19-205139 REV 01 RS

STRUCTURAL CALCULATIONS REVISONS TO CONCRETE STRENGTH

PROJECT: Kramer / Falk Remodel 4145 SW Agate Lane Portland, OR 97239

for

Eric Butler Design 2400 SE Holgate Blvd Portland, OR 97202





James G. Pierson, Inc. Consulting Structural Engineers 610 S.W. ALDER SUITE 918 PORTLAND, OR. 97205 (503) 226-1286 FAX 226-3130

May 9, 2022

REMODEL / ADDITION

Project located in Portland, Oregon

GENERAL DESIGN LOADS:

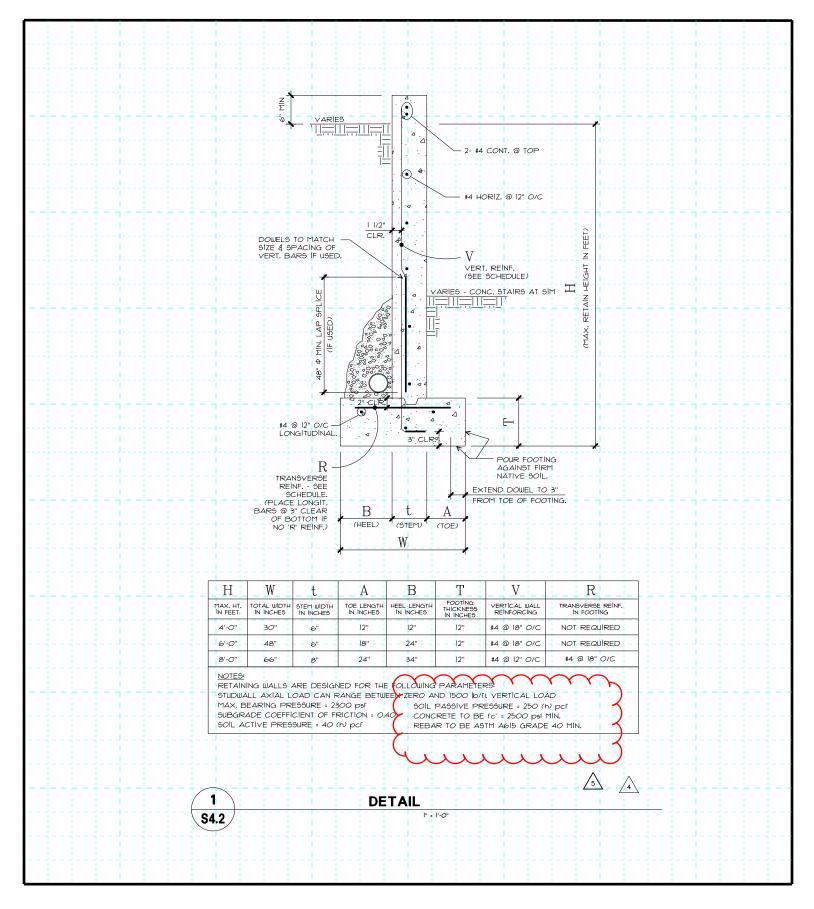
Project is designed in accord with requirements of the 2019 Oregon Structural Specialty Code. For this location the following design parameters apply:

Occupancy Category II Seismic Site Class D, Design Category D Roof Snow Load 25 PSF Roof Dead Load 15 PSF Floor Live Load 40 PSF Floor Dead Load 12 PSF Deck Live Load 60 PSF Wind: 98 MPH EXP C (ASCE 7-16) Allowable Soil Bearing Pressure = 2300 PSF (Per Strata Design dated 10/23/19)

Design Summary:

The following revised calculations are for the house remodel in Portland, Oregon. The design strength of the site retaining walls was changed from 3000 psi to 2500 psi concrete to eliminate the requirement for special inspection (that was not done when built). The 2nd item changed is detail 7/S4.1 for the epoxied dowels to tie the new foundation to existing, These dowels work with our without epoxy and the epoxy was not inspected when installed. As such, no special inspection would be required on project.

The techniques and principles of structural analysis used for these calculations conform to generally accepted standards of the engineering community. These design calculations have been prepared based upon architectural drawings furnished by client.



James G. Pierson, Inc.	Project Kramer/Falk Remodel	Job no.
Consulting Structural Engineers 610 S.W.Alder, Suite 918 Portland, Oregon 97205	Location 4145 SW Agate	Date 5/9/22
	Client Butler Design	Sheet no. Page 3 of 27

James G. Pierson, Inc. 610 SW Alder #918 Portland, OR 97205 503-226-1286 www.jgpierson.com

cense : KW-06056929 cense To : JAMES G. PIERSO	N	Cantilevereu	Retaining Wall Code	e: IBC 2018,A	CI 318-14,TMS 402
Criteria					
Retained Height	=	3.00 ft			
Wall height above soil	=	0.00 ft			
Slope Behind Wall	=	0.00			
Height of Soil over Toe	=	6.00 in			••••
Water height over heel	=	0.0 ft			Bartase
Load Factors					
Building Code	IB	C 2018,ACI			
Dead Load		1.200			
Live Load		1.600			
Earth, H		1.600			
Wind, W		1.000			
Seismic, E		1.000			
Soil Data and Lateral Ear	rth Pressu	re			
Allow Soil Bearing	=	2,300.0 psf	Soil Density, Heel	=	110.00 pcf
Equivalent Fluid Pressure Metho	od		Soil Density, Toe	=	0.00 pcf
Active Heel Pressure	=	40.0 psf/ft	Footing Soil Friction	=	0.400
			Soil height to ignore		
Passive Pressure	=	250.0 psf/ft	for passive pressure	=	12.00 in
Surcharge Loads					
buicharge Loaus					
	= rerturning	0.0 psf	Surcharge Over Toe Used for Sliding & Ove	= erturning	0.0
Surcharge Over Heel Used To Resist Sliding & Ov Axial Load Applied to Ste	erturning		Used for Sliding & Ove		
Surcharge Over Heel	rerturning	0.0 psf 0.0 lbs 0.0 lbs	-	= erturning =	0.0 0.0 in
Surcharge Over Heel Used To Resist Sliding & Ov Axial Load Applied to Ste Axial Dead Load Axial Live Load	em = =	0.0 lbs	Used for Sliding & Ove		
Surcharge Over Heel Used To Resist Sliding & Ov Axial Load Applied to Ste Axial Dead Load Axial Live Load	em = =	0.0 lbs	Used for Sliding & Ove		
Surcharge Over Heel Used To Resist Sliding & Ov Axial Load Applied to Ste Axial Dead Load Axial Live Load Lateral Load Applied to S	em = = Stem	0.0 lbs 0.0 lbs	Used for Sliding & Ove		
Surcharge Over Heel Used To Resist Sliding & Ov Axial Load Applied to Sto Axial Dead Load Axial Live Load Lateral Load Applied to S Lateral Load	em = = Stem = =	0.0 lbs 0.0 lbs 0.0 #/ft 0.00 ft	Used for Sliding & Ove		
Surcharge Over Heel Used To Resist Sliding & Ov Axial Load Applied to Sto Axial Dead Load Axial Live Load -ateral Load Applied to S Lateral Load Height to Top Height to Bottom	em = = Stem	0.0 lbs 0.0 lbs 0.0 #/ft	Used for Sliding & Ove		
Surcharge Over Heel Used To Resist Sliding & Ov Axial Load Applied to Ste Axial Dead Load Axial Live Load Lateral Load Height to Top Height to Bottom Load Type	em = = Stem = = = =	0.0 lbs 0.0 lbs 0.0 #/ft 0.00 ft 0.00 ft	Used for Sliding & Ove		
Surcharge Over Heel Used To Resist Sliding & Ov Axial Load Applied to Ste Axial Dead Load Axial Live Load Lateral Load Height to Top Height to Bottom Load Type	em = = Stem = = = =	0.0 lbs 0.0 lbs 0.0 #/ft 0.00 ft 0.00 ft Wind (W)	Used for Sliding & Ove		
Surcharge Over Heel Used To Resist Sliding & Ov Axial Load Applied to Ste Axial Dead Load Axial Live Load Lateral Load Applied to S Lateral Load Height to Top Height to Bottom Load Type	em = = Stem = = = =	0.0 lbs 0.0 lbs 0.0 #/ft 0.00 ft 0.00 ft Wind (W)	Used for Sliding & Ove		
Surcharge Over Heel Used To Resist Sliding & Over Axial Load Applied to Ster Axial Dead Load Axial Live Load Axial Live Load Axial Live Load Lateral Load Height to Top Height to Bottom Load Type Wind on Exposed Stem (Service Level)	rerturning = = = Stem = = = = =	0.0 lbs 0.0 lbs 0.0 #/ft 0.00 ft 0.00 ft Wind (W) (Service Level)	Used for Sliding & Ove		
Surcharge Over Heel Used To Resist Sliding & Ov Axial Load Applied to Ste Axial Dead Load Axial Live Load Lateral Load Applied to S Lateral Load Height to Top Height to Bottom Load Type Wind on Exposed Stem (Service Level) Adjacent Footing Load	rerturning = = = Stem = = = = =	0.0 lbs 0.0 lbs 0.0 #/ft 0.00 ft 0.00 ft Wind (W) (Service Level)	Used for Sliding & Ove	=	
Surcharge Over Heel Used To Resist Sliding & Over Axial Load Applied to State Axial Dead Load Axial Live Load Axial Live Load Axial Live Load Lateral Load Applied to State Lateral Load Height to Top Height to Bottom Load Type Mind on Exposed Stem (Service Level) Adjacent Footing Load	em = = Stem = = = =	0.0 lbs 0.0 lbs 0.0 lbs 0.0 #/ft 0.00 ft 0.00 ft Wind (W) (Service Level) 0.0 psf	Used for Sliding & Ove	=	0.0 in
Surcharge Over Heel Used To Resist Sliding & Over Axial Load Applied to State Axial Dead Load Axial Live Load Axial Live Load Axial Live Load Lateral Load Applied to State Lateral Load Height to Top Height to Bottom Load Type Mind on Exposed Stem (Service Level) Adjacent Footing Load Footing Width	rerturning = = = Stem = = = = = = = =	0.0 lbs 0.0 lbs 0.0 lbs 0.0 #/ft 0.00 ft 0.00 ft Wind (W) (Service Level) 0.0 psf 0.0 lbs 0.00 ft	Used for Sliding & Ove	= 	0.0 in
Surcharge Over Heel Used To Resist Sliding & Ov Axial Load Applied to Sta Axial Dead Load Axial Live Load Lateral Load Applied to S Lateral Load Height to Top Height to Bottom Load Type Wind on Exposed Stem (Service Level) Adjacent Footing Load	rerturning = = Stem = = = = = = =	0.0 lbs 0.0 lbs 0.0 lbs 0.0 #/ft 0.00 ft 0.00 ft Wind (W) (Service Level) 0.0 psf 0.0 lbs	Used for Sliding & Ove	=	0.0 in

James G. Pierson, Inc. 610 SW Alder #918 Portland, OR 97205 503-226-1286 www.jgpierson.com This Wall in File: X:\Residential Projects\Resider	Project Name/Number : ag Title 4 ft : Dsgnr: Golberg Description Site Retaining Wall sch. ntial Projects 2019\4145 SW Agate - Butler Design\	•	Page : 2 Date: 7 JAN 2020
RetainPro (c) 1987-2019, Build 11.19.11.12 License : KW-06056929 License To : JAMES G. PIERSON	Cantilevered Retaining Wall	Code: IBC 2018,ACI	318-14,TMS 402-16
Earth Pressure Seismic Load			
Method : Triangular			
Load at bottom of Triangular Distribution . Strength-Level)	= 112.000 psf Total Strength-Leve Total Service-Level	l Seismic Load Seismic Load	= 224.000 lbs = 156.800 lbs

License : KW-06056929 License To : JAMES G. PIERSON	Cantilevered Retaining Wall	Code: IBC 2018,ACI 318-14,TMS 402-16
Wall Design Summary		
Stability Ratios		

Stability Ratios		
Overturning	=	2.27 OK
Slab Resists All Sliding !		
Soil Bearing		
Total Bearing Load	=	950 lbs
resultant ecc.	=	4.82 in
Soil Pressure @ Toe	=	746 psf OK
Soil Pressure @ Heel	=	14 psf OK
Allowable	=	2,300 psf
Soil Pressure Less Tha	n Allowable	
ACI Factored @ Toe	=	1,045 psf
ACI Factored @ Heel	=	19 psf
Footing Shear @ Toe	=	2.1 psi OK
Footing Shear @ Heel	=	2.8 psi OK
Allowable	=	75.0 psi

Overturning

Resisting Moments

Resisting Moments	Force	Dist	tance	<u>Moment</u>
Soil Over Heel (above water table, if any)	275.0	lbs	2.08 ft	572.9ft-#
Soil Over Heel (below water table, if any)	0.0			
Water Table	0.0			
Soil Over Heel	275.0		2.08	572.9
Sloped Soil Over Heel	0.0			
Surcharge Over Heel	0.0			
Adjacent Footing Load	0.0			
Axial Dead Load on Stem	0.0			
Axial Live Load on Stem *	0.0			
Soil Over Toe	0.0		0.50	
Surcharge Over Toe	0.0			
Stem Weight(s)	300.0		1.33	400.0
Earth @ Stem Transitions	0.0			
Footing Weight	375.0		1.25	468.8
Key Weight	0.0		2.00	
Vert. Component	0.0			
Total Vertical Loads	950.0	lbs		
Resisting	Moment			1,441.7 ft-#
Eccentric	ity			4.8 in

* Axial live load NOT included in total displayed, or used for overturning or sliding resistance, but is included for soil pressure calculations.

tainPro (c) 1987-2019, Build 11.19.11.12 ense : KW-06056929 cense To : JAMES G. PIERSON	Cantilevered	Retaining Wall	Code: IBC 2018,ACI 318-14,TMS 402-16
Overturning			
Overturning Moments			
Overturning Moments	<u>Force</u>	<u>Distance</u>	Moment
Heel Active Pressure (above water table, if any Heel Active Pressure (below water table, if any Hydrostatic Force	.,	1.33 ft	426.7 ft-#
Buoyant Force	0.0		
Surcharge over Heel Adjacent Footing Surcharge Over Toe Load @ Stem Above Soil	0.0 0.0 0.0 0.0		
Added Lateral Load Seismic Load Seismic-Self-weight	0.0 156.8 0.0	1.33	209.1

Totals =

476.8 lbs Overturning Moment

635.7 ft-#

Page: 5 Date: 7 JAN 2020

nPro (c) 1987-2019, Build 11.19.11.12 ise : KW-06056929 nse To : JAMES G. PIERSON		Cantilevered	Retaining Wall	Code: IBC 2018,ACI 318-14,TMS 402
em Design Summary				
		Bottom		
		Stem OK		
Design Height Above Ftg	ft =	0.00		
Wall Material Above "Ht"	=	Concrete		
Design Method	=	LRFD		
Thickness	=	8.00		
Rebar Size	=	# 4		
Rebar Spacing	=	9.00		
Rebar Placed at	=	Edge		
Design Data				
fb/FB + fa/Fa	=	0.057		
Total Force @ Section				
Service Level	lbs =			
Strength Level	lbs =	414.0		
MomentActual Service Level	ft-# =			
Strength Leve	ft-# =	414.0		
MomentAllowable	=			
ShearActual				
Service Level	psi =			
Strength Leve	psi =	5.5		
ShearAllowable	psi =			
Anet	in2 =			
Rebar Depth 'd'	in =			
Masonry Data				
fm	psi =			
Fs	psi =			
Solid Grouting	=			
Modular Ratio 'n'	=			
Wall Weight	psf =	100.0		
Short Term Factor	=			
Equiv. Solid Thick.	=			
Masonry Block Type	=	Medium Weight		
Masonry Design Method	=	ASD		
Concrete Data		0 500 0		
f'c Fy	psi = psi =			

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Cantilevered Retaining Wall

Code: IBC 2018, ACI 318-14, TMS 402-16

Concrete Stem Rebar Area Details

Bottom Stem As (based on applied moment) :		cal Reinforcing 55 in2/ft	Horizontal Reinford	cing		
(4/3) * As :		07 in2/ft	Min Stem T&S Rei	nf Area 0.576 in2		
200bd/fy : 200(12)(6.25)/60000 :	0.25	in2/ft	Min Stem T&S Rei	nf Area per ft of ste	m Height :	: 0.192 in2/ft
0.0018bh : 0.0018(12)(8) :	0.172	28 in2/ft	Horizontal Reinford	cing Options :		
	====	=======	One layer of :	Two layers of :		
Required Area :	0.172	28 in2/ft	#4@ 12.50 in	#4@ 25.00 in		
Provided Area :	0.266	67 in2/ft	#5@ 19.38 in	#5@ 38.75 in		
Maximum Area :	0.846	67 in2/ft	#6@ 27.50 in	#6@ 55.00 in		
Footing Data						
Toe Width	=	1.00 ft	f'c		=	2,500 psi
Heel Width	=	1.50	Fy		=	60,000 psi
Total Footing Width	=	2.50 ft	Footing Conc	rete Density	=	150.00 pcf
Footing Thickness	=	12.00 in	Min. As %		=	0.0018
Key Width	=	0.00 in	Rebar Cover	@ Тор	=	2.00 in
Key Depth	=	0.00 in		@ Bottom	=	3.00 in
Key Distance from Toe	=	2.00 ft				

Footing Design Results

~		Toe	Heel	
Factored Pressure	=	1,045		psf
Mu' : Upward	=	5,448	46	ft-#
Mu' : Downward	=	1,476	200	ft-#
Mu: Design	=	143	-15	ft-#
Actual 1-Way Shear	=	2.05	2.82	psi
Allow 1-Way Shear	=	75.00	75.00	psi
Toe Reinforcing	=	# 4 @ 9.00 in		
Heel Reinforcing	=	# 4 @ 9.00 in		
Key Reinforcing	=	None Spec'd		
Toe: #4@ 9.25 in, #5@ 14.34 in, Heel: #4@ 9.25 in, #5@ 14.34 in, Key: No key defined	-	-	-	-
Min footing T&S reinf Area	0.65	5 in2		
Min footing T&S reinf Area per fo	0.26	6 in2 /ft		
If one layer of horizontal bars: #4@ 9.26 in #5@ 14.35 in #6@ 20.37 in		If two layers of horiz #4@ 18.52 in #5@ 28.70 in #6@ 40.74 in	ontal bars:	
Footing Torsion, Tu Footing Allow. Torsion, phi Tu	= =	0.00 ft-lbs 0.00 ft-lbs		

If torsion exceeds allowable, provide supplemental design for footing torsion.

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Cantilevered Retaining Wall

Code: IBC 2018, ACI 318-14, TMS 402-16

Tilt

Horizontal Deflection at Top of Wall due to settlement of soil

(Deflection due to wall bending not considered)

Soil Spring Reaction Modulus

250.0 pci 0.025 in

Horizontal Defl @ Top of Wall (approximate only)

The above calculation is not valid if the heel soil bearing pressure exceeds that of the toe,

because the wall would then tend to rotate into the retained soil.

James G. Pierson, Inc. 610 SW Alder #918 Portland, OR 97205 503-226-1286 www.jgpierson.com This Wall in File: X:\Residential Projects\Reside	Project Name/Number : a Title 4 ft : Dsgnr: Golberg Description Site Retaining Wall sch. ntial Projects 2019\4145 SW Agate - Butler Design\	agate - retai Page: 8 Date: 7 JAN 2020
RetainPro (c) 1987-2019, Build 11.19.11.12 License : KW-06056929 License To : JAMES G. PIERSON	Cantilevered Retaining Wall	Code: IBC 2018,ACI 318-14,TMS 402-16
Rebar Lap & Embedment Lengths In	nformation	
Stem Design Segment: Bottom		
Stem Design Height: 0.00 ft above top of fo	poting	
Lap Splice length for #4 bar specified in this st	em design segment =	18.72 in
Development length for #4 bar specified in this	s stem design segment =	14.40 in
Hooked embedment length into footing for #4 b	bar specified in this stem design segment =	8.40 in
As Provided =		0.2667 in2/ft
As Required =		0.1728 in2/ft

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cense : KW-06056929 cense To : JAMES G. PIERSON	I	Cantilevered		2010,F	CI 318-14,TMS 402
Criteria					
Retained Height	=	5.00 ft			
Wall height above soil	=	0.00 ft			
Slope Behind Wall	=	0.00			
Height of Soil over Toe	=	6.00 in			
Water height over heel	=	0.0 ft			Extrat
Load Factors					
Building Code	IE	3C 2018,ACI			
Dead Load		1.200			
Live Load		1.600			
Earth, H		1.600			
Wind, W		1.000			
Seismic, E		1.000			
Soil Data and Lateral Eart	h Pressu	ire			
Allow Soil Bearing	=	2,300.0 psf	Soil Density, Heel	=	110.00 pcf
Equivalent Fluid Pressure Method	b		Soil Density, Toe	=	0.00 pcf
Active Heel Pressure	=	40.0 psf/ft	Footing Soil Friction	=	0.400
	_		Soil height to ignore		
Passive Pressure	=	250.0 psf/ft	for passive pressure	=	12.00 in
	= rturning	0.0 psf	Surcharge Over Toe Used for Sliding & Ove	= erturning	0.0
Surcharge Over Heel Used To Resist Sliding & Over	rturning	0.0 psf	-		0.0
Axial Load Applied to Ste	rturning m		Used for Sliding & Ove	erturning	
Surcharge Over Heel Used To Resist Sliding & Over	rturning	0.0 psf 0.0 lbs 0.0 lbs	-		0.0 0.0 in
Surcharge Over Heel Used To Resist Sliding & Over Axial Load Applied to Ster Axial Dead Load Axial Live Load	rturning m = =	0.0 lbs	Used for Sliding & Ove	erturning	
Surcharge Over Heel Used To Resist Sliding & Over Axial Load Applied to Ster Axial Dead Load Axial Live Load	rturning m = =	0.0 lbs	Used for Sliding & Ove	erturning	
Surcharge Over Heel Used To Resist Sliding & Over Axial Load Applied to Ster Axial Dead Load Axial Live Load	rturning m = = tem	0.0 lbs 0.0 lbs	Used for Sliding & Ove	erturning	
Surcharge Over Heel Used To Resist Sliding & Over Axial Load Applied to Ster Axial Dead Load Axial Live Load -ateral Load Applied to Si Lateral Load Height to Top	rturning = = tem =	0.0 lbs 0.0 lbs 0.0 #/ft 0.00 ft	Used for Sliding & Ove	erturning	
Surcharge Over Heel Used To Resist Sliding & Over Axial Load Applied to Ster Axial Dead Load Axial Live Load -ateral Load Applied to St Lateral Load Height to Top Height to Bottom	rturning m = = tem =	0.0 lbs 0.0 lbs 0.0 #/ft	Used for Sliding & Ove	erturning	
Surcharge Over Heel Used To Resist Sliding & Over Axial Load Applied to Ster Axial Dead Load Axial Live Load Axial Live Load Lateral Load Height to Top Height to Bottom Load Type	rturning = = = tem = = =	0.0 lbs 0.0 lbs 0.0 #/ft 0.00 ft 0.00 ft	Used for Sliding & Ove	erturning	
Surcharge Over Heel Used To Resist Sliding & Over Axial Load Applied to Ster Axial Dead Load Axial Live Load Axial Live Load Lateral Load Height to Top Height to Bottom Load Type	rturning = = = tem = = =	0.0 lbs 0.0 lbs 0.0 #/ft 0.00 ft 0.00 ft Wind (W)	Used for Sliding & Ove	erturning	
Surcharge Over Heel Used To Resist Sliding & Over Axial Load Applied to Ster Axial Dead Load Axial Live Load 	rturning = = = tem = = =	0.0 lbs 0.0 lbs 0.0 #/ft 0.00 ft 0.00 ft Wind (W)	Used for Sliding & Ove	erturning	
Surcharge Over Heel Used To Resist Sliding & Over Axial Load Applied to Ster Axial Dead Load Axial Live Load Axial Live Load Lateral Load Height to Top Height to Bottom Load Type Vind on Exposed Stem (Service Level)	rturning = = : tem = = = =	0.0 lbs 0.0 lbs 0.0 lbs 0.0 #/ft 0.00 ft 0.00 ft Wind (W) (Service Level)	Used for Sliding & Ove	erturning	
Surcharge Over Heel Used To Resist Sliding & Over Axial Load Applied to Ster Axial Dead Load Axial Live Load Axial Live Load Height to Top Height to Top Height to Bottom Load Type Vind on Exposed Stem (Service Level) Adjacent Footing Load	rturning = = : tem = = = =	0.0 lbs 0.0 lbs 0.0 lbs 0.0 #/ft 0.00 ft 0.00 ft Wind (W) (Service Level)	Used for Sliding & Ove	erturning =	
Surcharge Over Heel Used To Resist Sliding & Over Axial Load Applied to Ster Axial Dead Load Axial Live Load Axial Live Load Lateral Load Applied to St Lateral Load Height to Top Height to Bottom Load Type Vind on Exposed Stem (Service Level) Adjacent Footing Load	rturning	0.0 lbs 0.0 lbs 0.0 lbs 0.0 #/ft 0.00 ft 0.00 ft Wind (W) (Service Level) 0.0 psf	Used for Sliding & Ove	erturning =	0.0 in
Surcharge Over Heel Used To Resist Sliding & Over Axial Load Applied to Ster Axial Dead Load Axial Live Load -ateral Load Applied to St Lateral Load Height to Top Height to Bottom Load Type Wind on Exposed Stem	rturning	0.0 lbs 0.0 lbs 0.0 lbs 0.0 ft 0.00 ft Wind (W) (Service Level) 0.0 psf 0.0 lbs	Used for Sliding & Ove	erturning =	0.0 in

James G. Pierson, Inc. 610 SW Alder #918 Portland, OR 97205 503-226-1286 www.jgpierson.com This Wall in File: X:\Residential Projects\Residential	Title 6 ft : Dsgnr: Golberg Description Site Retaining W	/all sch.	
RetainPro (c) 1987-2019, Build 11.19.11.12 License : KW-06056929 License To : JAMES G. PIERSON	Cantilevered Retaining W	Code: IBC 2018,ACI 318-14,TMS	6 402-16
Earth Pressure Seismic Load			
Method : Triangular			
Load at bottom of Triangular Distribution Strength-Level)	•	ength-Level Seismic Load = 525.00 vice-Level Seismic Load = 367.50	

Total Service-Level Seismic Load. =

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Wall Design Summary		

Wall Design Summary

Stability Ratios Overturning Slab Resists All Sliding !	=	2.40 OK
Soil Bearing		
Total Bearing Load	=	2,108 lbs
resultant ecc.	=	6.64 in
Soil Pressure @ Toe	=	964 psf OK
Soil Pressure @ Heel	=	90 psf OK
Allowable	=	2,300 psf
Soil Pressure Less Tha	an Allowable)
ACI Factored @ Toe	=	1,350 psf
ACI Factored @ Heel	=	126 psf
Footing Shear @ Toe	=	7.5 psi OK
Footing Shear @ Heel	=	7.0 psi OK
Allowable	=	75.0 psi

Overturning

Resisting Moments

Resisting Moments	Force	<u>Distan</u>	<u>ce</u>	<u>Moment</u>		
Soil Over Heel (above water table, if any)	1,008.3	lbs 3	.08 ft	3,109.0ft-#		
Soil Over Heel (below water table, if any)	0.0					
Water Table	0.0					
Soil Over Heel	1,008.3	3	.08	3,109.0		
Sloped Soil Over Heel	0.0					
Surcharge Over Heel	0.0					
Adjacent Footing Load	0.0					
Axial Dead Load on Stem	0.0					
Axial Live Load on Stem *	0.0					
Soil Over Toe	0.0	0	.75			
Surcharge Over Toe	0.0					
Stem Weight(s)	500.0	1	.83	916.7		
Earth @ Stem Transitions	0.0					
Footing Weight	600.0	2	.00	1,200.0		
Key Weight	0.0	2	.00			
Vert. Component	0.0					
Total Vertical Loads	2,108.3	lbs				
Resistin	Resisting Moment					
Eccentr	icity			6.6 in		

* Axial live load NOT included in total displayed, or used for overturning or sliding resistance, but is included for soil pressure calculations.

RetainPro (c) 1987-2019, Build 11.19.11.12 License : KW-06056929 License To : JAMES G. PIERSON	Cantilevered	Retaining Wal	Code: IBC 2018,ACI 318-14,TMS 402-16
Overturning			
Overturning Moments			
Overturning Moments	<u>Force</u>	<u>Distance</u>	<u>Moment</u>
Heel Active Pressure (above water table, if a Heel Active Pressure (below water table, if a Hydrostatic Force	• /	2.00 ft	1,440.0 ft-#
Buoyant Force	0.0		
Surcharge over Heel Adjacent Footing Surcharge Over Toe Load @ Stem Above Soil	0.0 0.0 0.0 0.0		
Added Lateral Load Seismic Load Seismic-Self-weight	0.0 367.5 0.0	2.00	735.0
Totals =	1,087.5 lbs		

Overturning Moment

2,175.0 ft-#

nPro (c) 1987-2019, Build 11.19.11.12 se : KW-06056929 1se To : JAMES G. PIERSON		Cantilevered F	Retaining Wall	Code: IBC 2018,ACI 318-14,TMS 402-
em Design Summary				
		Bottom		
		Stem OK		
Design Height Above Ftg	ft =	0.00		
Wall Material Above "Ht"	=	Concrete		
Design Method	=	LRFD		
Thickness	=	8.00		
Rebar Size	=	# 4		
Rebar Spacing	=	9.00		
Rebar Placed at	=	Edge		
Design Data				
fb/FB + fa/Fa	=	0.272		
Total Force @ Section				
Service Level	lbs =	:		
Strength Level	lbs =	1,164.6		
MomentActual				
Service Level	ft-# =	:		
Strength Leve	ft-# =	1,941.0		
MomentAllowable	=	7,122.4		
ShearActual				
Service Level	psi =	:		
Strength Level	psi =	15.5		
ShearAllowable	psi =	75.0		
Anet	in2 =	:		
Rebar Depth 'd'	in =	6.25		
Masonry Data				
f'm	psi =	:		
Fs	psi =	:		
Solid Grouting	=	:		
Modular Ratio 'n'	=			
Wall Weight	psf =	100.0		
Short Term Factor	=			
Equiv. Solid Thick.	=	:		
Masonry Block Type	=	Medium Weight		
Masonry Design Method	=	ASD		
Concrete Data	psi =	2,500.0		
f'c Fy	psi = psi =	-		

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Cantilevered Retaining Wall

Code: IBC 2018, ACI 318-14, TMS 402-16

Concrete Stem Rebar Area Details

Bottom Stem As (based on applied moment) :		cal Reinforcing 27 in2/ft	Horizontal Reinford	cing		
(4/3) * As :		7 in2/ft	Min Stem T&S Rei	inf Area 0.960 in2		
200bd/fy : 200(12)(6.25)/60000 :	0.25	in2/ft	Min Stem T&S Rei	inf Area per ft of ste	m Height :	0.192 in2/ft
0.0018bh : 0.0018(12)(8) :	0.172	28 in2/ft	Horizontal Reinford	cing Options :		
	====	=======	One layer of :	Two layers of :		
Required Area :	0.172	28 in2/ft	#4@ 12.50 in	#4@ 25.00 in		
Provided Area :	0.26	67 in2/ft	#5@ 19.38 in	#5@ 38.75 in		
Maximum Area :	0.846	67 in2/ft	#6@ 27.50 in	#6@ 55.00 in		
Footing Data						
Toe Width	=	1.50 ft	f'c		=	2,500 psi
Heel Width	=	2.50	Fy		=	60,000 psi
Total Footing Width	=	4.00 ft	Footing Conc	crete Density	=	150.00 pcf
Footing Thickness	=	12.00 in	Min. As %		=	0.0018
Key Width	=	0.00 in	Rebar Cover	@ Top	=	2.00 in
Key Depth	=	0.00 in		@ Bottom	=	3.00 in
Key Distance from Toe	=	2.00 ft				

Footing Design Results

		Toe	Heel	
Factored Pressure	=	1,350	126	psf
Mu' : Upward	=	16,160	526	ft-#
Mu' : Downward	=	3,321	1,412	ft-#
Mu: Design	=	553	-172	ft-#
Actual 1-Way Shear	=	7.46	6.97	psi
Allow 1-Way Shear	=	75.00	75.00	psi
Toe Reinforcing	=	# 4 @ 9.00 in		
Heel Reinforcing	=	# 4 @ 9.00 in		
Key Reinforcing	=	None Spec'd		
Toe: #4@ 9.25 in, #5@ 14.34 in, Heel: #4@ 9.25 in, #5@ 14.34 in, Key: No key defined	-	-	-	-
Min footing T&S reinf Area	1.04	l in2		
Min footing T&S reinf Area per fo	0.26	6 in2 /ft		
If one layer of horizontal bars: #4@ 9.26 in #5@ 14.35 in #6@ 20.37 in		If two layers of horiz #4@ 18.52 in #5@ 28.70 in #6@ 40.74 in	zontal bars:	
Footing Torsion, Tu Footing Allow. Torsion, phi Tu	= =	0.00 ft-lbs 0.00 ft-lbs		

If torsion exceeds allowable, provide supplemental design for footing torsion.

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Cantilevered Retaining Wall

Code: IBC 2018, ACI 318-14, TMS 402-16

Tilt

Horizontal Deflection at Top of Wall due to settlement of soil

(Deflection due to wall bending not considered)

Soil Spring Reaction Modulus

250.0 pci

Horizontal Defl @ Top of Wall (approximate only) 0.033 in

The above calculation is not valid if the heel soil bearing pressure exceeds that of the toe,

because the wall would then tend to rotate into the retained soil.

James G. Pierson, Inc. 610 SW Alder #918 Portland, OR 97205 503-226-1286 www.jgpierson.com This Wall in File: X:\Residential Projects\Residential	Project Name/Number : a Title 6 ft : Dsgnr: Golberg Description Site Retaining Wall sch. ntial Projects 2019\4145 SW Agate - Butler Design\	agate - retai Page: 8 Date: 9 MAY 2022
RetainPro (c) 1987-2019, Build 11.19.11.12 License : KW-06056929 License To : JAMES G. PIERSON	Cantilevered Retaining Wall	Code: IBC 2018,ACI 318-14,TMS 402-16
Rebar Lap & Embedment Lengths In	offormation	
Stem Design Segment: Bottom		
Stem Design Height: 0.00 ft above top of fo	poting	
Lap Splice length for #4 bar specified in this ste	em design segment =	18.72 in
Development length for #4 bar specified in this	stem design segment =	14.40 in
Hooked embedment length into footing for #4 b	par specified in this stem design segment =	8.40 in
As Provided =		0.2667 in2/ft
As Required =		0.1728 in2/ft

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etainPro (c) 1987-2019, Build 11.19.11. cense : KW-06056929 cense To : JAMES G. PIERSON			Retaining Wall Code	e: IBC 2018,A	ACI 318-14,TMS 402
Criteria					
Retained Height	=	7.00 ft			
Wall height above soil	=	0.00 ft			
Slope Behind Wall	=	0.00			
Height of Soil over Toe	=	6.00 in			
Water height over heel	=	0.0 ft			Partage •
Load Factors					
Building Code	IB	C 2018,ACI			
Dead Load		1.200			
Live Load		1.600			
Earth, H		1.600			
Wind, W		1.000			
Seismic, E		1.000			
Soil Data and Lateral Earth	Pressu	ire			
Allow Soil Bearing	=	2,300.0 psf	Soil Density, Heel	=	110.00 pcf
Equivalent Fluid Pressure Method			Soil Density, Toe	=	0.00 pcf
Active Heel Pressure	=	40.0 psf/ft	Footing Soil Friction	=	0.400
	_		Soil height to ignore		
Passive Pressure	=	250.0 psf/ft	for passive pressure	=	12.00 in
Surcharge Loads					
	= urning	0.0 psf	Surcharge Over Toe Used for Sliding & Ove	= erturning	0.0
Surcharge Over Heel Used To Resist Sliding & Overti	urning	0.0 psf	_		0.0
Surcharge Over Heel Used To Resist Sliding & Overtu Axial Load Applied to Stem	urning 1		Used for Sliding & Ove	erturning	
Surcharge Over Heel Used To Resist Sliding & Overti	urning	0.0 psf 0.0 lbs 0.0 lbs	_		0.0 0.0 in
Surcharge Over Heel Used To Resist Sliding & Overtu Axial Load Applied to Stem Axial Dead Load Axial Live Load	urning 1 = =	0.0 lbs	Used for Sliding & Ove	erturning	
Surcharge Over Heel Used To Resist Sliding & Overtu Axial Load Applied to Stem Axial Dead Load Axial Live Load Lateral Load Applied to Ste	urning 1 = =	0.0 lbs 0.0 lbs 0.0 #/ft	Used for Sliding & Ove	erturning	
Surcharge Over Heel Used To Resist Sliding & Overtu Axial Load Applied to Stem Axial Dead Load Axial Live Load Lateral Load Applied to Ste	urning = = em	0.0 lbs 0.0 lbs	Used for Sliding & Ove	erturning	
Surcharge Over Heel Used To Resist Sliding & Overtu Axial Load Applied to Stem Axial Dead Load Axial Live Load -ateral Load Applied to Ste Lateral Load Height to Top	urning = = em =	0.0 lbs 0.0 lbs 0.0 #/ft	Used for Sliding & Ove	erturning	
Surcharge Over Heel Used To Resist Sliding & Overtu Axial Load Applied to Sterr Axial Dead Load Axial Live Load -ateral Load Applied to Ste Lateral Load Height to Top Height to Bottom	urning = = = em = =	0.0 lbs 0.0 lbs 0.0 #/ft 0.00 ft 0.00 ft Wind (W)	Used for Sliding & Ove	erturning	
Surcharge Over Heel Used To Resist Sliding & Overtu Axial Load Applied to Stem Axial Dead Load Axial Live Load -ateral Load Applied to Ste Lateral Load Height to Top Height to Bottom Load Type	urning = = em = = =	0.0 lbs 0.0 lbs 0.0 #/ft 0.00 ft 0.00 ft	Used for Sliding & Ove	erturning	
Surcharge Over Heel Used To Resist Sliding & Overtu Axial Load Applied to Stem Axial Dead Load Axial Live Load Lateral Load Applied to Ste Lateral Load Height to Top Height to Bottom Load Type	urning = = em = = =	0.0 lbs 0.0 lbs 0.0 #/ft 0.00 ft 0.00 ft Wind (W)	Used for Sliding & Ove	erturning	
Surcharge Over Heel Used To Resist Sliding & Overtu Axial Load Applied to Stem Axial Dead Load Axial Live Load Axial Live Load Lateral Load Applied to Ste Lateral Load Height to Top Height to Bottom Load Type Wind on Exposed Stem (Service Level)	urning = = = = = = =	0.0 lbs 0.0 lbs 0.0 lbs 0.0 #/ft 0.00 ft 0.00 ft Wind (W) (Service Level)	Used for Sliding & Ove	erturning	
Surcharge Over Heel Used To Resist Sliding & Overtu Axial Load Applied to Stem Axial Dead Load Axial Live Load -ateral Load Applied to Ste Lateral Load Height to Top Height to Bottom Load Type Wind on Exposed Stem (Service Level) Adjacent Footing Load	urning = = = = = = =	0.0 lbs 0.0 lbs 0.0 lbs 0.0 #/ft 0.00 ft 0.00 ft Wind (W) (Service Level)	Used for Sliding & Ove	erturning =	
Surcharge Over Heel Used To Resist Sliding & Overtu Axial Load Applied to Stem Axial Dead Load Axial Live Load Axial Live Load Lateral Load Applied to Ste Lateral Load Height to Top Height to Bottom Load Type Mind on Exposed Stem (Service Level) Adjacent Footing Load	urning = = = = = = = =	0.0 lbs 0.0 lbs 0.0 lbs 0.0 ft 0.00 ft Wind (W) (Service Level) 0.0 psf 0.0 lbs	Used for Sliding & Ove	erturning =	0.0 in
Surcharge Over Heel Used To Resist Sliding & Overtu Axial Load Applied to Stem Axial Dead Load Axial Live Load Lateral Load Applied to Ste Lateral Load Applied to Ste Lateral Load Height to Top Height to Bottom Load Type Mind on Exposed Stem (Service Level) Adjacent Footing Load Footing Width	urning = = = = = = = = = =	0.0 lbs 0.0 lbs 0.0 lbs 0.0 ft 0.00 ft Wind (W) (Service Level) 0.0 psf 0.0 lbs 0.00 ft	Used for Sliding & Ove	erturning = 	0.0 in
Axial Load Applied to Stem Axial Dead Load Axial Dead Load Axial Live Load Lateral Load Applied to Ste Lateral Load Height to Top Height to Bottom Load Type Wind on Exposed Stem (Service Level) Adjacent Footing Load	urning = = = = = = = =	0.0 lbs 0.0 lbs 0.0 lbs 0.0 ft 0.00 ft Wind (W) (Service Level) 0.0 psf 0.0 lbs	Used for Sliding & Ove	erturning =	0.0 in

James G. Pierson, Inc. 610 SW Alder #918 Portland, OR 97205 503-226-1286 www.jgpierson.com This Wall in File: X:\Residential Projects\Residentia	Project Name/Number : a Title 8 ft : Dsgnr: Golberg Description Site Retaining Wall sch. al Projects 2019\4145 SW Agate - Butler Design\	i gate - retai Page : 2 Date: 9 MAY 2022
RetainPro (c) 1987-2019, Build 11.19.11.12 License : KW-06056929 License To : JAMES G. PIERSON	Cantilevered Retaining Wall	Code: IBC 2018,ACI 318-14,TMS 402-16
Earth Pressure Seismic Load		
Method : Triangular		
Load at bottom of Triangular Distribution Strength-Level)		el Seismic Load = 1,372.000 lbs I Seismic Load = 960.400 lbs

Total Service-Level Seismic Load. = 960.400 lbs

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Wall Design Summary		

Wall Design Summary

Stability Ratios Overturning Slab Resists All Sliding !	=	2.14 OK
Soil Bearing		
Total Bearing Load	=	3,707 lbs
resultant ecc.	=	10.87 in
Soil Pressure @ Toe	=	1,340 psf OK
Soil Pressure @ Heel	=	8 psf OK
Allowable	=	2,300 psf
Soil Pressure Less That	n Allowable	e
ACI Factored @ Toe	=	1,876 psf
ACI Factored @ Heel	=	11 psf
Footing Shear @ Toe	=	17.6 psi OK
Footing Shear @ Heel	=	15.2 psi OK
Allowable	=	75.0 psi

Overturning

Resisting Moments

Resisting Moments	Force	Distar	nce	<u>Moment</u>
Soil Over Heel (above water table, if any)	2,181.7	lbs	4.08 ft	8,908.5ft-#
Soil Over Heel (below water table, if any)	0.0			
Water Table	0.0			
Soil Over Heel	2,181.7		4.08	8,908.5
Sloped Soil Over Heel	0.0			
Surcharge Over Heel	0.0			
Adjacent Footing Load	0.0			
Axial Dead Load on Stem	0.0			
Axial Live Load on Stem *	0.0			
Soil Over Toe	0.0		1.00	
Surcharge Over Toe	0.0			
Stem Weight(s)	700.0		2.33	1,633.3
Earth @ Stem Transitions	0.0			
Footing Weight	825.0		2.75	2,268.8
Key Weight	0.0		2.00	
Vert. Component	0.0			
Total Vertical Loads	3,706.7	lbs		
Resisting		12,810.6 ft-#		
Eccentri		10.9 in		

* Axial live load NOT included in total displayed, or used for overturning or sliding resistance, but is included for soil pressure calculations.

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Overturning			
Overturning Moments			
Overturning Moments	<u>Force</u>	<u>Distance</u>	Moment
Heel Active Pressure (above water table, if an Heel Active Pressure (below water table, if an Hydrostatic Force		2.67 ft	3,413.3 ft-#
Buoyant Force	0.0		
Surcharge over Heel Adjacent Footing Surcharge Over Toe Load @ Stem Above Soil	0.0 0.0 0.0 0.0		
Added Lateral Load Seismic Load Seismic-Self-weight	0.0 960.4 0.0	2.67	2,561.1
Totals =	2,240.4 lbs Overturning	Moment	5,974.4 ft-#

nPro (c) 1987-2019, Build 11.19.11.12 se : KW-06056929 nse To : JAMES G. PIERSON		Cantilevered Re	etaining Wall	Code: IBC 2018,ACI 318-14,TMS 402-
em Design Summary				
		Bottom		
		Stem OK		
Design Height Above Ftg	ft =	0.00		
Wall Material Above "Ht"	=	Concrete		
Design Method	=	LRFD		
Thickness	=	8.00		
Rebar Size	=	# 4		
Rebar Spacing	=	9.00		
Rebar Placed at	=	Edge		
Design Data				
fb/FB + fa/Fa	=	0.857		
Total Force @ Section				
Service Level	lbs =			
Strength Level	lbs =	2,618.4		
MomentActual				
Service Level	ft-# =			
Strength Level	ft-# =	,		
MomentAllowable	=	7,122.4		
ShearActual				
Service Level	psi =			
Strength Leve	psi =	34.9		
ShearAllowable	psi =	75.0		
Anet	in2 =			
Rebar Depth 'd'	in =	6.25		
Masonry Data				
fm	psi =			
Fs	psi =			
Solid Grouting	=			
Modular Ratio 'n'	=			
Wall Weight	psf =	100.0		
Short Term Factor	=			
Equiv. Solid Thick.	=			
Masonry Block Type	=	Medium Weight		
Masonry Design Method	=	ASD		
Concrete Data		2 500 0		
f'c Fy	psi = psi =			

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Cantilevered Retaining Wall

Code: IBC 2018, ACI 318-14, TMS 402-16

Concrete Stem Rebar Area Details

Bottom Stem As (based on applied moment) :		cal Reinforcing 39 in2/ft	Horizontal Reinford	cing					
(4/3) * As :		52 in2/ft	Min Stem T&S Rei	nf Area 1.344 in2					
200bd/fy : 200(12)(6.25)/60000 :	0.25 in2/ft		Min Stem T&S Rei	Min Stem T&S Reinf Area per ft of stem Height : 0.192 in2/ft					
0.0018bh : 0.0018(12)(8) :	0.172	28 in2/ft	Horizontal Reinford	Horizontal Reinforcing Options :					
	====	=======	One layer of :	Two layers of :					
Required Area :	0.25	in2/ft	#4@ 12.50 in	#4@ 25.00 in					
Provided Area :	0.266	67 in2/ft	#5@ 19.38 in	#5@ 38.75 in					
Maximum Area :	0.846	67 in2/ft	#6@ 27.50 in	#6@ 55.00 in					
Footing Data									
Toe Width	=	2.00 ft	fc		=	2,500 psi			
Heel Width	=	3.50	Fy		=	60,000 psi			
Total Footing Width	=	5.50 ft	Footing Conc	rete Density	=	150.00 pcf			
Footing Thickness	=	12.00 in	Min. As %		=	0.0018			
Key Width	=	0.00 in	Rebar Cover	@ Top	=	2.00 in			
Key Depth	=	0.00 in		@ Bottom	=	3.00 in			
Key Distance from Toe	=	2.00 ft							

Footing Design Results

~		Toe	Heel	
Factored Pressure	=	1,876	11	psf
Mu' : Upward	=	39,594	1,330	ft-#
Mu' : Downward	=	5,904	4,431	ft-#
Mu: Design	=	1,395	-644	ft-#
Actual 1-Way Shear	=	17.59	15.22	psi
Allow 1-Way Shear	=	75.00	75.00	psi
Toe Reinforcing	=	# 4 @ 9.00 in		
Heel Reinforcing	=	# 4 @ 9.00 in		
Key Reinforcing	=	None Spec'd		
Toe: #4@ 9.25 in, #5@ 14.34 in, Heel: #4@ 9.25 in, #5@ 14.34 in, Key: No key defined	-	-	-	-
Min footing T&S reinf Area	1.43	3 in2		
Min footing T&S reinf Area per fo	0.26	6 in2 /ft		
If one layer of horizontal bars: #4@ 9.26 in #5@ 14.35 in #6@ 20.37 in		If two layers of horiz #4@ 18.52 in #5@ 28.70 in #6@ 40.74 in	ontal bars:	
Footing Torsion, Tu Footing Allow. Torsion, phi Tu	= =	0.00 ft-lbs 0.00 ft-lbs		

If torsion exceeds allowable, provide supplemental design for footing torsion.

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Cantilevered Retaining Wall

Code: IBC 2018, ACI 318-14, TMS 402-16

Tilt

Horizontal Deflection at Top of Wall due to settlement of soil

(Deflection due to wall bending not considered)

Soil Spring Reaction Modulus

250.0 pci 0.047 in

Horizontal Defl @ Top of Wall (approximate only)

The above calculation is not valid if the heel soil bearing pressure exceeds that of the toe,

because the wall would then tend to rotate into the retained soil.

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RetainPro (c) 1987-2019, Build 11.19.11.12 License : KW-06056929 License To : JAMES G. PIERSON	Cantilevered Retaining Wall	Code: IBC 2018,ACI 318-14,TMS 402-16
Rebar Lap & Embedment Lengths Ir	nformation	
Stem Design Segment: Bottom		
Stem Design Height: 0.00 ft above top of fo	poting	
Lap Splice length for #4 bar specified in this st	em design segment =	18.72 in
Development length for #4 bar specified in this	14.40 in	
Hooked embedment length into footing for #4 t	8.40 in	
As Provided =		0.2667 in2/ft
As Required =	0.2500 in2/ft	