTS WITH 2" TYPE W DRYWALL SCREWS 12" O.C. SECOND LAYER JOINTS OFFSET 24" FROM BASE LAYER JOINTS. THIRD LAYER - 5/8" TYPE X GYPSUM WALLBOARD APPLIED AT RIGHT ANGLES TO JOISTS WITH 2-1/2" TYPE W DRYWALL SCREWS 12" O.C. THIRD LAYER JOINTS OFFSET 12" FROM SECOND LAYER JOINTS. HAT-SHAPED 7/8" RIGID FURRING CHANNELS 24" O.C. APPLIED AT RIGHT ANGLES TO JOISTS OVER THIRD LAYER WITH TWO 2-1/2" LONG TYPE W DRYWALL SCREWS AT EACH JOIST. FACE LAYER - 5/8" TYPE X GYPSUM WALLBOARD APPLIED AT RIGHT ANGLES TO FURRING CHANNELS WITH 1-1/8" TYPE S DRYWALL SCREWS 12" O.C. WOOD JOISTS SUPPORTING 3/4" T&G EDGE PLYWOOD FLOOR APPLIED AT RIGHT ANGLES TO JOISTS WITH 8d NAILS 6" O.C. AT JOINTS AND 12" AT INTERMEDIATE JOISTS. CEILING PROVIDES TWO-HOUR FIRE-RESISTANCE PROTECTION FOR WOOD FRAMING.

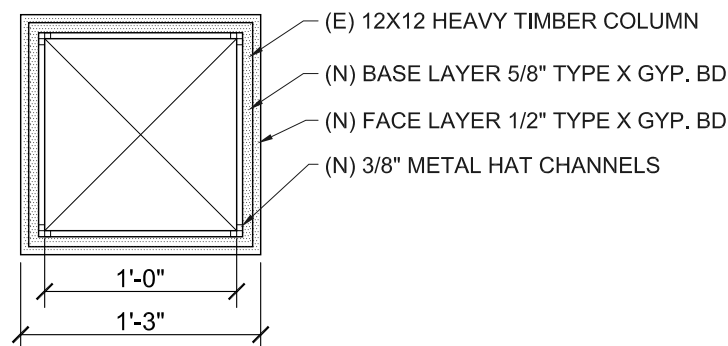
FIRE TEST: UL R4024, 00NK26545, 4-27-01; UL R4024, 03NK11206, 3-19-03; UL DESIGN L556; ULC DESIGN M514

**76 2-HR FIRE-RATED FLOOR/CEILING DETAIL**  
A3.1 SCALE: 1" = 1' - 0" GA FILE NO.: FC 5725



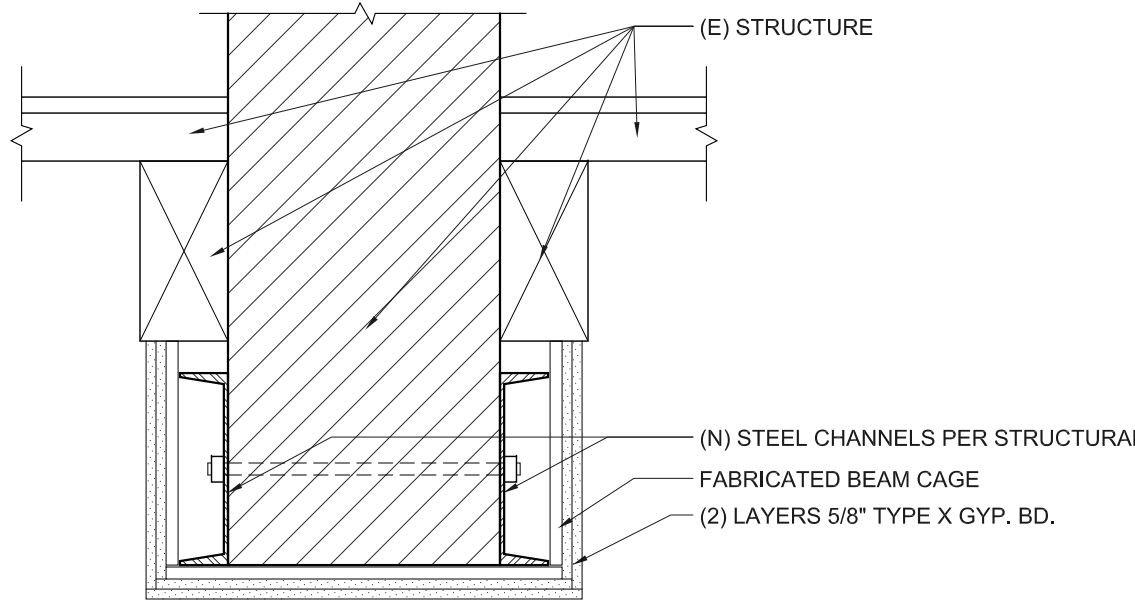
CONSTRUCTION:  
BASE LAYER 5/8" TYPE X GYPSUM WALLBOARD ATTACHED TO 3/8" METAL HAT CHANNELS WHICH ARE ATTACHED TO 14X16 HEAVY TIMBER WOOD BEAM NOMINAL (MINIMUM 8X12 NOMINAL). FACE LAYER 1/2" TYPE X GYPSUM WALLBOARD.

**53 2 HR. HEAVY TIMBER BEAM WRAP**  
A3.1 SCALE: 1" = 1' - 0" CITY OF PORTLAND BUILDING CODE APPEAL IDXXXX



CONSTRUCTION:  
BASE LAYER 5/8" TYPE X GYPSUM WALLBOARD ATTACHED TO 3/8" METAL HAT CHANNELS WHICH ARE ATTACHED TO 12X12 HEAVY TIMBER WOOD COLUMN (MINIMUM 12X12 NOMINAL). FACE LAYER 1/2" TYPE X GYPSUM WALLBOARD.

**54 2 HR. HEAVY TIMBER COLUMN WRAP**  
A3.1 SCALE: 1" = 1' - 0" CITY OF PORTLAND BUILDING CODE APPEAL IDXXXX

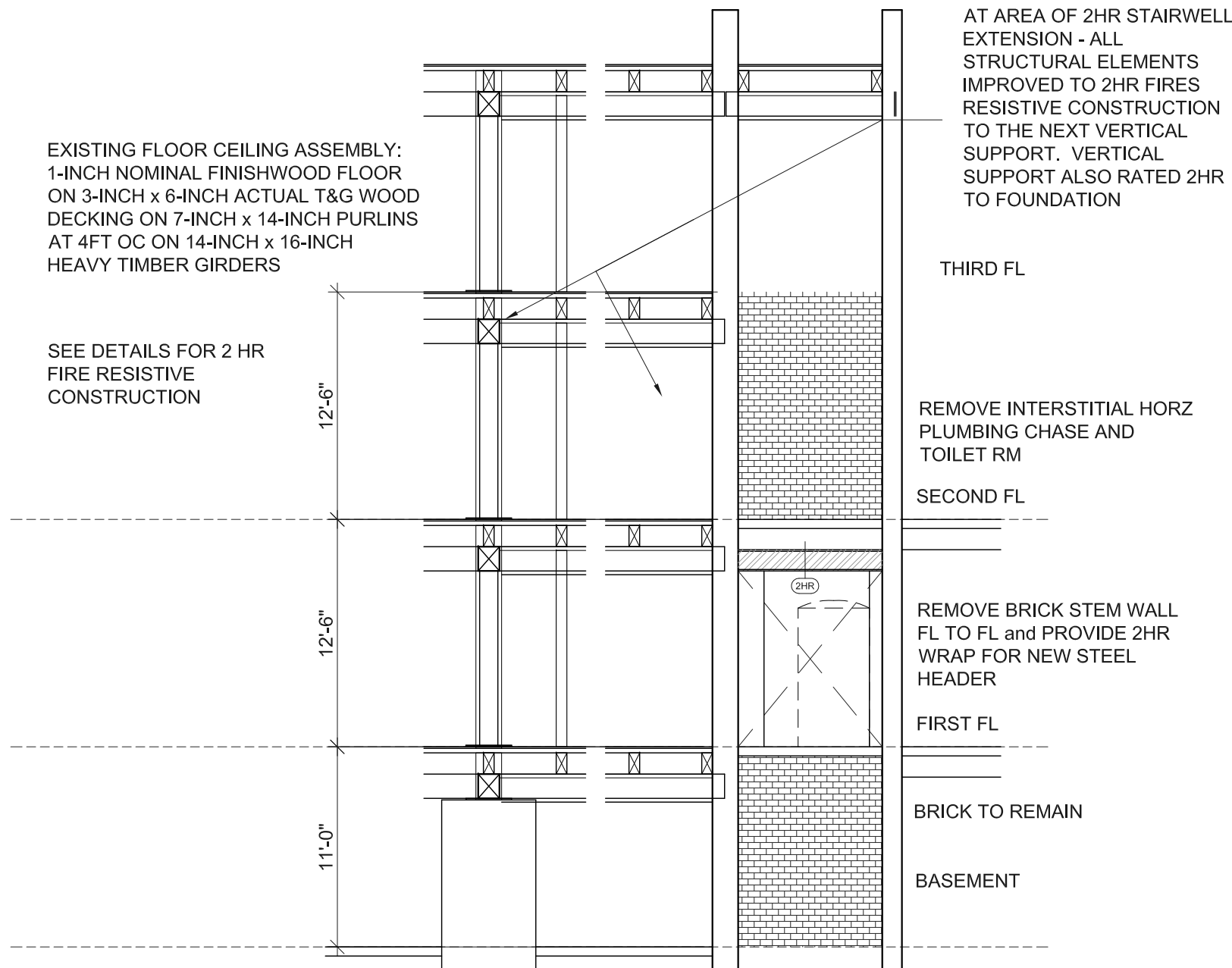


BASE LAYER - 5/8" TYPE X GYPSUM WALLBOARD OR GYPSUM VENEER BASE APPLIED TO BEAM CAGE WITH 1-1/4" TYPE S DRYWALL SCREWS 16" O.C.. FACE LAYER - 5/8" TYPE X GYPSUM WALLBOARD OR GYPSUM VENEER BASE APPLIED TO BEAM CAGE WITH 1-3/4" TYPE S DRYWALL SCREWS 8" O.C..

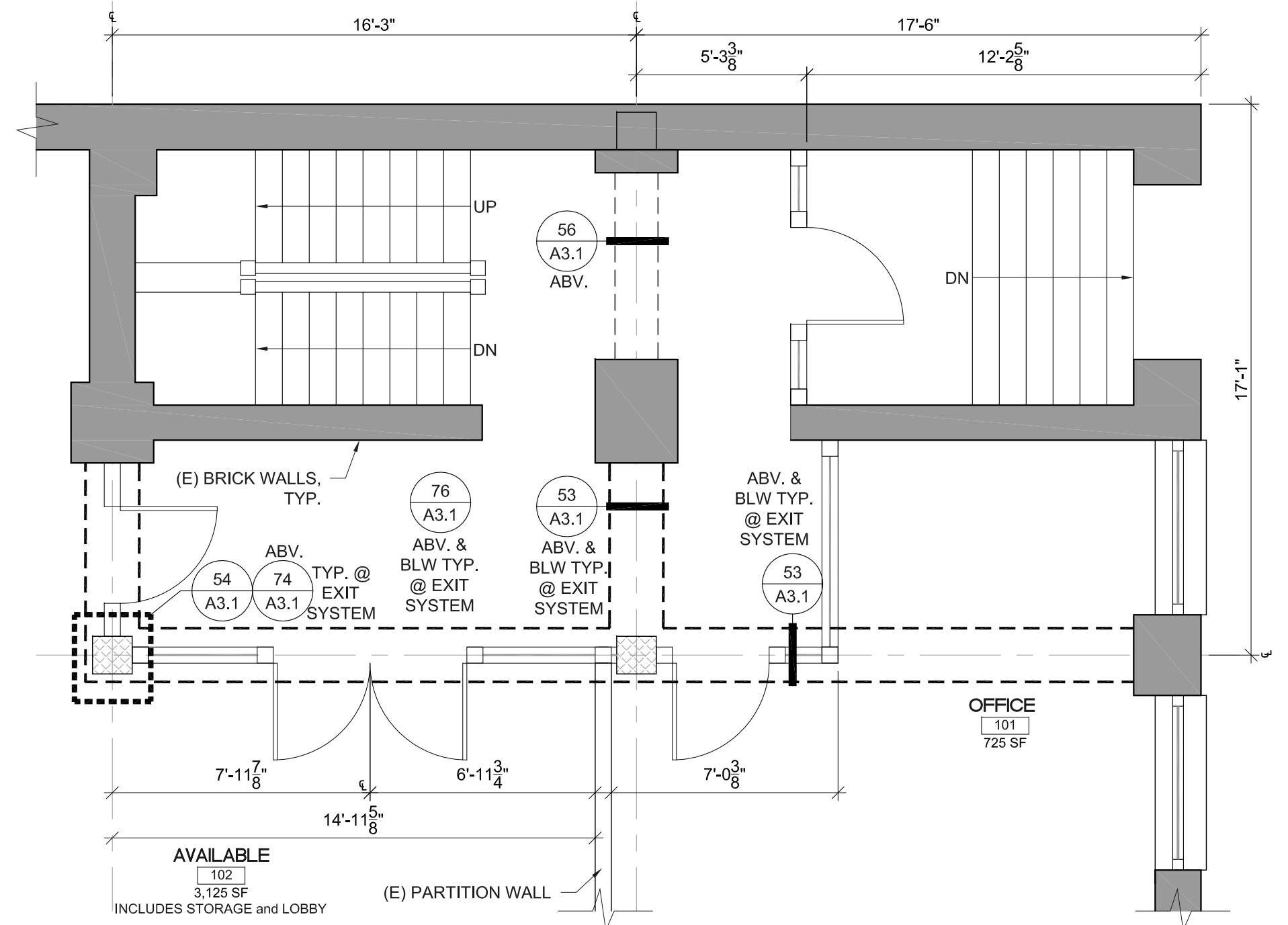
BEAM CAGE FABRICATED FROM HORIZONTAL INSTALLED STEEL ANGLES (25 GA STEEL HAVING 1" AND 2" LEGS) LOCATED NOT LESS THAN 1/2" FROM BEAM FLANGES. 1" LEGS OF THE UPPER ANGLES SECURED TO STEEL DECK UNITS WITH 1/2" TYPE S PAN HEAD SCREWS 12" O.C. 4" U" SHAPED BRACKETS FORMED OF 25 GA "U" SHAPED STEEL CHANNELS (1-11/16" WIDE WITH 1" LEGS) 24" O.C. SUSPENDED FROM UPPER ANGLES WITH 1/2" TYPE S PAN HEAD SCREWS AND SUPPORTED 1" X 2" ANGLES AT LOWER CORNERS ATTACHED TO BRACKETS WITH 1/2" TYPE S PAN HEAD SCREWS. OUTSIDE CORNERS OF GYPSUM BOARD PROTECTED BY 0.020" THICK STEEL CORNER BEADS CRIMPED OR NAILED. MINIMUM BEAM SIZE W8X24. (TWO HOUR RESTRAINED OR UNRESTRAINED BEAM.)

FIRE TEST: UL R4024-5, 9-14-66,  
UL DESIGN N501;  
ULC DESIGN O501

**56 2-HR FIRE-RATED BEAM WRAP DETAIL**  
A3.1 SCALE: 1" = 1' - 0" GA FILE NO.: BM 2120



**34 ELEVATION + SECTION AT EXIT SYSTEM**  
A3.1 SCALE: 1/8" = 1'-0"



**36 ENLARGED FIRST FLOOR EXIT LOBBY**  
A3.1 SCALE: 1/4" = 1'-0"

80

70

60

50

40

30

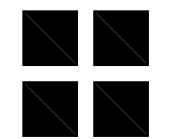
20

10

0



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PORTLAND, OR

1410 NW JOHNSON STREET  
for GANN BUILDING LLC  
EXTERIOR ELEVATIONS

PERMIT SET

PLL1410NWJ - 05

A5.0

05.09.2019

1

2

3

4

5

80

70

60

50

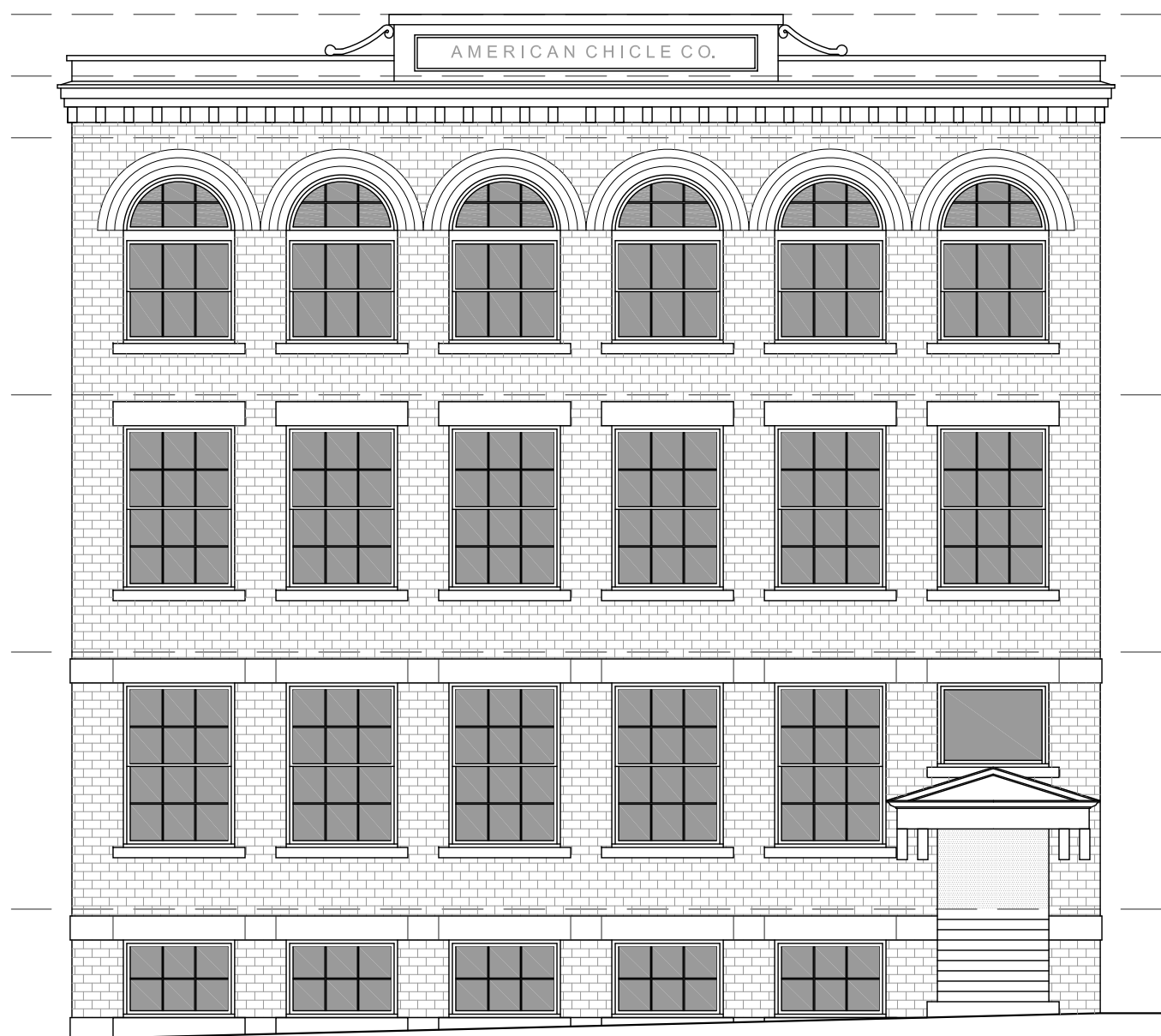
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30

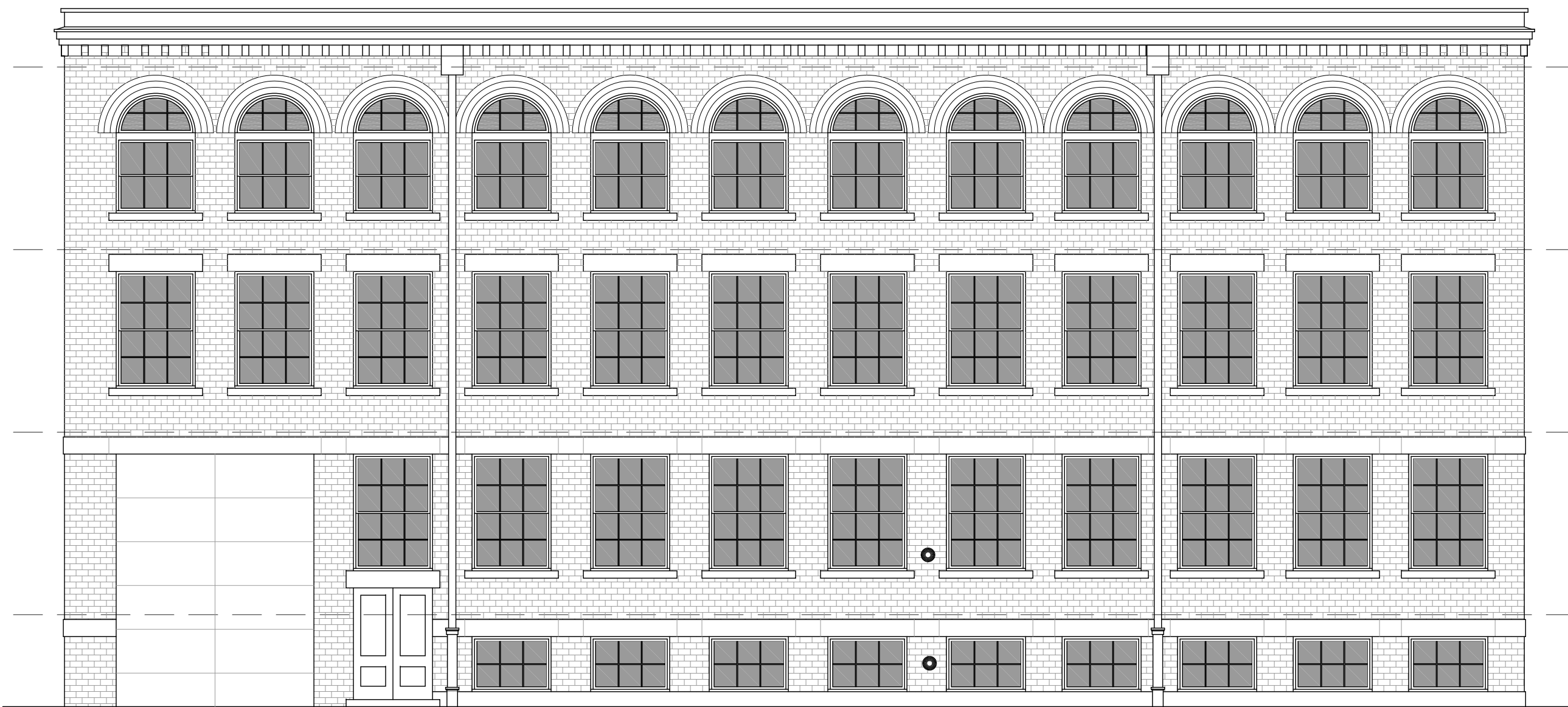
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10

6

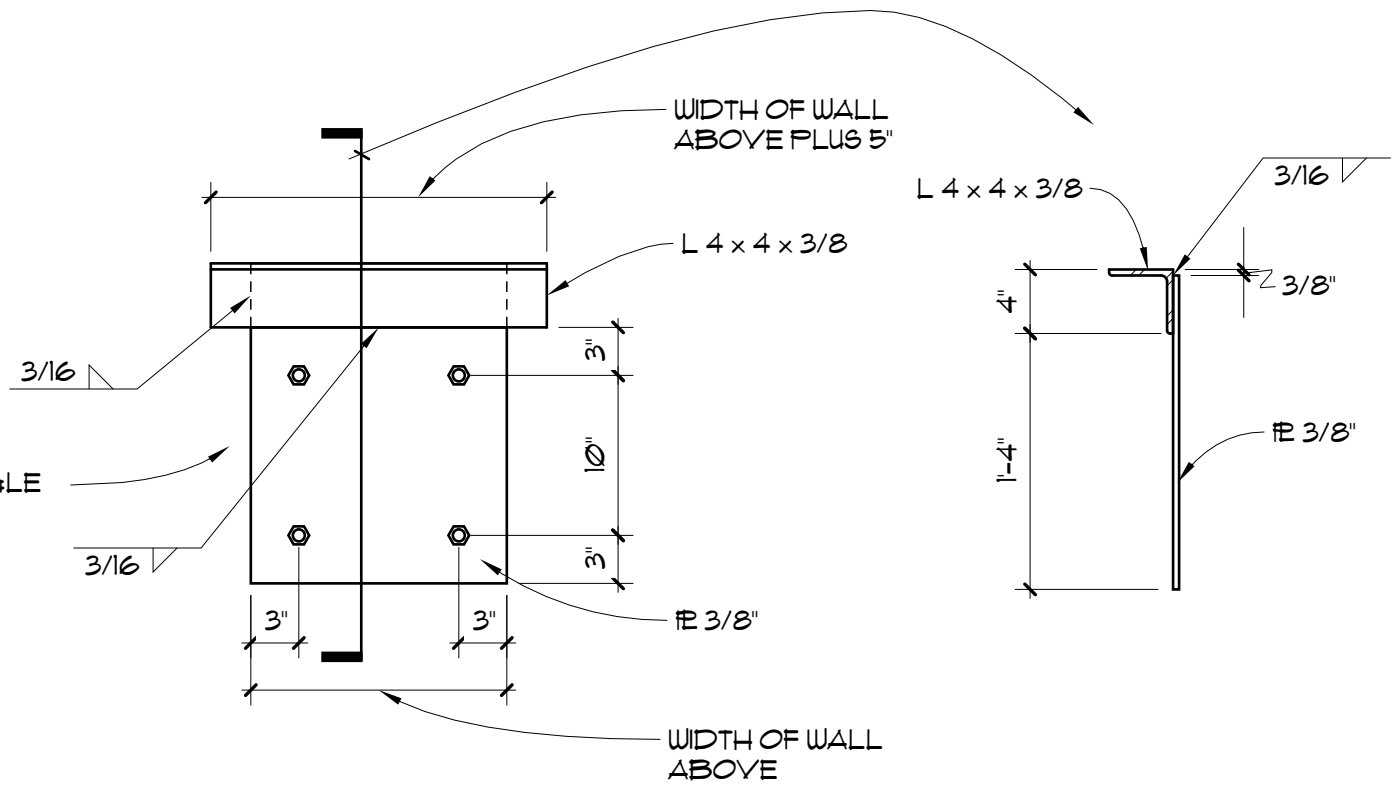
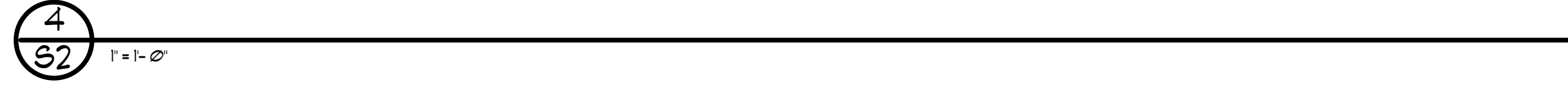
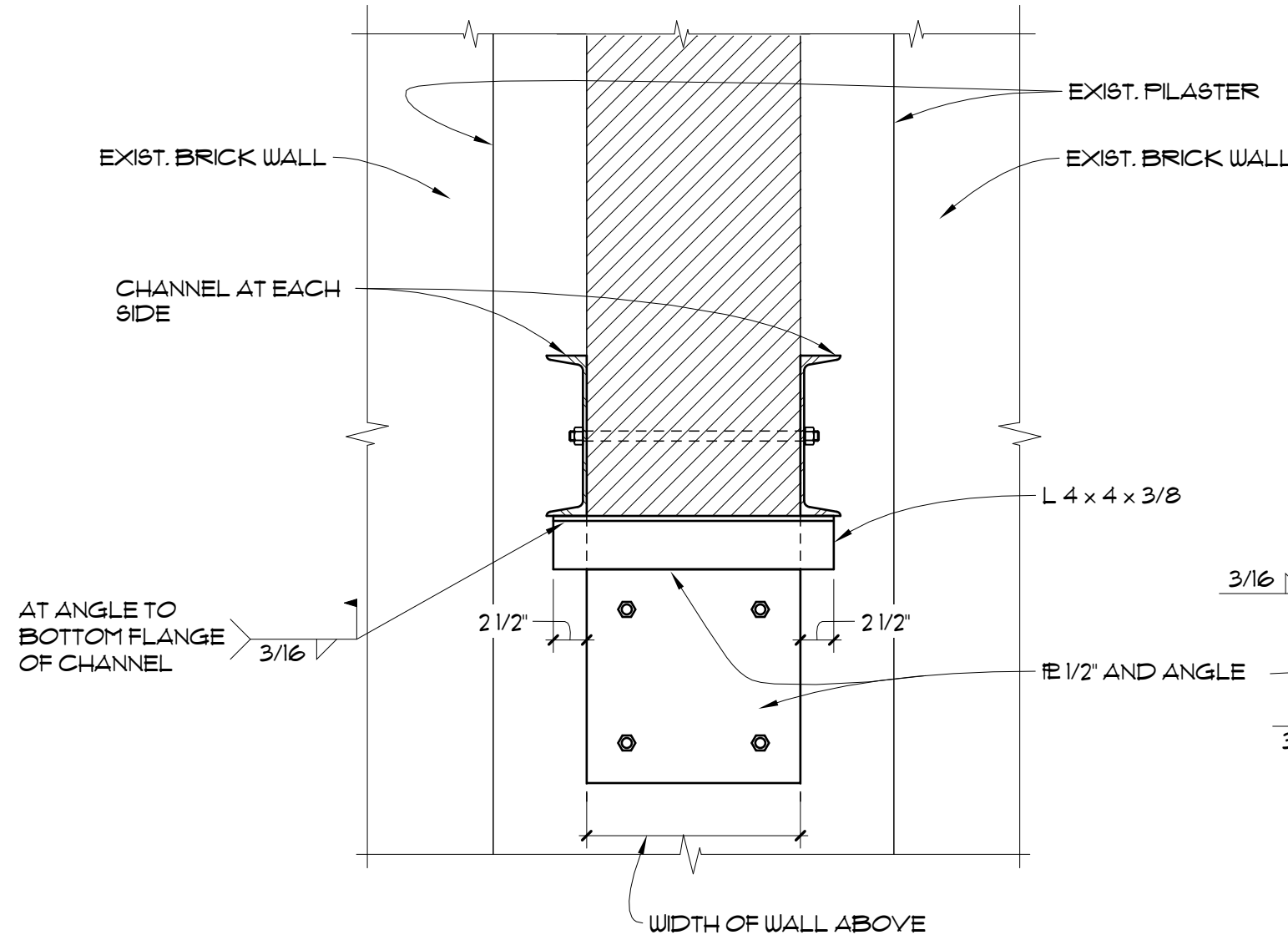
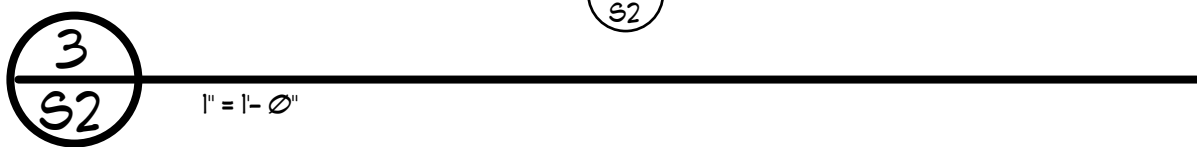
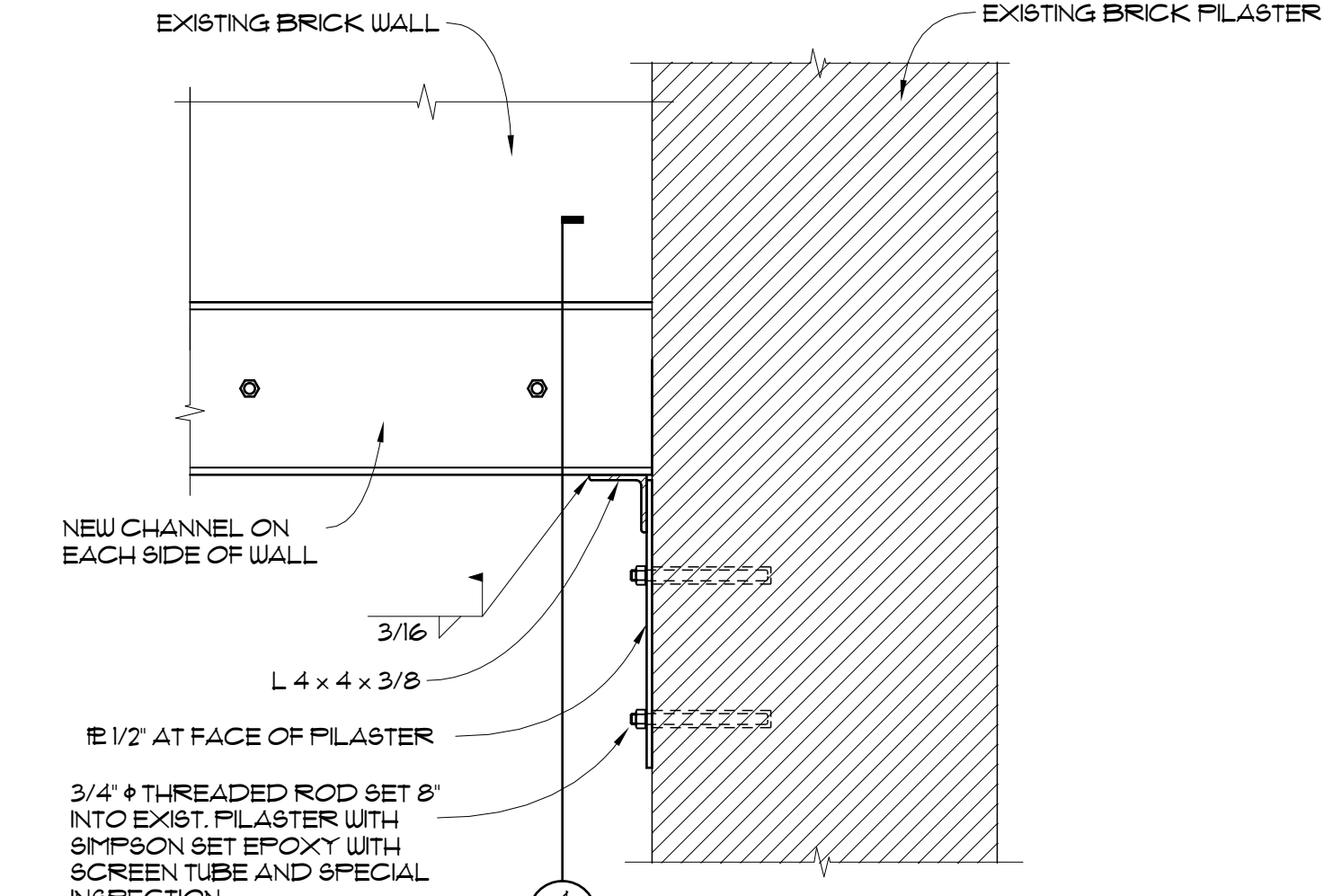
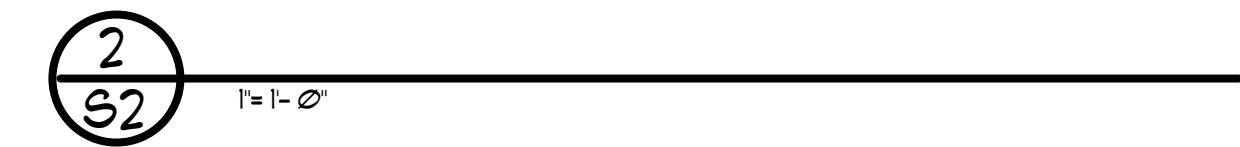
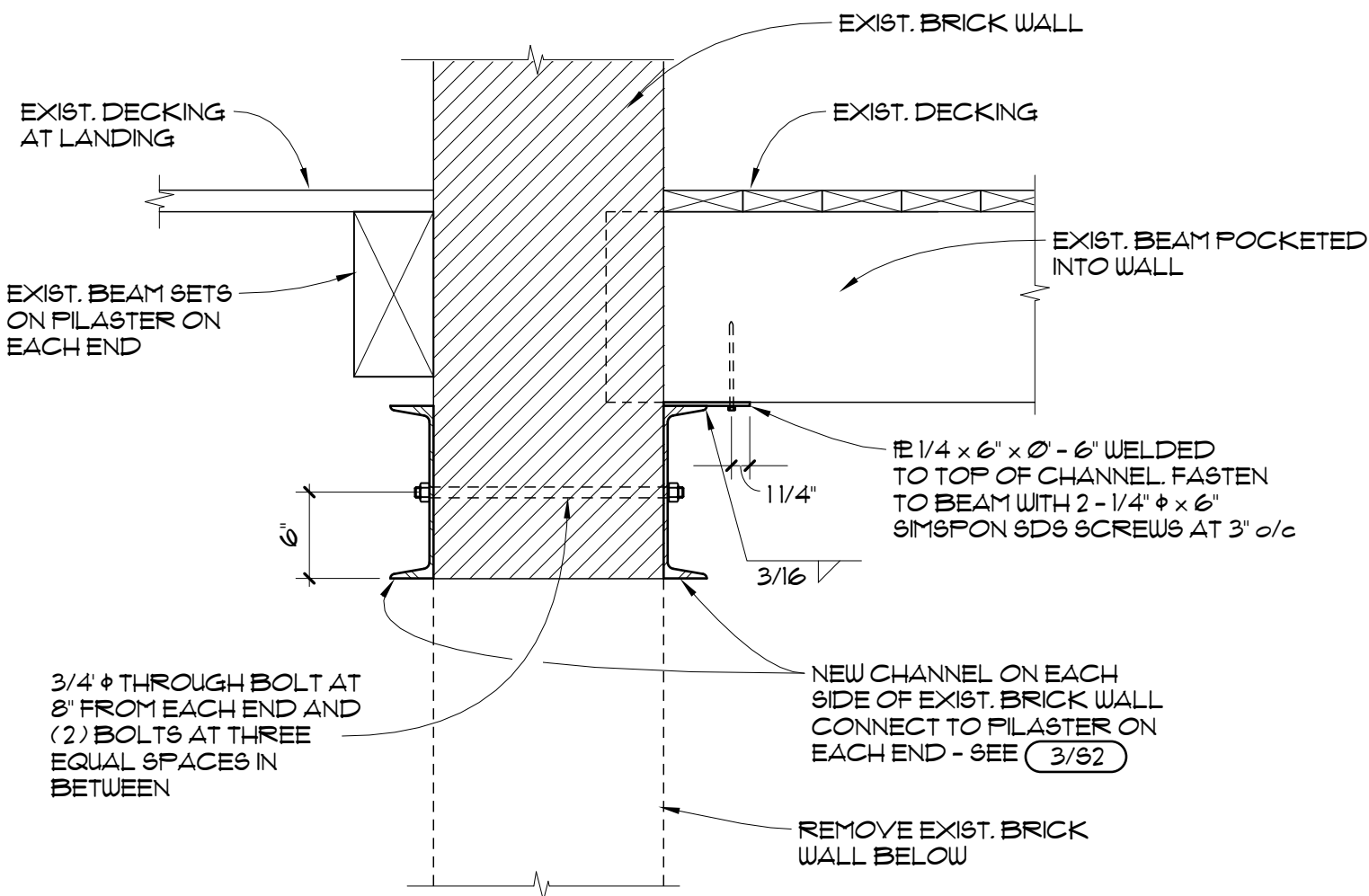
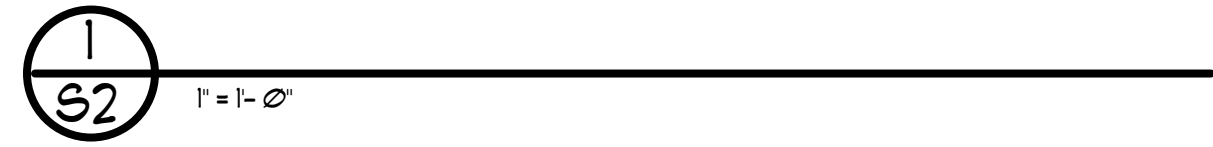
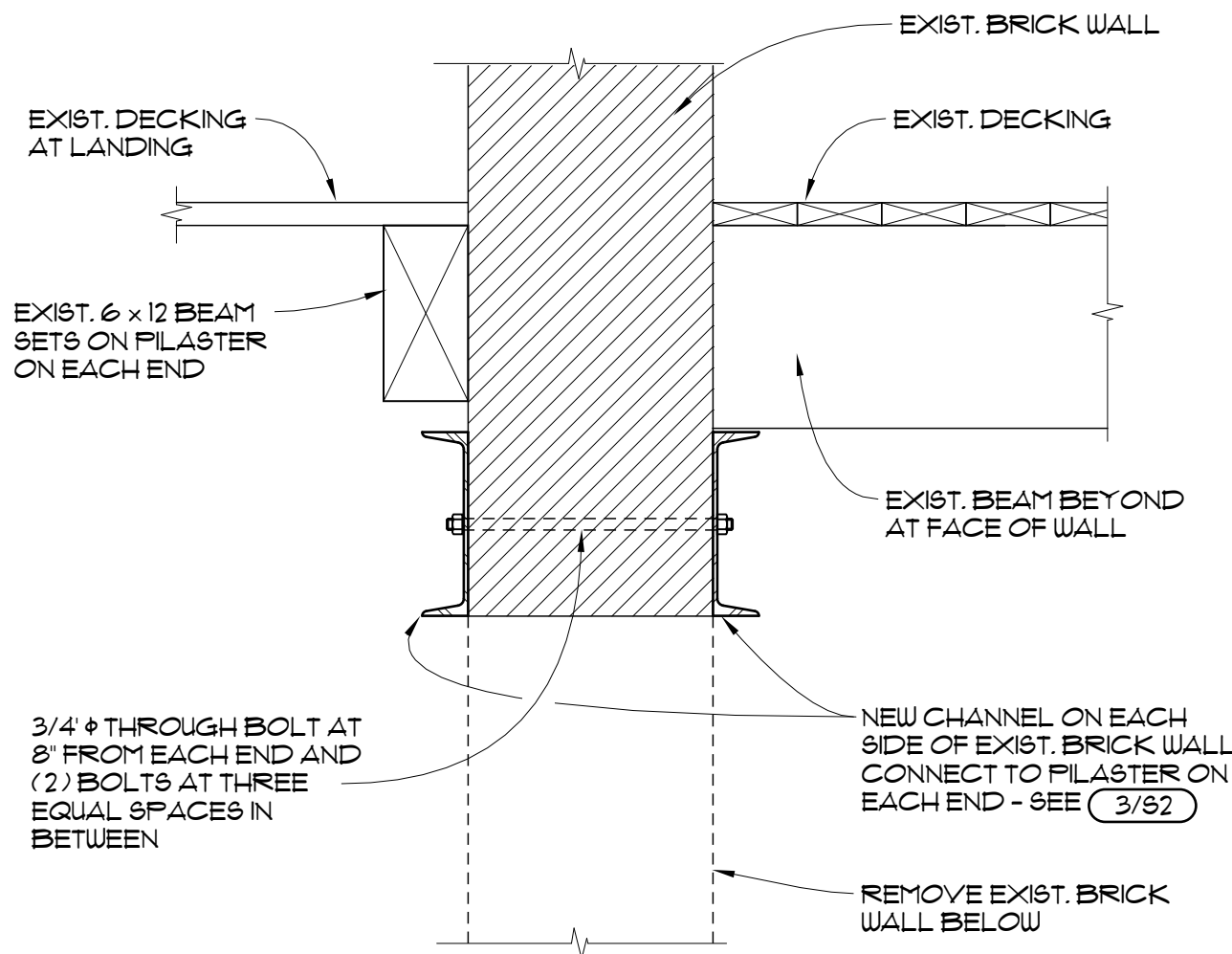


24 JOHNSON STREET ELEVATION  
A5.0 SCALE: 1/8" = 1'-0"



46 10TH AVENUE ELEVATION  
A5.0 SCALE: 1/8" = 1'-0"





EXPIRES: 12/31/2019

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**1410 NW JOHNSON STREET**  
for PORTLAND LEEDS LIVING  
PLANS

PORTLAND, OR

PLANS

**S2**

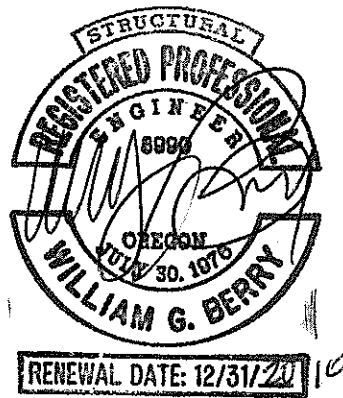
04.22.2019

# STRUCTURAL CALCULATIONS

FOR

## Net Section Analysis for Posts and Floor Beams

1410 NW Johnson St.  
Portland, OR



ENGINEER WAS RETAINED IN A LIMITED CAPACITY FOR THIS PROJECT. DESIGN IS BASED UPON INFORMATION PROVIDED BY THE CLIENT WHO IS SOLELY RESPONSIBLE FOR ACCURACY OF THAT INFORMATION. NO RESPONSIBILITY AND/OR LIABILITY ARE ASSUMED BY, OR ARE TO BE ASSIGNED TO, THE ENGINEER FOR ITEMS BEYOND THAT SHOWN IN THESE CALCULATIONS.



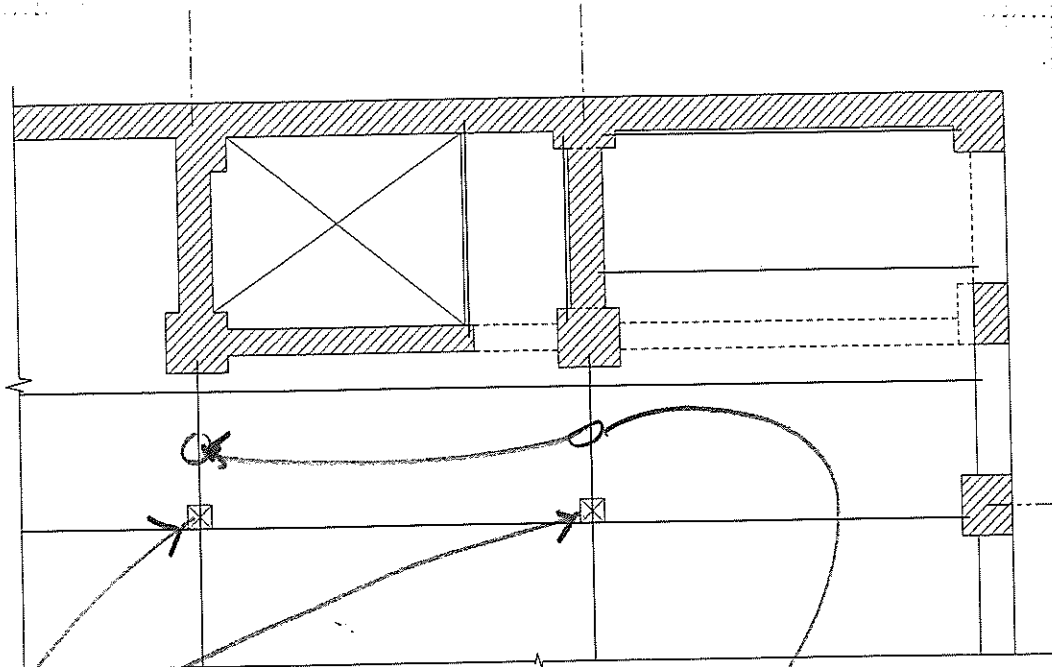
Project: Post and Beam Analysis @ NW Johnson St.

Client: Marty Kehoe Proj. No.: 19-045

Date: 05/2019 By: BB Sheet No.: COVER

## **DESIGN SUMMARY**

The intent of these calculations is to verify the load capacity for floor beams and posts in an area of two-hour protection adjacent to the stairs after a fire. A Fire Protection Engineer has determined the depth of char on the members. For the floor beam the depth of char is 2" on two sides and the bottom. For the post the depth of char is 2" on all four sides. The existing floor beam is a 14x16 wood member. The effective size will be reduced to 10x14. The existing post is a 12x12 wood member. The effective size after the fire is 8x8. The calculations show that the floor beam and post will be adequate as reduced sections.



CHECK THESE TWO POSTS  
AS REDUCED SECTIONS

CHECK THESE BEAMS  
AS REDUCED SECTIONS

SECOND FLOOR FRAMING PLAN



Project: 14th & JOHNSON

Client: MARTY KEHOE

Proj. No.: \_\_\_\_\_

Date: 5/20/19

By: BB

Sheet No.: 1

CALCULATE LOADS ON  
FLOOR BEAM AND POST  
IN TWO HR RATED  
AREA ADJACENT TO  
STAIR WELL

LOADING:

ROOF:

SNOW 25 PSF  
DEAD 15 PSF

FLOORS

OFFICE LOADING

LIVE LOAD: 50 PSF

PARTITIONS: 15 PSF

DEAD: 15 PSF → [1]  
→ 22 PSF → [2]

[1] DEAD LOAD DUE  
TO PLR FINISH, DECKING,  
FRAMING

[2] ADD 7 PSF DUE TO  
GYD CEILING

ADJACENT TO  
STAIR WELL

LIVE LOAD = 100 PSF  
DEAD LOAD = 22 PSF

PARTITION LOAD = 0 PSF



Project: 14th & JOHNSON

Client: MARTY KEHOE

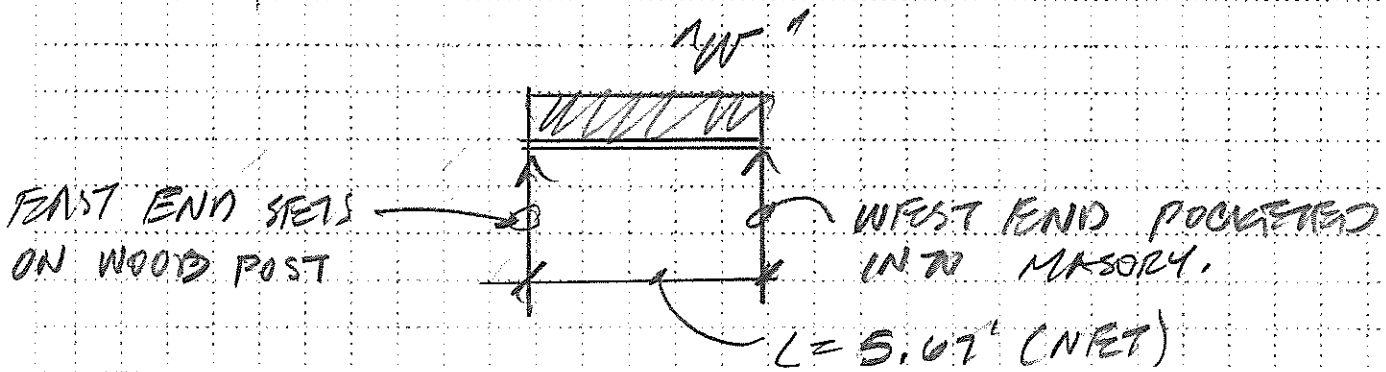
Proj. No.:

Date: 5/20/19

By: BB

Sheet No.: 2

# CHECK FLOOR BEAM



## DETERMINE "W"

### FLOOR LOADS:

LIVE LOAD = 100 PSF  
DEAD LOAD = 22 PSF  
PARTITION = 0 PSF

$$W = (122 \text{ psf}) (16.5 + 16.25) / 2$$

$$= 1998 \#/\text{ft}$$

$$M = 1998 \#/\text{ft} \times 5.67^2 / 8$$

$$= 8030 \text{ ft-lb}$$

ALLOWABLE BENDING  
STRESS FOR 6x WAREHOUSE  
DF/L #1.

$$F_b = 1300 \text{ psi}$$

ORIGINAL BEAM:

$$14 \times 16$$

$$\text{NET} = 13'1/2 \times 15'1/2$$

AFTER FIRE WITH  
2" CHART ON (3) SIDES

$$9.5" \times 13.5"$$

$$S = (9.5)(13.5)^2 / 6$$

$$= 288 \text{ in}^3$$



Project: 14th & JOHNSON

Client: MARTY KEHOE

Date: 5/20/19 By: BB

Proj. No.: \_\_\_\_\_

Sheet No.: 3

K1 M= 8030#-1

SNET AFTER PAINT  
= 288 IN 3

$$f_b = \frac{8030(12)}{288}$$
$$= 335 \text{ psi}$$

$$F_b = 1300 \text{ psi} > 335$$

PREAM IS OKAY



Project: 14th & JOHNSON

Client: MARTY KEROE

Proj. No.: \_\_\_\_\_

Date: 5/20/19 By: BB

Sheet No.: 4

DETERMINE TOTAL  
LOAD ON POST

TRIBUTARY AREA FOR  
LOAD ON POST

$$\begin{aligned}\text{TRIBUTARY WIDTH} \\ &= (10.25 + 16.5) / 2 \\ &= 16.37'\end{aligned}$$

$$\begin{aligned}\text{TRIBUTARY LENGTH} \\ &= (6 + 15.83) / 2 \\ &= 10.92'\end{aligned}$$

AT ROOF:

SNOW = 25 PSF

DEAD LOAD: 15 PSF & 22 PSF

$$\begin{aligned}P &= (25 + 15)(16.37) \times 6 / 2 \\ &+ (25 + 22)(16.37)(15.83 / 2) \\ &= 1965\# + 6090\# \\ &= 8055\#\end{aligned}$$

AT 3RD FLR

$$\begin{aligned}P &= (100 + 22)(16.37)(6 / 2) \\ &+ (50 + 15 + 15)(16.37)(15.83 / 2) \\ &= 5992\# + 10,365\# \\ &= 16357\#\end{aligned}$$

AT 2ND FLR

LOAD ON POST IS THE  
SAME AS AT 3RD  
FLR

$$P = 16357\#$$

AT 1ST FLR

LOAD ON POST IS THE  
SAME AS AT 3RD FLR

$$P = 16357\#$$



Project: 14th & JOHNSON

Client: MARTY KEHOE

Proj. No.: \_\_\_\_\_

Date: 5/20/19 By: BB

Sheet No.: 5

## CHECK LIVE LOAD REDUCTION

$$\begin{aligned} \text{AREA} &= (16.37)(6/2) \\ &\quad + (16.37)(15.83/2) \\ &= 50 + 130 \\ &= 180 \text{ ft}^2 \end{aligned}$$

NO REDUCTION AT ROOF

INTERIOR POST

$$K_L = 4$$

$$K_L A_T = 720 \text{ ft}^2$$

$$L = L_0 \left( 0.25 + \frac{15}{(K_L A_T)^{1/2}} \right)$$

$$L = L_0 \left( 0.25 + \frac{15}{(720)^{1/2}} \right)$$

$$L = L_0 (0.25 + 0.56)$$

$$L = L_0 (0.81)$$

REDUCE LIVE LOAD AT  
EACH LEVEL BY 19%

FOR (3) LEVELS

TOTAL REDUCTION IS

$$19 \times 3 = 57\%$$

TOTAL ALLOWABLE  
REDUCTION ON POST  
IS 60% OK

## REDUCED LOADS

AT ROOF DIVIDE LOAD  
BY 1.15 FOR LOAD  
DURATION FACTOR  
 $= 7005 \text{ lb}$

## AT THIRD FLOOR

AT STAIRS:

$$\text{LIVE LOAD} = 100 \times 0.57 = 60 \text{ psf}$$

AT OFFICE

$$\text{LIVE LOAD} = 50 \times 0.57 = 30 \text{ psf}$$

$$\begin{aligned} P &= (60 + 22)(16.37)(6/2) \\ &\quad + (30 + 15 + 15)(16.37)(15.83/2) \\ &= 4090 \text{ lb} + 7775 \text{ lb} \\ &= 11,805 \text{ lb} \end{aligned}$$

LOAD SAME AT  
SECOND AND FIRST  
FLR



Project: 14th & JOHNSON

Client: MARTY KEHOE

Proj. No.: \_\_\_\_\_

Date: 5/20/19

By: BB

Sheet No.: 6

# CHECK LOAD CAPACITY FOR POST

NET HEIGHT OF POST.

AT FIRST FLR TO  
SECOND FLR

FINISHED FLR TO FIN. FLR  
 $H = 12'-6"$

NET HEIGHT OF POST

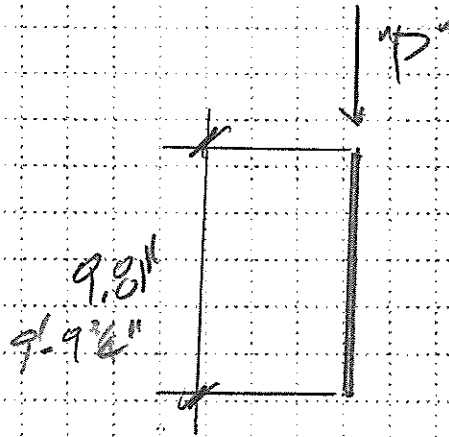
FIN. FLR =  $3/4"$

DECILING =  $2'1/2"$

FLR PURLIN =  $7 \times 14'$  ( $13'1/2"$ )

FLR BEAM =  $14 \times 16'$  ( $15'1/2"$ )

$$\begin{aligned} \text{NET} &= 12'-6" - (3/4" + 2'1/2" + 13'1/2" + 15'1/2") \\ &= 12'-6" - (2.69') \\ &= 9.91' \end{aligned}$$



$$\begin{aligned} P &= 7005\# + 11,805\# \\ &\quad + 11,805\# \\ &= 30,615\# \end{aligned}$$

AT  $7.5' \times 7.5'$  POST

$$P_{CAP} = 14.5K$$



Project: 14th & JOHNSON

Client: MARTY KEHOE

Date: 5/20/19

By: BB

Proj. No.: \_\_\_\_\_

Sheet No.: 7

## Wood Column

Lic. #: KW-06007984

DESCRIPTION: 9'-9.75" Column

— POST AT FIRST TO SECOND F.R.

### Code References

Calculations per NDS 2015, IBC 2015, CBC 2016, ASCE 7-10

Load Combinations Used : ASCE 7-16

### General Information

Analysis Method :		Allowable Stress Design		Wood Section Name		8x8	
End Fixities		Top & Bottom Pinned		Wood Grading/Manuf.		Graded Lumber	
Overall Column Height		9.813 ft		Wood Member Type		Sawn	
( Used for non-slender calculations )							
Wood Species		Douglas Fir - Larch		Exact Width		7.50 in	
Wood Grade		No.1		Exact Depth		7.50 in	
Fb +		1,350.0 psi	Fv	170.0 psi	Area		56.250 in^2
Fb -		1,350.0 psi	Ft	675.0 psi	Ix		263.672 in^4
Fc - Prll		925.0 psi	Density	31.210 pcf	Iy		263.672 in^4
Fc - Perp		625.0 psi					
E : Modulus of Elasticity . . .		x-x Bending	y-y Bending	Axial			
		Basic	1,600.0	1,600.0	1,600.0 ksi		
		Minimum	580.0	580.0			
Allow Stress Modification Factors							
Cf or Cv for Bending 1.0							
Cf or Cv for Compression 1.0							
Cf or Cv for Tension 1.0							
Cm : Wet Use Factor 1.0							
Ct : Temperature Factor 1.0							
Cfu : Flat Use Factor 1.0							
Kf : Built-up columns 1.0							
Use Cr : Repetitive ? No							
Brace condition for deflection (buckling) along columns :							
X-X (width) axis : Unbraced Length for buckling ABOUT Y-Y Axis = 9.813 ft, K =							
Y-Y (depth) axis : Unbraced Length for buckling ABOUT X-X Axis = 9.813 ft, K =							

### Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Column self weight included : 119.634 lbs \* Dead Load Factor

AXIAL LOADS ...

Load @ top of Column: Axial Load at 9.813 ft, D = 30.615 k

### DESIGN SUMMARY

#### Bending & Shear Check Results

PASS	Max. Axial+Bending Stress Ratio =	0.7378 : 1	Maximum SERVICE Lateral Load Reactions . .			
	Load Combination	+D+H	Top along Y-Y	0.0 k	Bottom along Y-Y	0.0 k
	Governing NDS Formula	Comp Only, $f_c/F_c'$	Top along X-X	0.0 k	Bottom along X-X	0.0 k
	Location of max.above base	0.0 ft	Maximum SERVICE Load Lateral Deflections . .			
	At maximum location values are ...		Along Y-Y	0.0 in at 0.0 ft above base		
	Applied Axial	30.735 k		for load combination : n/a		
	Applied Mx	0.0 k-ft	Along X-X	0.0 in at 0.0 ft above base		
	Applied My	0.0 k-ft		for load combination : n/a		
	Fc : Allowable	740.58 psi	Other Factors used to calculate allowable stresses ...			
PASS	Maximum Shear Stress Ratio =	0.0 : 1		Bending	Compression	Tension
	Load Combination	+D+S+H				
	Location of max.above base	9.813 ft				
	Applied Design Shear	0.0 psi				
	Allowable Shear	195.50 psi				

### Load Combination Results

Load Combination	C <sub>D</sub>	C <sub>P</sub>	Maximum Axial + Bending Stress Ratios			Maximum Shear Ratios		
			Stress Ratio	Status	Location	Stress Ratio	Status	Location
+D+H	0.900	0.890	0.7378	PASS	0.0 ft	0.0	PASS	9.813 ft
+D+L+H	1.000	0.874	0.6756	PASS	0.0 ft	0.0	PASS	9.813 ft
+D+Lr+H	1.250	0.834	0.5666	PASS	0.0 ft	0.0	PASS	9.813 ft
+D+S+H	1.150	0.850	0.6039	PASS	0.0 ft	0.0	PASS	9.813 ft

### Maximum Reactions

Note: Only non-zero reactions are listed.

Load Combination	X-X Axis Reaction		k	Y-Y Axis Reaction		Axial Reaction	My - End Moments		Mx - End Moments	
	@ Base	@ Top		@ Base	@ Top		@ Base	@ Top	@ Base	@ Top
+D+H						30.735				
+D+L+H						30.735				
+D+Lr+H						30.735				

5/17/20

## Wood Column

Lic. #: KW-05007984

DESCRIPTION: 9'-9.75" Column

### Maximum Reactions

Note: Only non-zero reactions are listed.

Load Combination	X-X Axis Reaction		k	Y-Y Axis Reaction		Axial Reaction	My - End Moments		k-ft	Mx - End Moments	
	@ Base	@ Top		@ Base	@ Top	@ Base	@ Base	@ Top		@ Base	@ Top
+D+S+H						30.735					
+D+0.750Lr+0.750L+H						30.735					
+D+0.750L+0.750S+H						30.735					
+D+0.60W+H						30.735					
+D+0.750Lr+0.450W+H						30.735					
+D+0.750S+0.450W+H						30.735					
+0.60D+0.60W+0.60H						18.441					
+D+0.70E+0.60H						30.735					
+D+0.750L+0.750S+0.5250E+H						30.735					
+0.60D+0.70E+H						18.441					
D Only						30.735					
Lr Only											
L Only											
S Only											
W Only											
E Only											
H Only											

### Maximum Deflections for Load Combinations

Load Combination	Max. X-X Deflection		Distance	Max. Y-Y Deflection		Distance
+D+H	0.0000 in	0.000 ft		0.000 in	0.000 ft	
+D+L+H	0.0000 in	0.000 ft		0.000 in	0.000 ft	
+D+Lr+H	0.0000 in	0.000 ft		0.000 in	0.000 ft	
+D+S+H	0.0000 in	0.000 ft		0.000 in	0.000 ft	
+D+0.750Lr+0.750L+H	0.0000 in	0.000 ft		0.000 in	0.000 ft	
+D+0.750L+0.750S+H	0.0000 in	0.000 ft		0.000 in	0.000 ft	
+D+0.60W+H	0.0000 in	0.000 ft		0.000 in	0.000 ft	
+D+0.750Lr+0.450W+H	0.0000 in	0.000 ft		0.000 in	0.000 ft	
+D+0.750S+0.450W+H	0.0000 in	0.000 ft		0.000 in	0.000 ft	
+0.60D+0.60W+0.60H	0.0000 in	0.000 ft		0.000 in	0.000 ft	
+D+0.70E+0.60H	0.0000 in	0.000 ft		0.000 in	0.000 ft	
+D+0.750L+0.750S+0.5250E+H	0.0000 in	0.000 ft		0.000 in	0.000 ft	
+0.60D+0.70E+H	0.0000 in	0.000 ft		0.000 in	0.000 ft	
D Only	0.0000 in	0.000 ft		0.000 in	0.000 ft	
Lr Only	0.0000 in	0.000 ft		0.000 in	0.000 ft	
L Only	0.0000 in	0.000 ft		0.000 in	0.000 ft	
S Only	0.0000 in	0.000 ft		0.000 in	0.000 ft	
W Only	0.0000 in	0.000 ft		0.000 in	0.000 ft	
E Only	0.0000 in	0.000 ft		0.000 in	0.000 ft	
H Only	0.0000 in	0.000 ft		0.000 in	0.000 ft	

## Wood Column

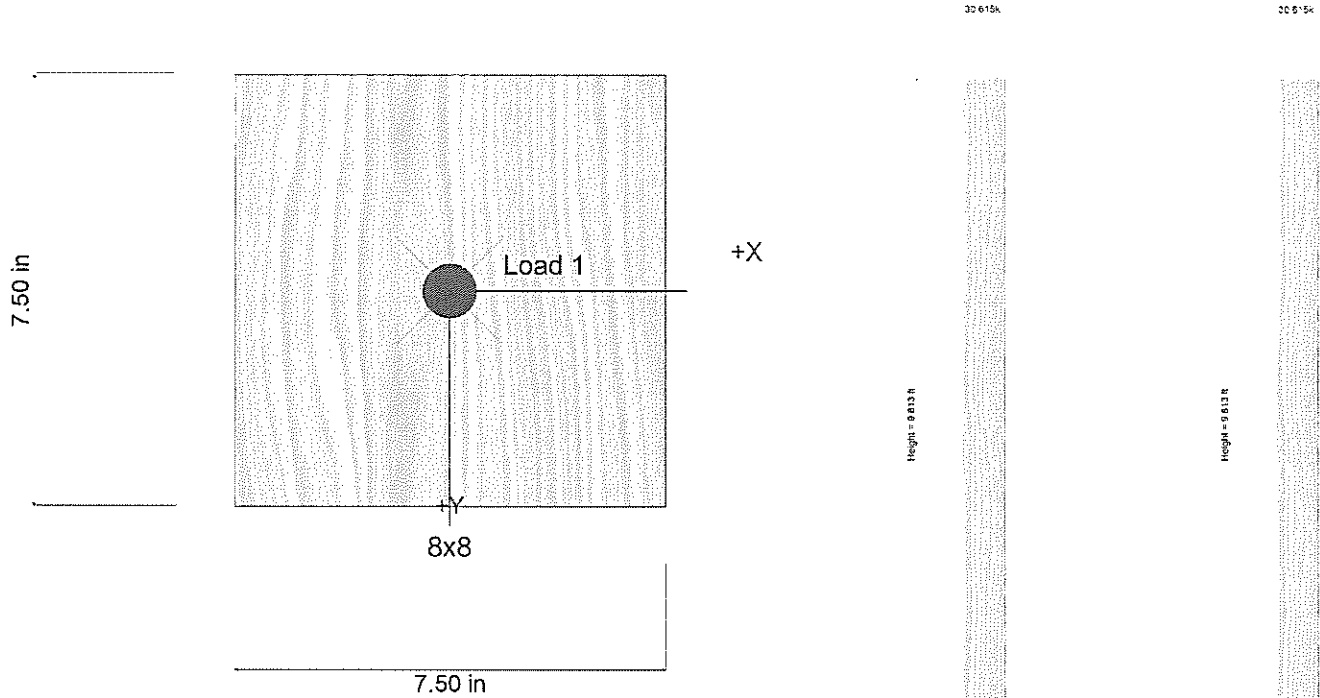
Lic. #: KW-06007984

File = C:\Users\MATTVA~1\Desktop\BILLST~1\calcs.ec6  
Software copyright ENERCALC, INC. 1983-2019, Build:10.19.1.30

BK ENGINEERS INC

DESCRIPTION: 9'-9.75" Column

### Sketches





# 1410 NW Johnson Street

## Engineering Judgement Report #1

### Protection of 2-hour Rated Column

Client Name: Barry R. Smith, PC, Architect

Client Address: 715 SW Morrison Street, Suite 909, Portland, OR 97205

Date: 4/4/2019

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# 1 PROJECT OVERVIEW

Barry R. Smith, PC, Architect, is renovating the existing 1410 NW Johnson Street building. The existing building is 3 stories with a basement of Type III-B construction and includes Group F-2 occupancy. An NFPA 13 fire sprinkler system is provided throughout.

Code Unlimited has been asked to provide engineering analysis for the fire protection of a column member adjacent to the west stair to ensure 2-hour protection is provided as required by OSSC.

## 2 APPLICABLE CODES, STANDARDS, AND GUIDES

- 2014 Oregon Structural Specialty Code (OSSC)
- Calculating the Fire Resistance of Wood Members and Assemblies Technical Report No. 10 – American Wood Council

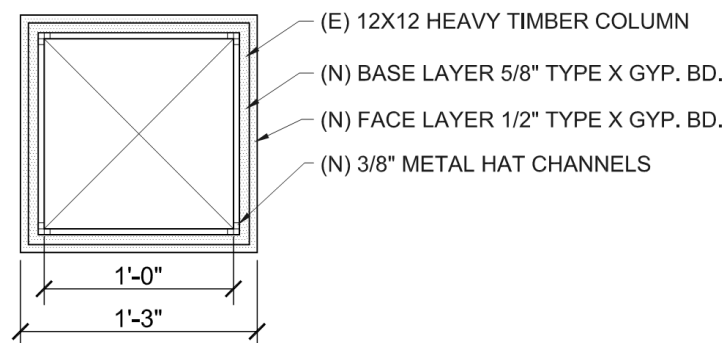
## 3 DISCUSSION

### 3.1 Approach

- The proposed column assembly has been analyzed in accordance with 2014 OSSC §703.3 **Alternative Methods for Determining Fire Resistance.**
- NDS TR-10 is utilized to calculate fire resistance for Type X gypsum board covering a wood member.
- The proposed design has been evaluated by an Oregon Licensed Fire Protection Engineer.

## 4 PROPOSED DESIGN

The 2-hour assembly design is composed of (1) 1/2" face layer and (1) 5/8" base layer of Type "X" gypsum wallboard wrapped around 3/8" metal hat channels which are attached to the greater than or equal to 12" x 12" in size timber column. Table 1 portrays the assembly design in detail:



*Figure 1. Proposed column assembly detail*

## 5 ASSEMBLY ANALYSIS

There are three technical elements in the assembly design:

- Item 1. Finish materials on fire-exposed side of wall that includes Type X gypsum wallboard
- Item 2. Hat channel and clips to provide extra spacing between the wood member and finish materials for walls
- Item 3. Design equations for unprotected fire-resistant exposed wood members.

The analysis will follow.

**Item 1.** 2014 OSSC Table 722.2.1.4(2) allows for equivalent fire protection time of 40 minutes for 5/8" Type X gypsum wallboard and 25 minutes for 1/2" Type X gypsum wallboard on fire-exposed side of walls. Per NDS TR-10, time assigned to the last layer (1/2" Type X gypsum wallboard) can only be multiplied by 0.50 which, in this case, is equivalent to 12.5 minutes.

**Item 2.** Since we are evaluating this application with respect to a 2-hour timber column rather than wall, 3/8" hat channels will be provided. The hat channels will prevent rapid heat transfer between the gypsum board and timber member, reducing preheating of wood column in a fire event.

**Item 3.** Fire resistance of unprotected/exposed wood column on all four sides permits additional equivalent protection per 2014 OSSC 722.6.3 equation 7-20:

$$2.54Zd \left[ 3 - \left( \frac{d}{b} \right) \right] \text{ for columns which may be exposed to fire on four sides}$$

$b$  = The breadth (width) of a larger side of a column before exposure to fire (inches).

$d$  = The depth of a smaller side of a column before exposure to fire (inches).

$Z$  = Load factor, based on Figure 722.6.3(1).

For this condition,  $b=12$ ,  $d=12$ ,  $Z=1.2$  (100% design load)

The calculation yields an equivalent protection time of 73.15 minutes.

Table 1. Timber column size and summary of equivalency for EJ of 2-hour rated wood column.

Timber Column Size	Assembly Description	Rating Provision	Code Section / Additional Provision	Equivalency
12 x 12 nominal	2-hour	(1) 5/8" Type X Gyp	OSSC Table 722.2.1.4(2)	40 minutes
		(1) 1/2" Type X Gyp	OSSC Table 722.2.1.4(2) / NDS TR-10	+ 12.5 minutes
		3/8" Hat Channels	----	Air Gap
		2.54 [1.2] 12 [3 - 12/12]	OSSC 722.6.3 Eq. 7-20	+ 73.15 minutes
		<b>TOTAL ASSEMBLY</b>	----	<b>Exceeds 2-hour requirements</b>

## 6 SUMMARY

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The 2-hour fire protection of the column will be achieved by the protection provided from the Type X gypsum boards and fire-resistance of the heavy timber column.

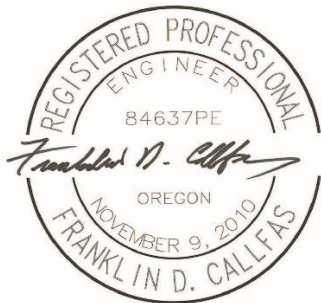
After adding (2) layers (5/8" + 1/2") of Type "X" gypsum wallboard wrap to the face of the assembly an additional 52.5 minutes of equivalent time is added per 2014 OSSC Table 722.2.1.4(2) and NDS TR-10. When we consider the convective and conductive heat transfer reduction by positioning 3/8" hat channels between the wood member and gypsum wrap assembly, the assembly will have a conservative total effective equivalent time of more than 125 minutes. Therefore, the assembly will easily satisfy the design requirements for 2 hours of equivalent protection.

## 7 CONCLUSION

---

The proposed design of the primary structural column meets the code requirement to provide 2-hour fire resistance.

As evaluated in this EJ, the column will maintain a 2-hour fire resistance as required by the OSSC.



*Franklin Callfas*  
Principal/Fire Protection Engineer  
Code Unlimited



# 1410 NW Johnson Street

## Engineering Judgement Report #2

### Protection of 2-hour Rated Beam

Client Name: Barry R. Smith, PC, Architect

Client Address: 715 SW Morrison Street, Suite 909, Portland, OR 97205

Date: 4/4/2019

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## 1 PROJECT OVERVIEW

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Barry R. Smith, PC, Architect, is renovating the existing 1410 NW Johnson Street building. The existing building is 3 stories with a basement of Type III-B construction and includes Group F-2 occupancy. An NFPA 13 fire sprinkler system is provided throughout.

Code Unlimited has been asked to provide engineering analysis for the fire protection of a beam member adjacent to the west stair to ensure 2-hour protection is provided as required by OSSC.

## 2 APPLICABLE CODES, STANDARDS, AND GUIDES

---

- 2014 Oregon Structural Specialty Code (OSSC)
- Calculating the Fire Resistance of Wood Members and Assemblies Technical Report No. 10 – American Wood Council

## 3 DISCUSSION

---

### 3.1 Approach

- The proposed beam assembly has been analyzed in accordance with 2014 OSSC §703.3 **Alternative Methods for Determining Fire Resistance**.
- NDS TR-10 is utilized to calculate fire resistance for Type X gypsum board covering a wood member.
- The proposed design has been evaluated by an Oregon Licensed Fire Protection Engineer.

## 4 PROPOSED DESIGN

The 2-hour assembly design is composed of (1) 1/2" face layer and (1) 5/8" base layer of Type "X" gypsum wallboard wrapped around 3/8" metal hat channels which are attached to the greater than or equal to 8" x 12" nominal in size timber beam. Table 1 portrays the assembly design in detail:

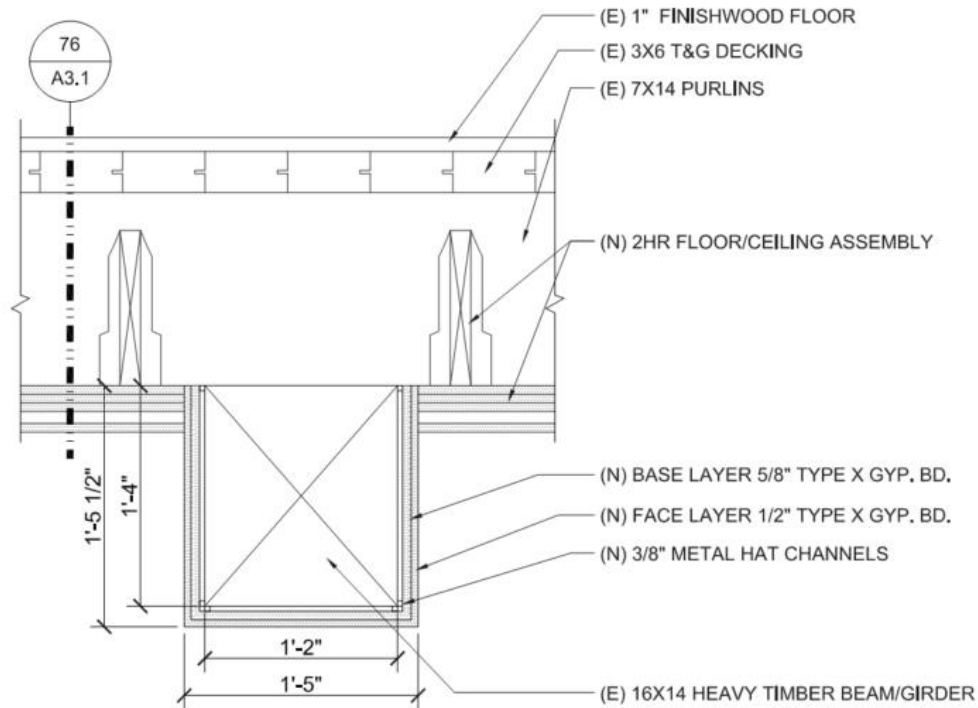


Figure 1. Proposed beam assembly detail

## 5 ASSEMBLY ANALYSIS

There are three technical elements in the assembly design:

- Item 1. Finish materials on fire-exposed side of wall that includes Type X gypsum wallboard
- Item 2. Hat channel and clips to provide extra spacing between the wood member and finish materials for walls
- Item 3. Design equations for unprotected fire-resistant exposed wood members.

The analysis will follow.

**Item 1.** 2014 OSSC Table 722.2.1.4(2) allows for equivalent fire protection time of 40 minutes for 5/8" Type X gypsum wallboard and 25 minutes for 1/2" Type X gypsum wallboard on fire-exposed side of walls. Per NDS TR-10, time assigned to the last layer (1/2" Type X gypsum wallboard) can only be multiplied by 0.50 which, in this case, is equivalent to 12.5 minutes.

**Item 2.** Since we are evaluating this application with respect to a 2-hour timber beam rather than wall, 3/8" hat channels will be provided. The hat channels will prevent rapid heat transfer between the gypsum board and timber member, reducing preheating of wood beam in a fire event.

**Item 3.** Fire resistance of unprotected/exposed wood beam on three sides permits additional equivalent protection, per 2014 OSSC 722.6.3 equation 7-19:

$$2.54Zd \left[ 4 - \left( \frac{d}{b} \right) \right] \text{ for columns which may be exposed to fire on four sides}$$

$b$  = The breadth (width) of a beam before exposure to fire (inches).

$d$  = The depth of a beam before exposure to fire (inches).

$Z$  = Load factor, based on Figure 722.6.3(1).

For this condition,  $b=8$ ,  $d=12$ ,  $Z=1.0$  (100% design load)

The calculation yields an equivalent protection time of 67.7 minutes.

Table 1. Timber beam size and summary of equivalency for EJ of 2-hour rated wood beam.

Timber Beam Size	Assembly Description	Rating Provision	Code Section / Additional Provision	Equivalency
8" x 12" nominal (14" x 16")	2-hour	(1) 5/8" Type X Gyp	OSSC Table 722.2.1.4(2)	40 minutes
		(1) 1/2" Type X Gyp	OSSC Table 722.2.1.4(2) / NDS TR-10	+ 12.5 minutes
		3/8" Hat Channels	----	Air Gap
		2.54 [1.0] 16 [3 - 16/14]	OSSC 722.6.3 Eq. 7-20	+ 67.7 minutes
		<b>TOTAL ASSEMBLY</b>	----	<b>Exceeds 2-hour requirements</b>

## 6 SUMMARY

The 2-hour fire protection of the beam will be achieved by the protection provided from the Type X gypsum boards and fire-resistance of the heavy timber beam.

After adding (2) layers (5/8" + 1/2") of Type "X" gypsum wallboard wrap to the face of the assembly an additional 52.5 minutes of equivalent time is added per 2014 OSSC Table 722.2.1.4(2) and NDS TR-10. When we consider the conductive heat transfer reduction by positioning 3/8" hat channels between the wood member and gypsum wrap assembly, the assembly will have a conservative total effective equivalent time of more than 120 minutes. Therefore, the assembly will satisfy the design requirement for 2 hours of equivalent protection.

## 7 CONCLUSION

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The proposed design of the primary structural beam meets the code requirement to provide 2-hour fire resistance.

As evaluated in this EJ, the beam will maintain a 2-hour fire resistance as required by the OSSC.



EXPIRES 12-31-19

*Franklin Callfas*  
Principal/Fire Protection Engineer  
Code Unlimited



# 1410 NW Johnson Street

## Engineering Judgement Report #3

### Protection of support for 2-hour Rated Beam

Client Name: Barry R. Smith, PC, Architect

Client Address: 715 SW Morrison Street, Suite 909, Portland, OR 97205

Date: 5/1/2019

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  - 5.1 W/D Ratio..... 5
  - 5.2 UL Design No X520 Comparison..... 6
- 6. Summary..... 8
- 7. Conclusion ..... 9

## 1. PROJECT OVERVIEW

Barry R. Smith, PC, Architect, is renovating the existing 1410 NW Johnson Street building. The existing building is 3 stories with a basement of Type III-B construction and includes Group F-2 occupancy. An NFPA 13 fire sprinkler system is provided throughout.

Code Unlimited has been asked to provide engineering analysis for the fire protection of the support for the 2-hour beam assembly as required by OSSC.



Figure 1: Existing condition between the 2-hour column and 2-hour beam assemblies

## 2. APPLICABLE CODES, STANDARDS, AND GUIDES

- 2014 Oregon Structural Specialty Code (OSSC) including the recently adopted Appendix N.

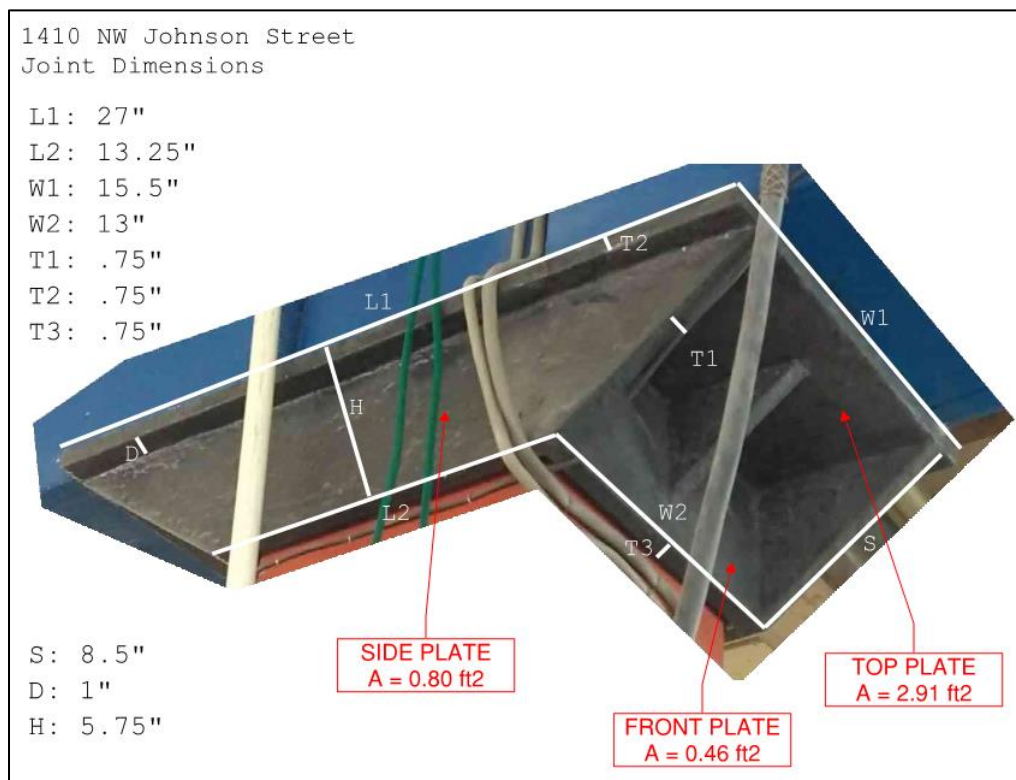
## 3. DISCUSSION

### 3.1 Approach

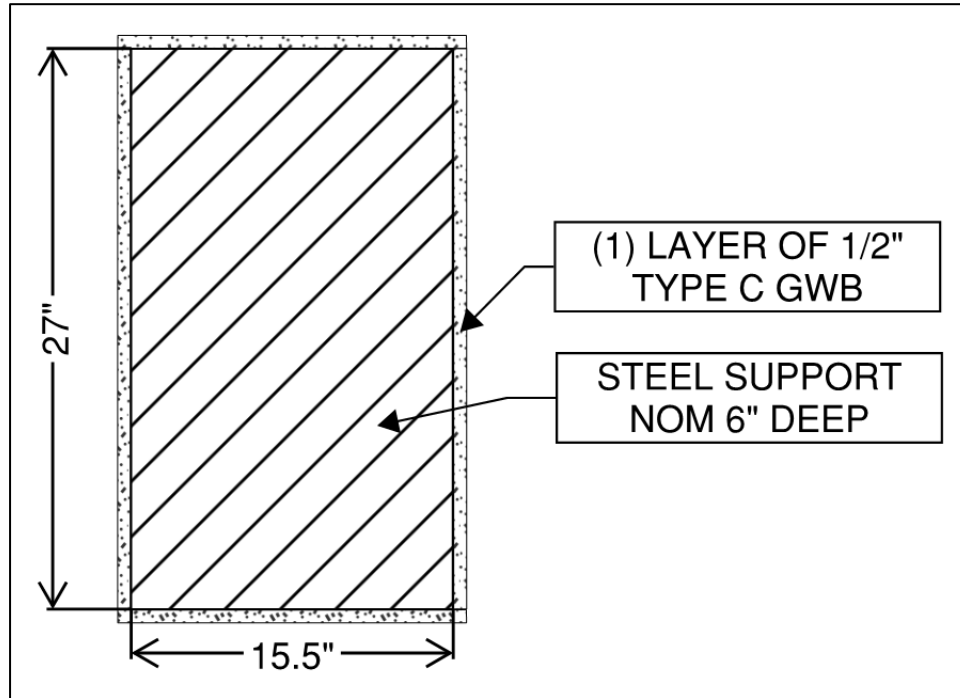
- The proposed assembly has been analyzed in accordance with 2014 OSSC Section 703.3 **Alternative Methods for Determining Fire Resistance**.
- The fire protection has been compared against a 2-hour fire rated column, UL Design No. X520.
- Portions of the tested assembly are modified to suit the unique design condition. The modification is analyzed for equivalency using published fire test data and accepted fire science principles.

## 4. PROPOSED DESIGN

The proposed 2-hour assembly design utilizes (1) 1/2" thick layer of Type C gypsum wallboard wrapped around a steel support assembly which connects 2-hour rated column and beam. The steel member protection is compared to a 2-hour fire rated column per UL X520. The steel is a continuation of the wood column below and requires equivalent protection to a tested assembly tested per ASTM E119 / UL 263. The provided fire resistance will be based on the UL assembly comparison per OSSC Section 703.3. Table 1 portrays the assembly design in detail:



*Figure 2: Dimensions of existing steel member.*



*Figure 3: Proposed protection of steel joint, plan view.*

## 5. ASSEMBLY ANALYSIS

### 5.1 W/D Ratio

The calculated W/D ratio of the steel member is determined for comparison of inherent fire-resistance against the tested column. The W/D value is a ratio between the linear weight of the steel (W), and the perimeter exposed to fire (D). The linear weight of the existing support member is determined with the known density of  $\frac{3}{4}$ " nominal thick steel plates ( 30.60 lbs/ft<sup>2</sup> ) (Engineering Toolbox *Steel Plates – Size and Weight*, 2009).

#### Joint Weight, using surface areas in Figure 2

Top plate: 30.60 lbs/ft<sup>2</sup> x 2.91 ft<sup>2</sup> = 89.05 lbs

Side plates: 30.60 lbs/ft<sup>2</sup> x (0.80 ft<sup>2</sup> x 2) = 48.96 lbs

Front and back plates: 30.60 lbs/ft<sup>2</sup> x (0.46 x 2) = 28.15 lbs

Approximate total weight = 166.16 lbs

Distributed across length of L1 = 27" = 2.25 ft:

166.16 lbs / 2.25 ft = **73.85 lbs/ft**

#### Heated Perimeter

Nominal depth x 4 sides = 6.75 in. x 2 = **13.5 in.**

Calculated W/D ratio = **5.47**

The minimum W/D ratio per the tested UL X520 (Figure 5) is:

W14x228 W/D = 2.44

Wide Flange Steel Specifications		
Steel Size	W/D	HP/A
W12X279	3.48	39
W14X311	3.26	41
W12X252	3.19	42
W14X283	3.00	45
W12X230	2.94	46
W14X257	2.75	49
W12X210	2.72	49
W14X233	2.52	53
W14X228	2.44	55

*Figure 4: W/D ratio per UL X520.*

## 5.2 UL Design No X520 Comparison

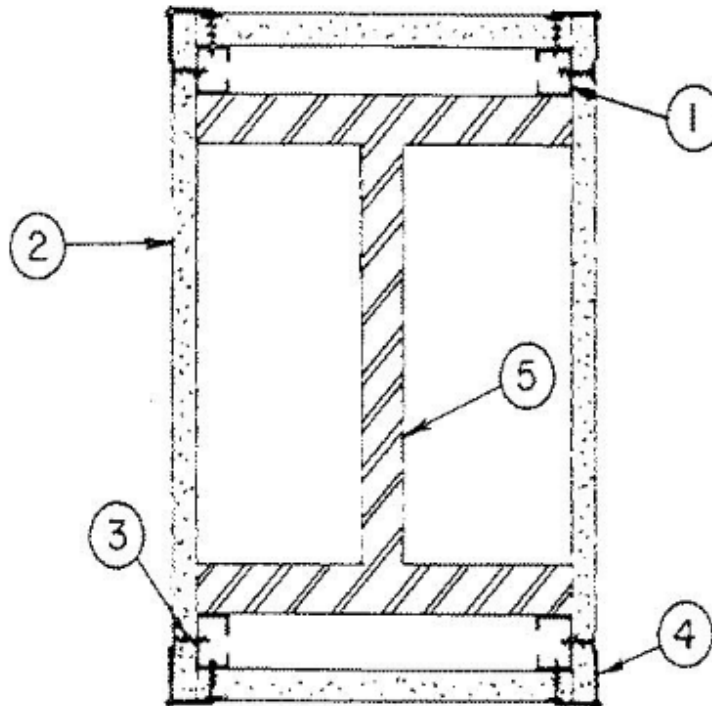
The proposed is a steel assembly, protected with (1) layer of 1/2" Type C gypsum board. It is compared to the 2-hour fire rated column per the tested assembly UL X520 as shown below.

**Design No. X520**

October 24, 2017

Rating — 2 Hr.

\* Indicates such products shall bear the UL or cUL Certification Mark for jurisdictions employing the UL or cUL Certification (such as Canada), respectively.



1. **Steel Studs** — 1-5/8 in. wide with leg dimensions of 1-5/16 and 1-7/16 in. with a 1/4 in. folded flange in legs fabricated from 25 MSG galv steel, 3/4 by 1-3/4 in. rectangular cutouts punched 8 and 16 in. from the ends. Steel stud cut 1/2 in. less in length than assembly height. Alternate Construction, **Steel Framing Members\*** — Clips attached to column flange 4 ft. OC and 1-1/4 in. from the top and bottom of column. 1-1/4 in. by 1-1/4 in. 28 MSG angle laid in place over clip. Angle cut 1 in. less in length than assembly height.  
**JOHN WAGNER ASSOCIATES INC, DBA GRABBER** — Types CB, CB1 Clips.

2. **Gypsum Board\*** — 1/2 in. thick, one layer. Nom 3/32 in. thick gypsum veneer plaster may be applied to the entire surface of Classified veneer baseboard.  
**ACADIA DRYWALL SUPPLIES LTD** — Type C.

**AMERICAN GYPSUM CO** — Type AG-C

**CERTAINTED GYPSUM INC** — Type FRPC, SF3 or Type C.

**CONTINENTAL BUILDING PRODUCTS OPERATING CO, L L C** — Type LGFC-C/A.

**GEORGIA-PACIFIC GYPSUM L L C** — Types 5, C, DAP, DA, DAPC, TG-C.

**NATIONAL GYPSUM CO** — Types -eXP-C, FSW-G, FSW-1, FSK-G, FSW-C, FSK-C.

## Joint Protection Engineering Judgement Report

PABCO BUILDING PRODUCTS L L C, DBA PABCO GYPSUM — Types PG-3, PG-C.

THAI GYPSUM PRODUCTS PCL — Type C.

3. Screws — 1 in. long self-drilling, self-tapping steel screws, spaced vertically 12 in. O.C.

4. Corner Beads — No. 28 MSG galv steel, 1-1/4-in. legs attached to wallboard by crimping spaced 6 in. O.C.

5. Steel Column — Min size of column, a W14X228, with outside dimensions of 16 by 15-7/8 in. with a flange thickness of 1-11/16 in., a web thickness of 1-1/16 in., and a cross-sectional area of 67.06 sq in.

\* Indicates such products shall bear the UL or cUL Certification Mark for jurisdictions employing the UL or cUL Certification (such as Canada), respectively.

Last Updated on 2017-10-24

Figure 5: UL X520.

Table 1: Comparison between the proposed design and the 2-hour fire rated UL X520 assembly

Element	UL Assembly Design No. X520	Proposed Design
1. Steel Member	Steel Column: W14x228 (W/D = 2.44 – Column) (Figures 4 and 5)	Steel Support (W/D = 5.47) (Figure 1 and Section 5.1) <b>Significantly Higher Inherent Fire-Resistance</b>
2. Gypsum Board	<b>1/2 in. thick, one layer.</b> Nom 3/32 in. thick gypsum veneer plaster may be applied to the entire surface of Classified veneer baseboard.	One <b>(1) layer of 1/2” thick</b> Type C gypsum board wrapped around the joint to provide encasement protection. <b>Equivalent</b>
<b>Fire-Resistance Rating</b>	<b>2-Hour</b>	<b>2-Hour (minimum)</b>

## 6. SUMMARY

The 2-hour fire protection of the steel connection will be achieved by a GWB membrane provided through 1 layer of Type C gypsum board and the inherent fire-resistance of steel, as compared to UL X520 (Table 1).

While evaluating fire resistance requirement of members, different sized beam and columns are compared against each other through a factor referred to as the W/D Ratio. The weight per unit length of a member is divided by the length of exposed heated perimeter area to determine the inherent fire resistance of a member. Lower W/D ratios correspond with thinner steel members that will be subject to earlier failure when heated.

During this evaluation, an encased column assembly UL X520 was referenced, where the minimum required W/D ratio (2.44) is far less than the proposed design W/D ratio (5.47). The proposed support member is protected with ½" Type C gypsum, which is the equivalent protection used in UL X520. The greater W/D ratio and equivalent Type C gypsum board encasement ensures a minimum of 2-hour fire-resistance as compared to the 2-hour fire rated column assembly, UL X520.

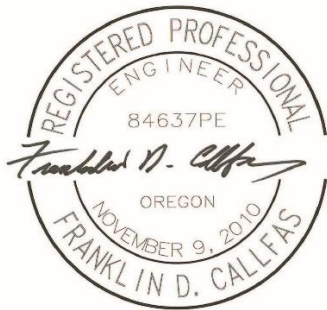
Adjacent Beam and Column protection will utilize 2-hour assemblies as provided in EJ#1 an EJ#2 (See Appeal #20220).

## 7. CONCLUSION

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The proposed assembly meets the code requirement to provide 2-hour fire-resistance and continuous fire protection of the adjacent 2-hour rated beam and column. The proposed design provides greater fire-resistance compared to the tested W-column in UL X520.

The significantly greater inherent fire-resistance of the steel member in addition to the equivalent Type C gypsum board encasement per UL X520 exceeds the protection of the tested column. Therefore, the proposed design for the steel support member encased with 1/2" Type C gypsum board will exceed the required minimum 2-hour fire-resistance required by code, as detailed in the report.



EXPIRES 12-31-19

*Franklin Callfas*  
Principal/Fire Protection Engineer  
Code Unlimited

Building is equipped with an automatic sprinkler system and needs upgrading to current NFPA 13 standards.

There are no combustible concealed attic spaces.

Where non-rated interior glass relite and doors are used, a 2HR rated fire curtain is provide.

RESPONSE: A Building Code appeal is required for substituting 2HR fire curtains in lieu of one-hour fire resistive construction.

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**Reason for alternative** The alternate gives the Owner flexibility to visually identify tenant access from egress components.

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## APPEAL DECISION

**Extension of stair enclosures: Hold for additional information.**

**Appellant may contact John Butler (503 823-7339) with questions.**



JOHNSON STREET ELEVATION

**1410 SW JOHNSON STREET - PORTLAND OR**

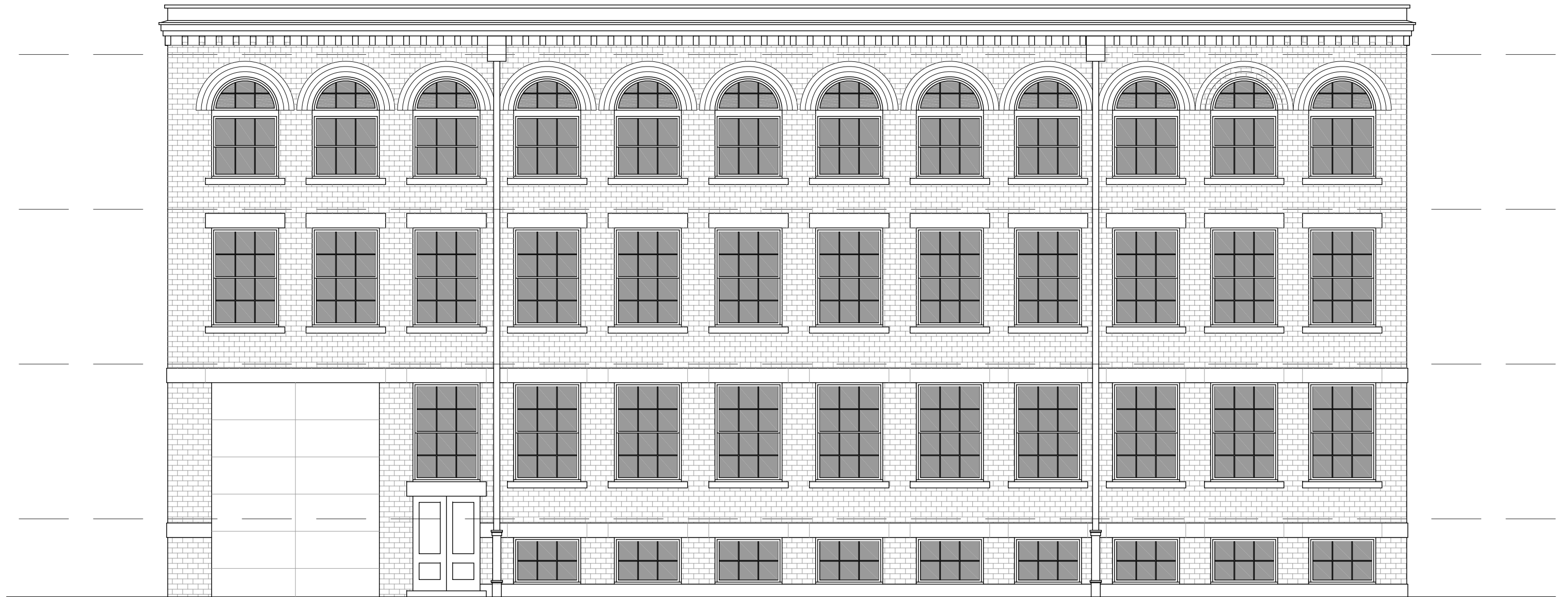


2019-01-30

DRAWINGS BASED ON AS BUILT PLANS - FIELD VERIFY ALL DIMENSIONS

**BARRY R SMITH, PC Architect**  
 715 SW MORRISON STREET SUITE 909  
 PORTLAND OR 97205 503.295.6261 [www.barrysmith.com](http://www.barrysmith.com)





10TH AVENUE ELEVATION

**1410 SW JOHNSON STREET - PORTLAND OR**



20FT

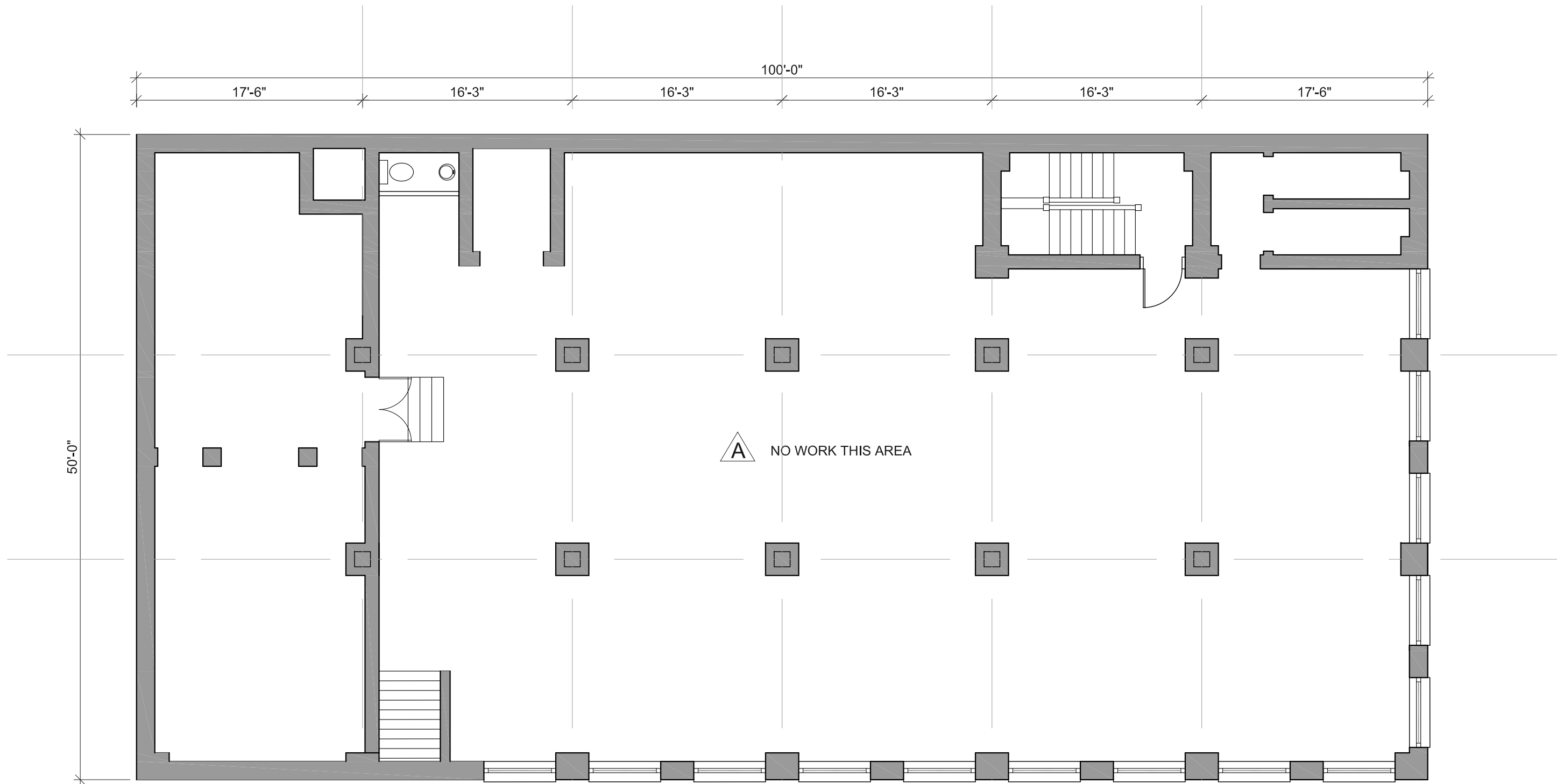


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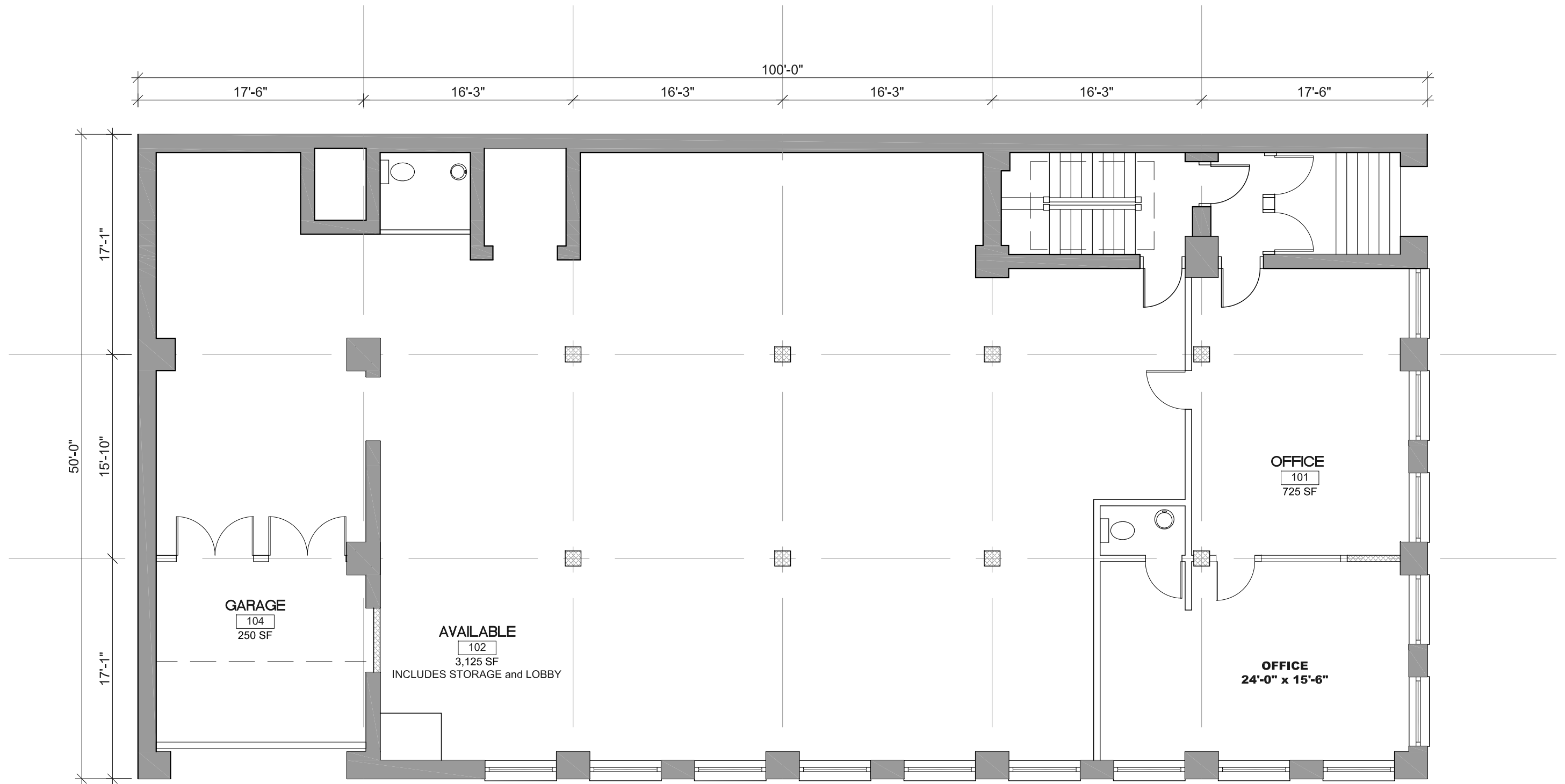
BASEMENT FLOOR PLAN  
**1410 SW JOHNSON STREET - PORTLAND OR**



2019-01-30  
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FIRST FLOOR PLAN - EXISTING CONDITIONS  
**1410 SW JOHNSON STREET - PORTLAND OR**

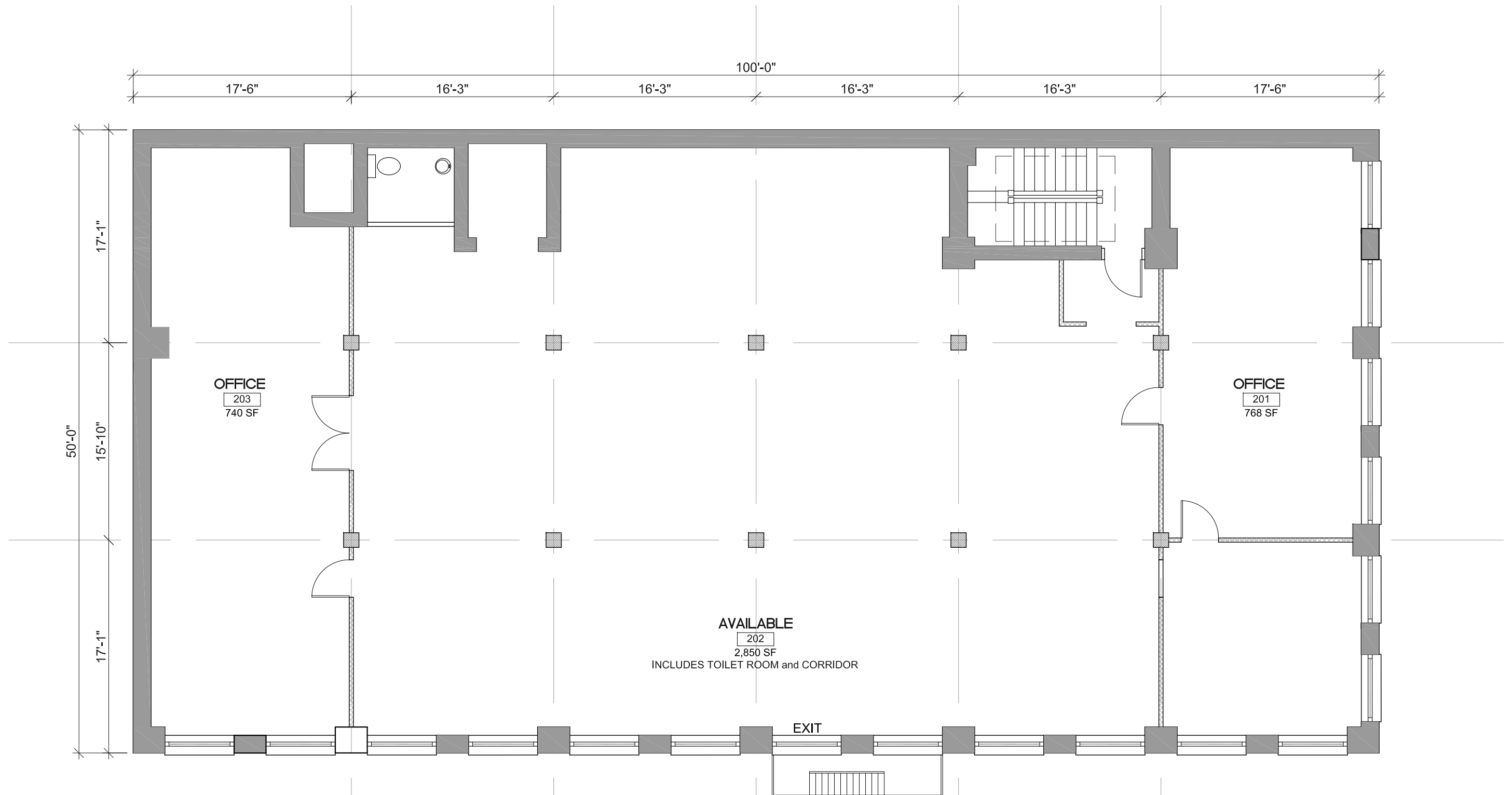


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SECOND FLOOR - EXISTING CONDITIONS  
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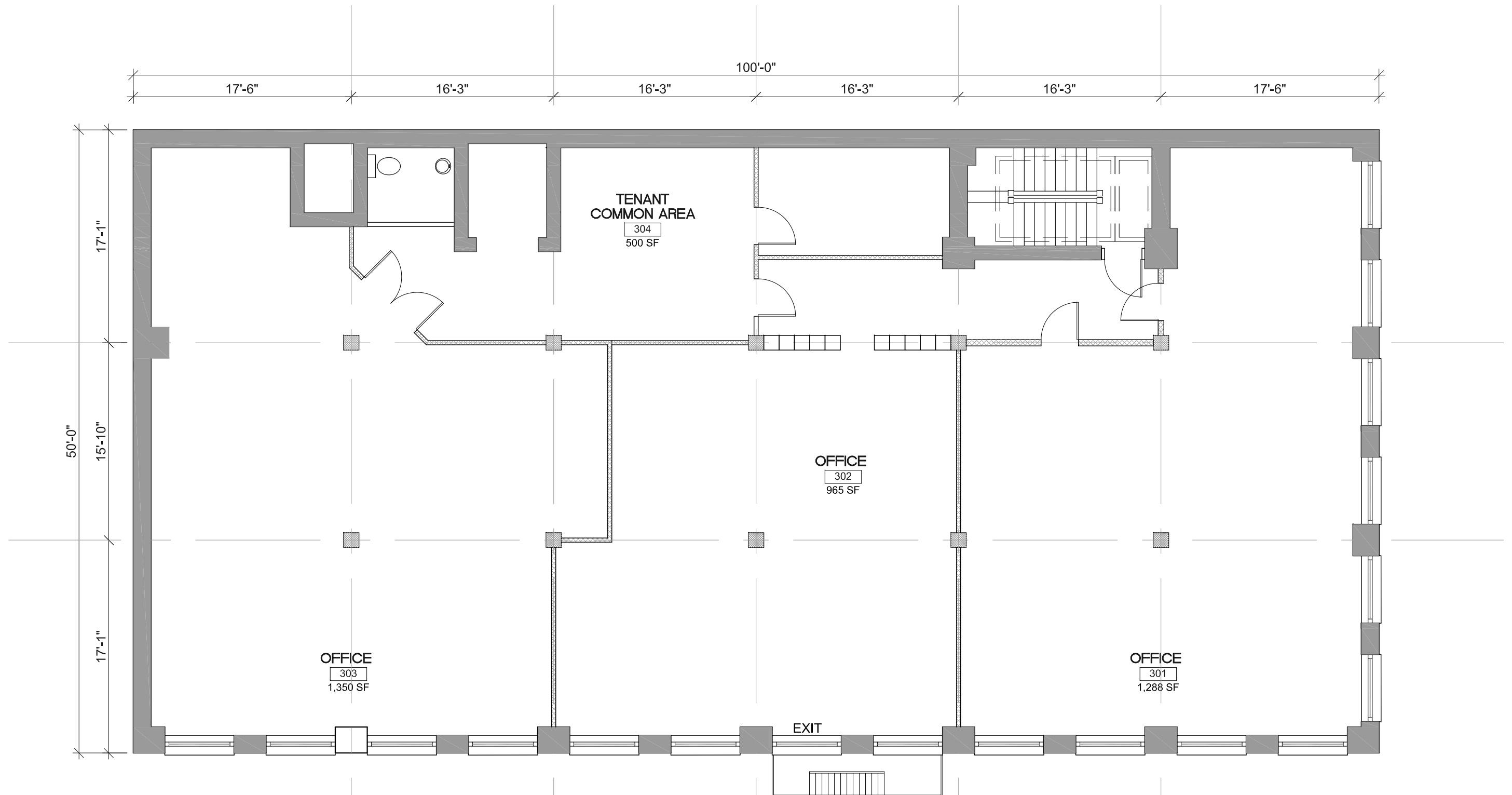


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THIRD FLOOR - EXISTING CONDITIONS  
**1410 SW JOHNSON STREET - PORTLAND OR**

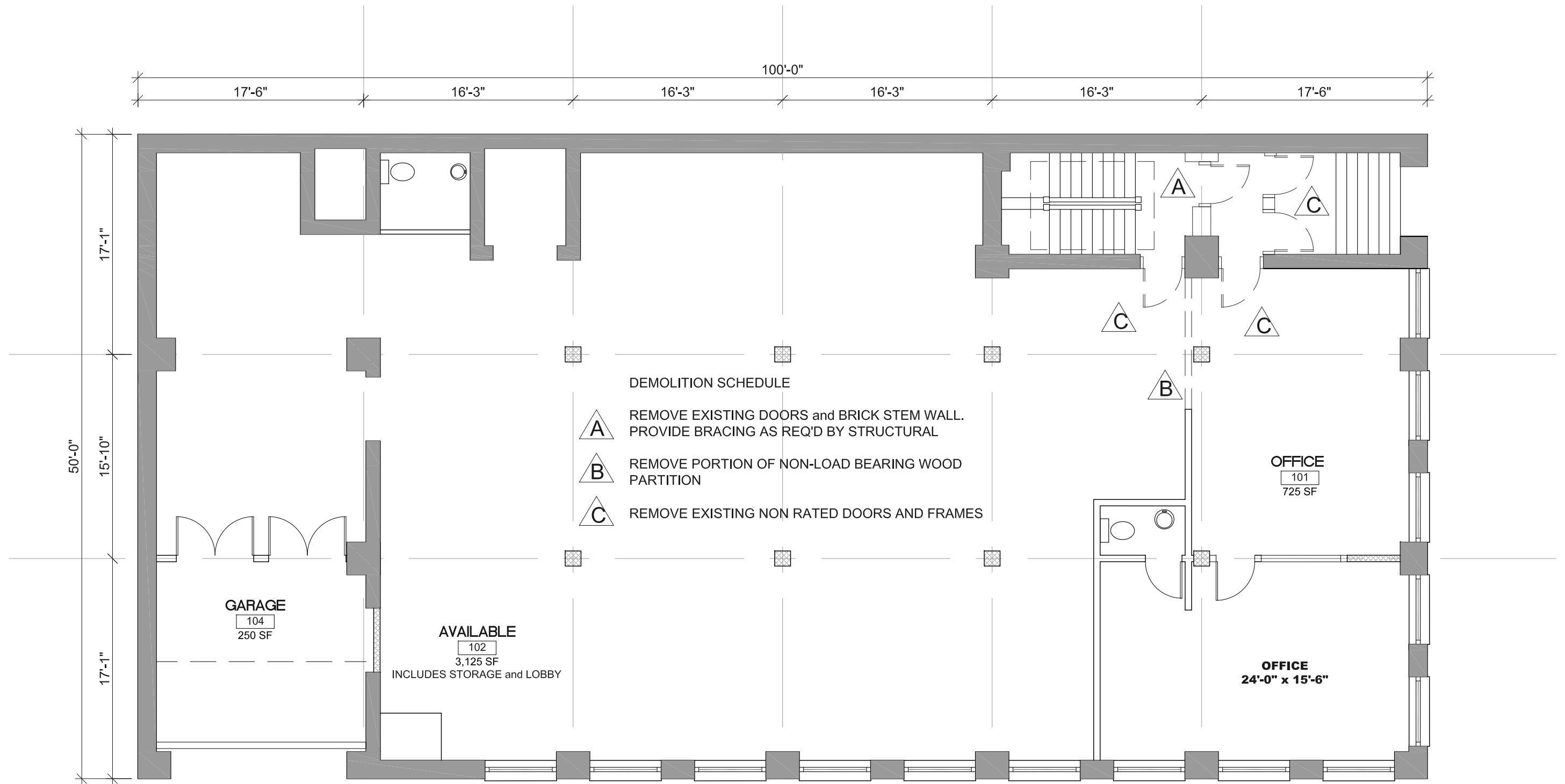


2019-01-30

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FIRST FLOOR - DEMOLITION PLAN

**1410 SW JOHNSON STREET - PORTLAND OR**

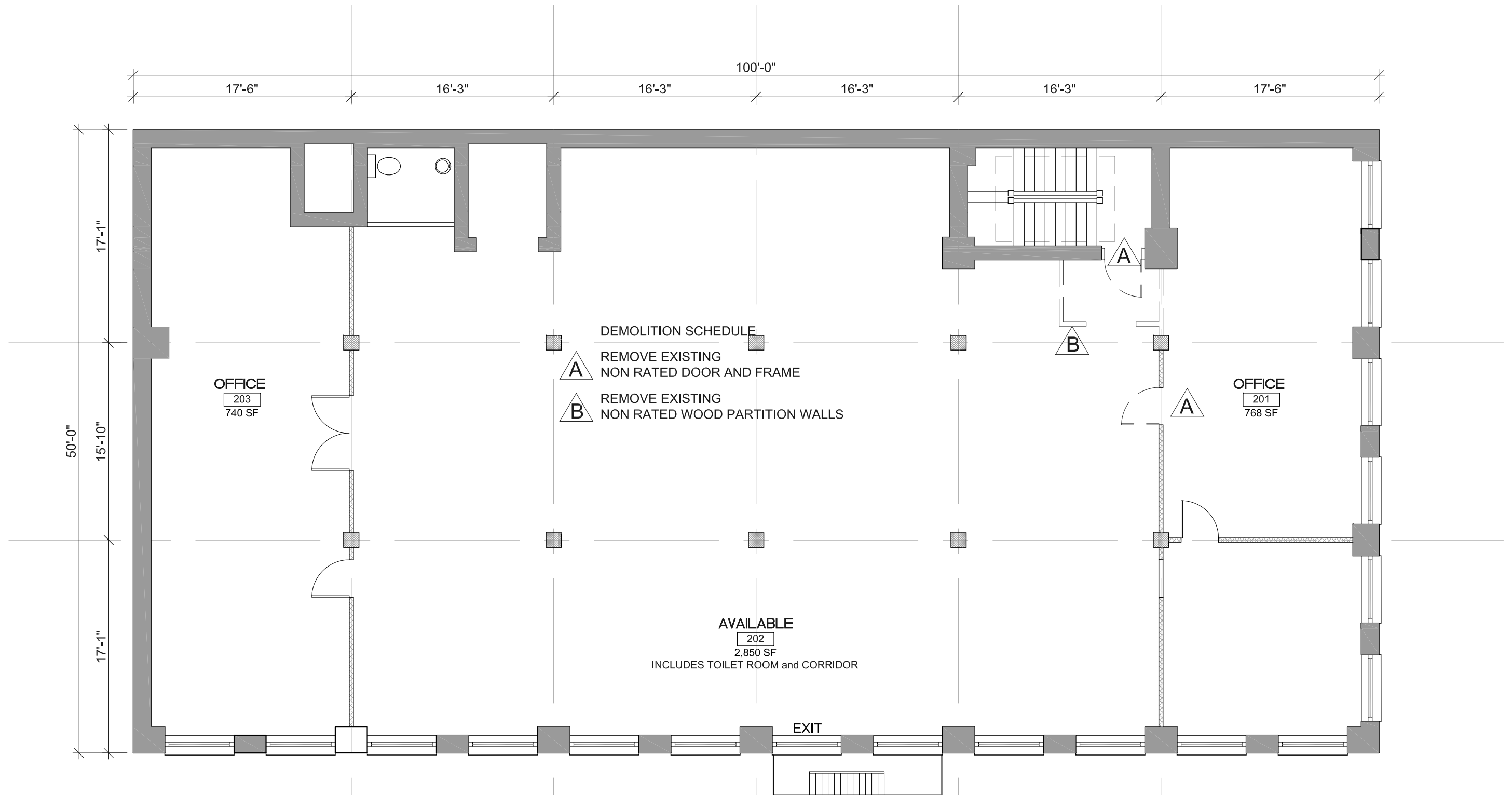


2019-01-30

DRAWINGS BASED ON AS BUILT PLANS - FIELD VERIFY ALL DIMENSIONS

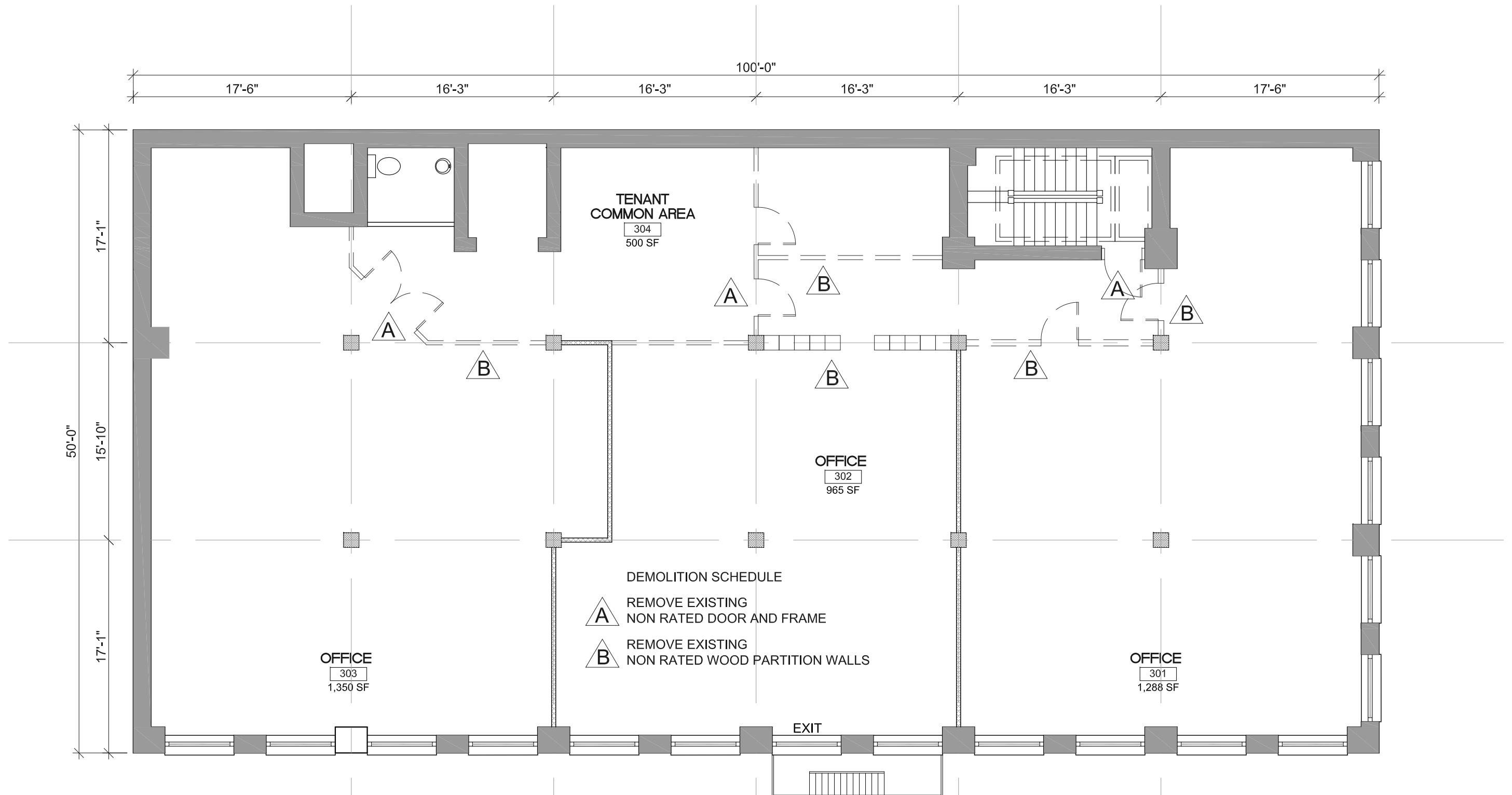
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SECOND FLOOR - DEMOLITION PLAN  
**1410 SW JOHNSON STREET - PORTLAND OR**





THIRD FLOOR - DEMOLITION PLAN  
**1410 SW JOHNSON STREET - PORTLAND OR**

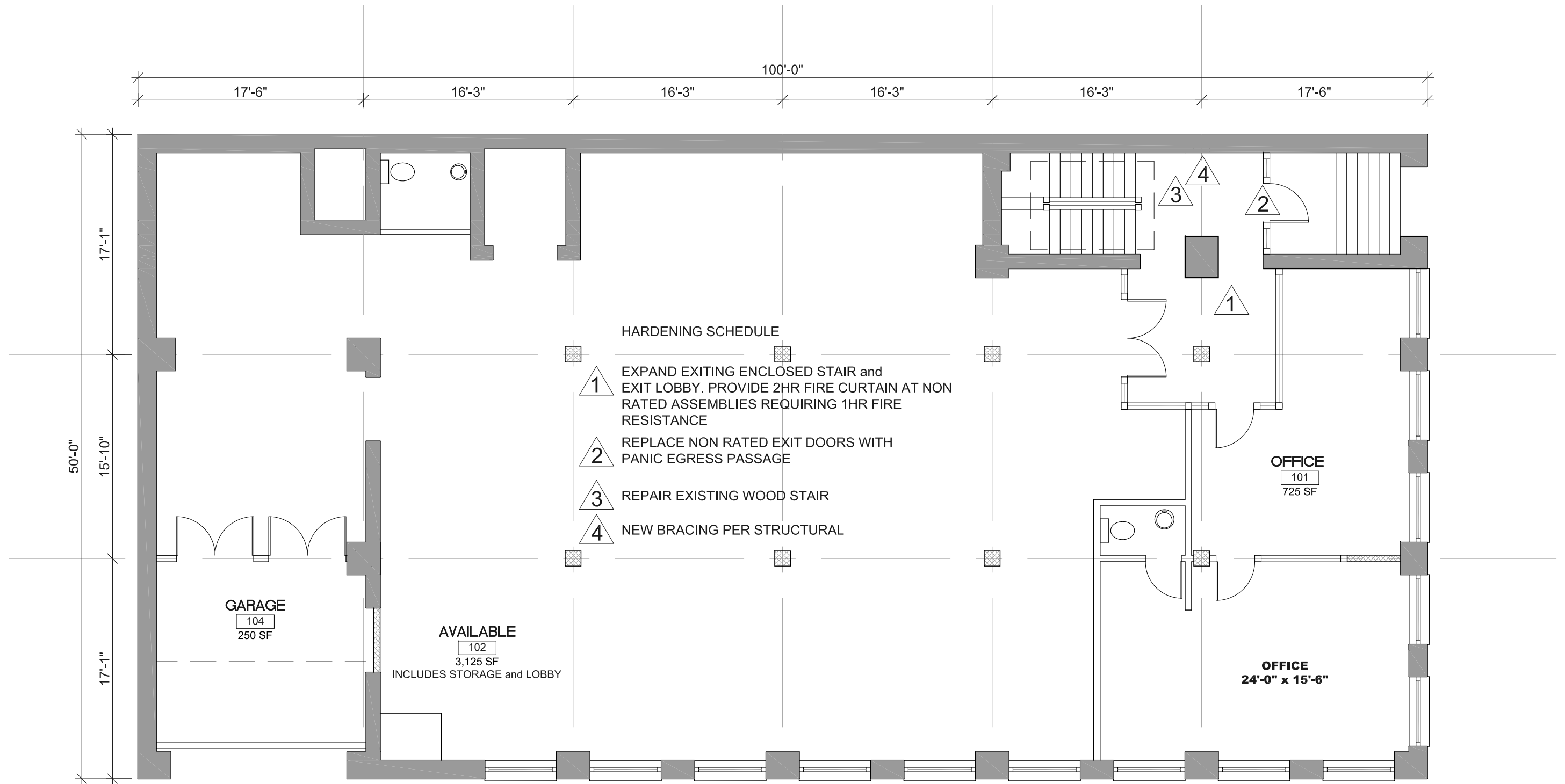


2019-01-30

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FIRST FLOOR - HARDENING PLAN

**1410 SW JOHNSON STREET - PORTLAND OR**

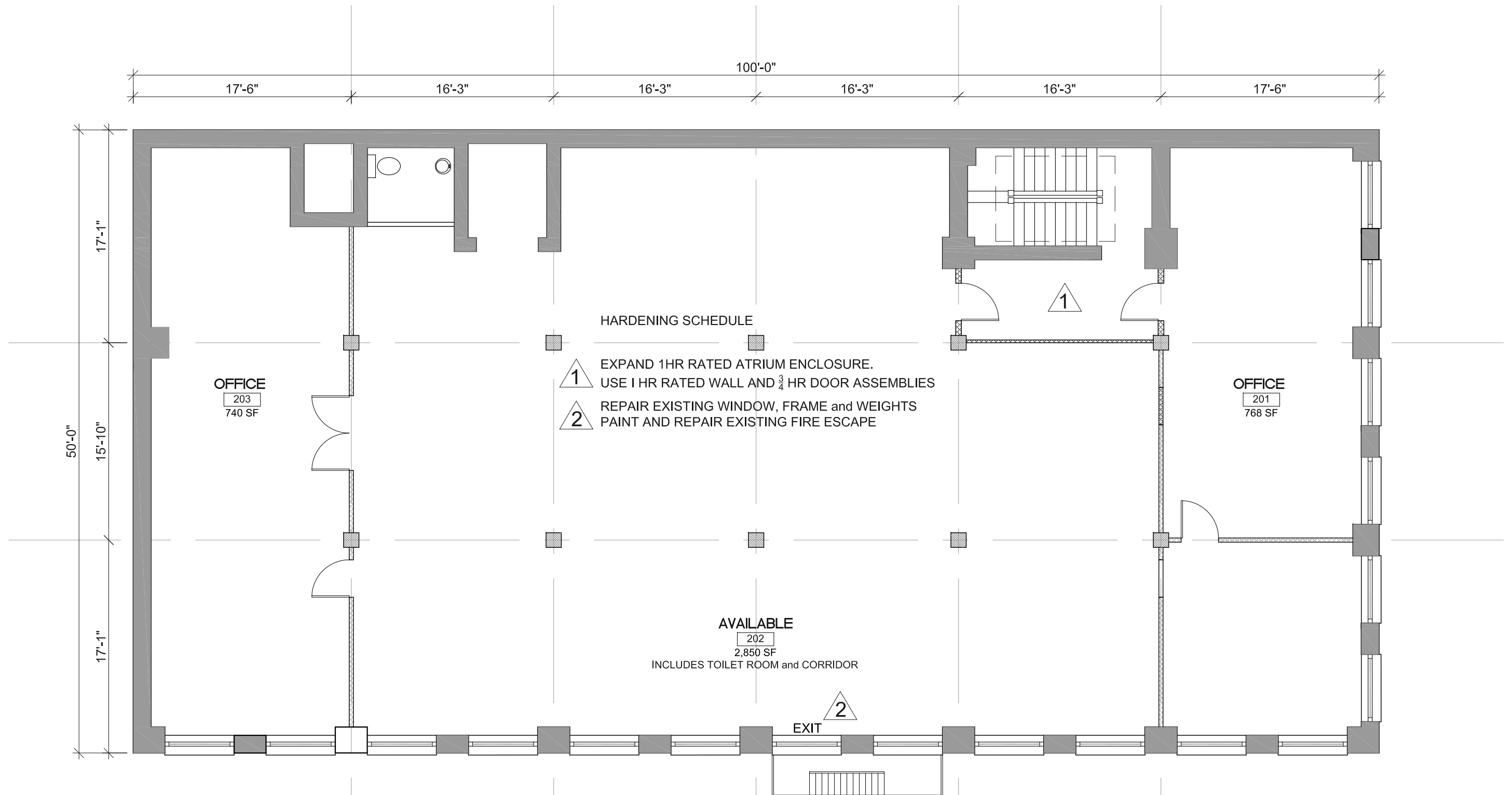


2019-01-30

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SECOND FLOOR - HARDENING PLAN  
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