Development Services

From Concept to Construction

Phone: 503-823-7300 Email: bds@portlandoregon.gov 1900 SW 4th Ave, Portland, OR 97201 More Contact Info (http://www.portlandoregon.gov//bds/article/519984)





APPEAL SUMMARY

Status: Decision Rendered - Reconsideration of ID 14623, items 2 and 3

Appeal ID: 14740	Project Address: 40 NE Tillamook St
Hearing Date: 3/8/17	Appellant Name: Dylan Lamar
Case No.: B-013	Appellant Phone: 503-804-1746 x102
Appeal Type: Building	Plans Examiner/Inspector: Steven Mortensen
Project Type: commercial	Stories: 3 Occupancy: R-2 Construction Type: V-B
Building/Business Name: Tillamook Row NE	Fire Sprinklers: Yes - 13R Throughout
Appeal Involves: Erection of a new structure	LUR or Permit Application No.: 16-280750-CO
Plan Submitted Option: pdf [File 1] [File 2] [File 3] [File 4] [File 5]	Proposed use: R-2 Multifamily Residential

APPEAL INFORMATION SHEET

Appeal item 1

Appear item I			
Code Section	OSSC 1026.6		
Requires	Exterior exit stairways shall be separated from the interior of the building as required in Section 1022.2 (1 hour fire barrier in our case). Openings shall be limited to those necessary for egress from normally occupied spaces.		
	Also, because our exterior stairways project beyond the face of the building, our plans examiner has directed us to provide fire separation and protected openings for a minimum of 10 feet from the stairway per Section 1022.7, a section of the code that does not apply to exterior stairways, and which is not referred to in Section 1026. Section 1026.5 which does apply to our exterior exit stair, indicates that a 10 foot fire separation distance is required only from the lot line or other buildings on the same lot.		
Proposed Design	The design contains four exterior exit stairways each of which provides egress for one or two dwelling units (Occupancy of 9 – 18). Adjacent to the stairways are entrance doors and sidelites, as well as fixed and operable windows. At the stairway landings we have doors which provide access to a mechanical closet with Energy Recovery Ventilators (ERV's). The ERV's are located immediately behind the doors—there is no ability for a person to pass into the closet or use the closet for other purposes. The door would be locked other than when in active use by service personnel standing on the landing with the door open to change the ERV filters approximately twice per year. Each ERV's has an intake and exhaust duct which would penetrate the wall above and below the stair.		
	Due to the low occupancy, we propose to provide 1 hour fire-rated exterior walls and protected openings surrounding the stairways and continuing for a minimum distance of 5 feet from the stairways (see attached "Exterior Stair Opening Protection.PDF"). Entry doors will be solid ¾ hour		

rated and all glazing within 5 feet shall be fixed windows protected with a closely spaced wate	r
curtain sprinkler.	

At the mechanical room doors at the stair landings, we propose the use of 1 hour rated fire doors (same rating as the wall) which are self-closing per 716.5.9.

At the ERV ducts we propose 1 hour fusible link fire dampers. At the other doors and windows along the main façade of the building we propose unrated doors and windows with interior closely spaced water curtain sprinklers protecting each opening.

 Reason for alternative
 The proposed separation exceeds that required by code. Considering the 13R sprinkler system, the low occupancy served by these stairs and the availability of numerous egress windows, the risk to life safety is very low.

Appeal item 2

Code Section	OSSC 722.6.2
Requires	722.6.2.3 prescribes 20 minutes of fire resistance for 2x4 wood studs at 16"o.c.722.6.2.5 prescribes 15 minutes of fire resistance to various types of insulation filling a stud cavity.
Proposed Design	Apply 20 minutes of fire resistance to 2x8 wood studs at 16"o.c.
	Apply 15 minutes of fire resistance to a 1 1/2" layer of continuous mineral wool insulation (8.0 lb/cf) on the exterior side of the stud wall, as shown in the wall assembly attached.
	The assembly would then have the following fire resistance as calculated per OSSC 722.6.2.1:
	FIRE EXPOSURE FROM INTERIOR:
	5/8" TYPE X GYPSUM BOARD 40 MIN TABLE 722.6.2 (1) 2x8 WOOD STUDS 16" O.C. 20 MIN TABLE 722.6.2 (2) GLASS FIBER CAVITY INSULATION 15 MIN TABLE 722.6.2 (5) TOTAL 75 MIN
	FIRE EXPOSURE FROM EXTERIOR:
	1 1/2" MINERAL WOOL, 8.0 LB/CF 15 MIN TABLE 722.6.2 (5) 15/32" PLYWOOD, EXTERIOR 10 MIN TABLE 722.6.2 (1) 2x8 WOOD STUDS 16" O.C. 20 MIN TABLE 722.6.2 (2) GLASS FIBER CAVITY INSULATION 15 MIN TABLE 722.6.2 (5) TOTAL 60 MIN
	Mineral wool to be held in place by 1x4 battens fastened to wall with #8 screws at 24" O.C. max, with min 1" embedment into studs.
Reason for alternative	Using larger wood studs (i.e. 2x8 instead of 2x4) is acceptable for UL ratings without reducing the assembly fire resistance rating.
	Mineral wool proposed is a Non-Combustible material with a Flame Spread rating of 0 and a melting point of 2,150 degrees F (see attached data sheet). A continuous 1 1/2" thick layer of this material would have at least a 15 minute fire resistance, which is equivalent to, for example, a layer of 19/32" plywood per Table 722.6.2 (1). By contrast plywood is a combustible material with a flame spread rating of approximately 100. Further, 1 1/2" of 8.0 pcf mineral wool results in 1.0 psf density of mineral wool material, whereas 722.6.2.5 prescribes 15 minutes of fire resistance to

3.3 pcf mineral wool within a 2x4 stud cavity (which is not continuous) which achieves 0.96 psf density of mineral wool material.

A desired option is to allow 2x2 blocking to break the mineral wool, similar to studs breaking stud cavity insulation, to help keep the siding in a uniform plane.

A similar appeal was approved by the City of Seattle, substituting a continous layer of 1 1/4" mineral wool insulation (8 lb/cf) for a layer of 5/8" Type X gypsum board. See attached.

APPEAL DECISION

1a. 5' of protected openings in walls less than 90 degrees to exterior exit stair, sprinklers in lieu of protected openings: Granted as proposed provided sprinklers are installed a minimum of 4 inches and a maximum of 24 inches from the fixed opening(s) spaced at 6 feet on center. Sprinklers are to be installed on the occupied side of the openings and shall be capable of wetting the entire surface. A separate permit from the Fire Marshal's Office is required.

1b. 1 hour fire self-closing door to mechanical room opening to exterior exit stair: Granted provided a sprinkler head is installed within the mechanical room.

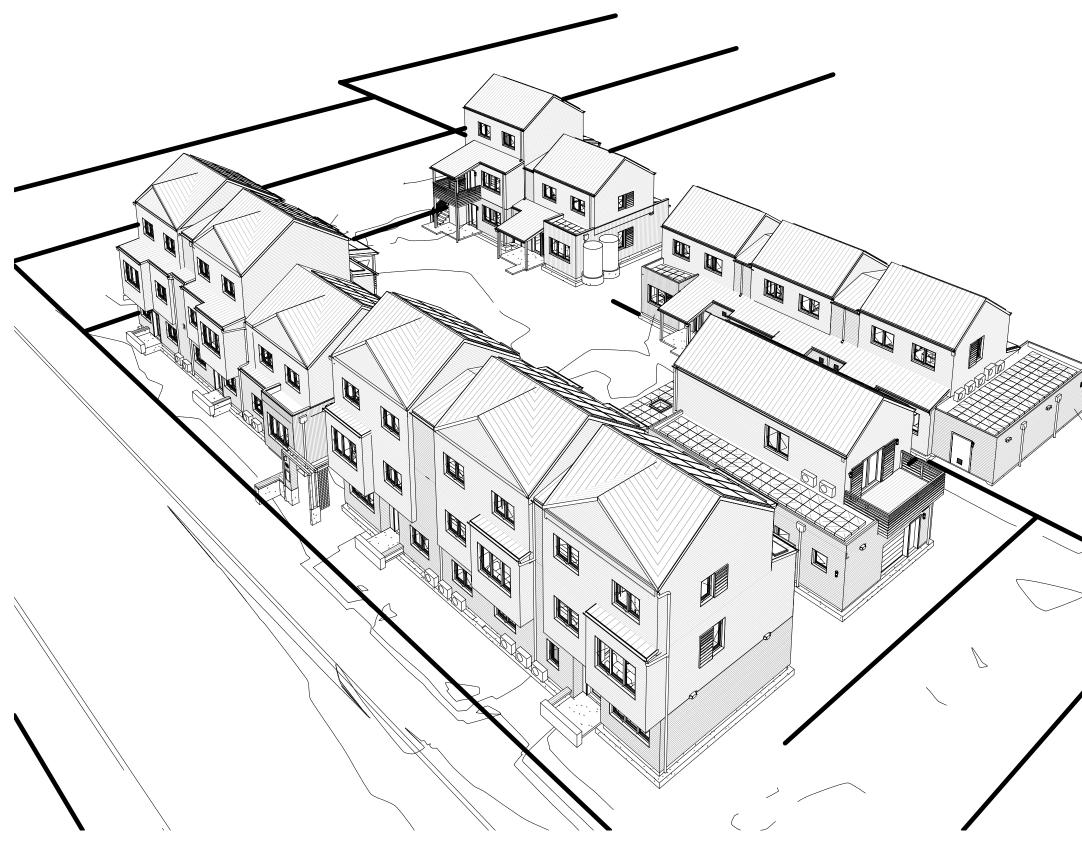
2. Alternate method for determining fire resistance rating of exterior wall assembly: Denied. Proposal does not demonstrate equivalent fire protection.

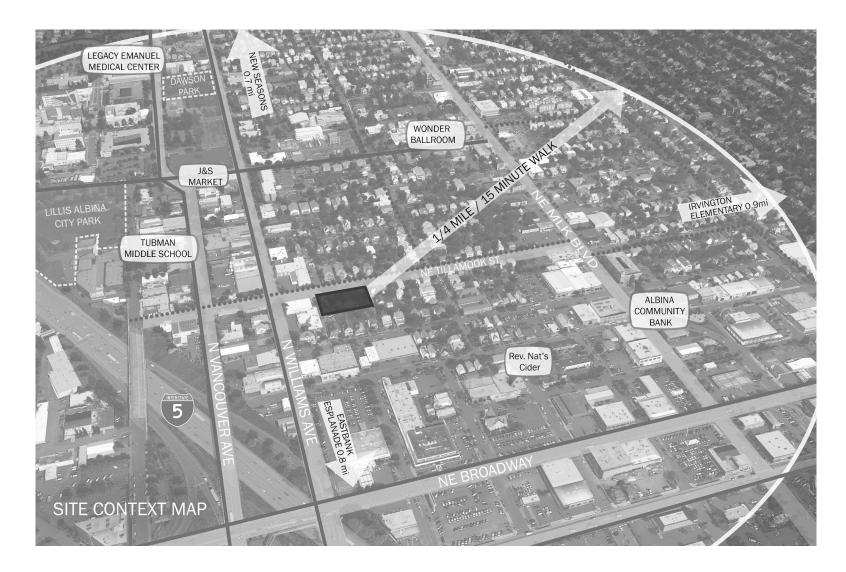
Appellant may contact Steve Mortensen (503-823-7272) with questions.

For the items granted, the Administrative Appeal Board finds that the information submitted by the appellant demonstrates that the approved modifications or alternate methods are consistent with the intent of the code; do not lessen health, safety, accessibility, life, fire safety or structural requirements; and that special conditions unique to this project make strict application of those code sections impractical.

Pursuant to City Code Chapter 24.10, you may appeal this decision to the Building Code Board of Appeal within 180 calendar days of the date this decision is published. For information on the appeals process and costs, including forms, appeal fee, payment methods and fee waivers, go to www.portlandoregon.gov/bds/appealsinfo, call (503) 823-7300 or come in to the Development Services Center.

TILLAMOOK ROW NET-ZERO-ENERGY POCKET NEIGHBORHOOD





VICINITY MAP

PROJECT DIRECTORY

OWNER

BCMC TILLAMOOK, LLC 4039 N MISSISSIPPI AVE #205 PORTLAND, OR 97227 (503) 282-1605 CONTACT: ANDREW WOODBURN

ARCHITECT

GREEN HAMMER DESIGN BUILD 1323 SE 6TH AVE. PORTLAND, OR 97214 503.804.1746 x 106 CONTACT: ERICA DUNN, AIA

CONTRACTOR

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STRUCTURAL ENGINEER

STRUCTURAL DEPARTMENT 503.334.1870 CONTACT: ZAC BLODGET

MECHANICAL ENGINEER

IMAGINENERGY 503.477.9585 CONTACT: JONATHAN COHEN

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VOL 3 - NW STRUCTURE

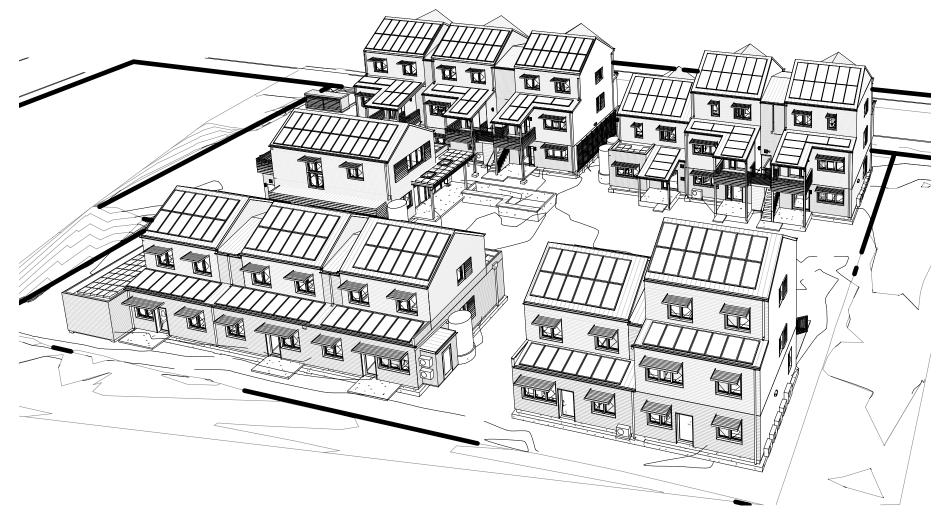
A201 NW	FIRST FLOOR PLAN
A202 NW	SECOND FLOOR PLAN
A203 NW	THIRD FLOOR PLAN
A204 NW	ROOF PLAN
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A302 NW	ELEVATIONS - EAST + WEST
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S202 NW	SECOND LEVEL FRAMING PLAN
S202L NW	SECOND LEVEL LATERAL PLAN
S203 NW	THIRD LEVEL FRAMING PLAN
S203L NW	THIRD LEVEL LATERAL PLAN
S204 NW	ROOF FRAMING PLAN

VOL 4 - NE STRUCTURE

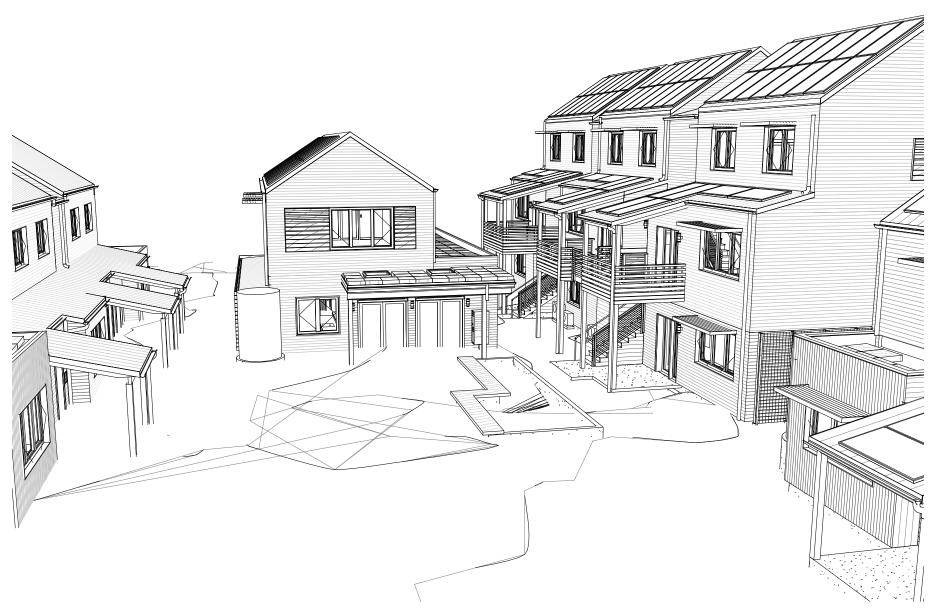
201 NE	FIRST FLOOR PLAN
A202 NE	SECOND FLOOR PLAN
A203 NE	THIRD FLOOR PLAN
\204 NE	ROOF PLAN
A301 NE	ELEVATIONS - NORTH
4302 NE	ELEVATIONS - EAST AND WEST



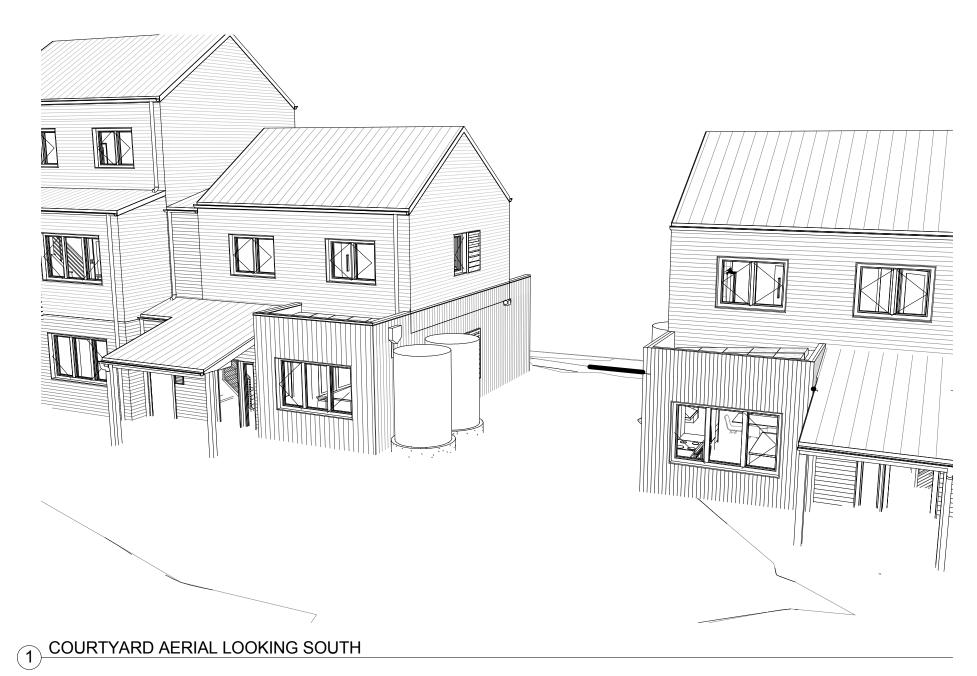
		Green hammer 1323 SE 6TH AVENUE, PORTLAND, OR 97214 (P) 503.804.1746 (F) 503.232.7924 www.greenhammer.com
A304 NE A402 NE A403 NE A602 NE A603 NE A701 NE A702 NE S201 NE S202 NE S202L NE S203 NE S203L NE	ELEVATIONS - SOUTH PERSPECTIVES BUILDING SECTIONS BUILDING SECTIONS SECOND FLOOR RCP THIRD FLOOR RCP INTERIOR ELEVATIONS KITCHENS INTERIOR ELEVATIONS BATHROOMS FOUNDATION PLAN SECOND LEVEL FRAMING PLAN SECOND LEVEL LATERAL PLAN THIRD LEVEL FRAMING PLAN THIRD LEVEL LATERAL PLAN ROOF FRAMING PLAN	STATE OF OFFICE
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A301 SW A302 SW A303 SW A402 SW A602 SW A701 SW S201 SW S202 SW S202 SW S202L SW S203 SW VOL 7 - A201 CM A202 CM A203 CM A301 CM A302 CM	ROOF PLAN ELEVATIONS - NORTH, EAST, WEST ELEVATIONS - SOUTH PERSPECTIVES BUILDING SECTIONS RCP SECOND FLOOR INTERIOR ELEVATIONS BATHROOMS FOUNDATION PLAN SECOND LEVEL FRAMING PLAN SECOND LEVEL LATERAL PLAN ROOF FRAMING PLAN COMMONS STRUCTURE FIRST FLOOR PLAN SECOND FLOOR PLAN ROOF PLAN ELEVATIONS PERSPECTIVES BUILDING SECTIONS	11/30/2016 CONSTRUCTION PACKAGES: FOUNDATION FRAME ENVELOPE MEP ROUGH-IN FINISHES ISSUE DATE REV
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2 SE AERIAL



3 COURTYARD AERIAL LOOKING WEST



PERSPECTIVE VIEWS ARE FOR GENERAL ILLUSTRATION PURPOSES ONLY. REFER TO PLAN, ELEVATIONS AND SECTION DRAWINGS FOR CONSTRUCTION INFORMATION.

LEGEND

ABBREVIATIONS

0	3" RISER, ABS OR PVC PIPE, SCHED 40
	3" LATERAL, MIN 1% SLOPE, ABS OR PVC PIPE, SCHED 40

SIDEWALL EXIT TO ROOF TERMINATION, \diamond SEE DET'L

-	A T
0	AT
NВ	AIR BARRIER
COUS	ACOUSTICAL
DJ	ADJUSTABLE
-	ABOVE FINISH FLO
LUM	ALUMINUM
APPROX	APPROXIMATE
RCH	ARCHITECT
-	
3D	BOARD
BLDG	BUILDING
BLK	BLOCK
BLKG	BLOCKING
BM	BEAM
BOT	BOTTTOM
30	BOTOM OF
3R	BACKER ROD
CAB	CABINET
PT	CARPET
) J	CONTROL JOINT
CT	CERAMIC TILE CERAMIC TILE BAS
TB	CERAMIC TILE BAS
CT CTB CLG	
LG	CEILING
LR	CLEAR
0	CASED OPENING
COL	COLUMN
CONC	CONCRETE
ONSTR	CONSTRUCTION
CONT	CONTINUOUS
CTR	CENTER
)BL	DOUBLE
DEPT	DEPARTMENT
DET	DETAIL
DIA	DIAMETER
DIM	DIMENSION
DN	DOWN
)R	DOOR
DWG	DOOR DRAWING EAST
:	EAST
	EAST
E)	EXISTING
A	EACH
IJ	EXPANSION JOINT
:L	ELEVATION
ELEC	ELECTRICAL
ELEV	ELEVATOR
MER	EMERGENCY
ENCL	ENCLOSURE
INGR	ENGINEER
Q	EQUAL
QUIP	EQUIPMENT
EXPO	EXPOSED
XP	EXPANSION
XT	EXTERIOR
	-
C	FIBER-CEMENT
D	FLOOR DRAIN
DN	
	FOUNDATION
G	FIBERGLASS
IN	FINISH
LR	FLOOR
	FACE OF
.0.	
P	FROST PROOF
RP	FIBER REINFORCE
T	FOOT, FEET
TG	FOOTING
UT	FUTURE
6A	GAUGE
SALV	GALVANIZED
	-
S L	GLASS, GLAZING
GND	GROUND
SR	GRADE
	-
SWB	GYPSUM WALL BO
SYP	GYPSUM
ΙB	HOSE BIB
IGR	JOIST HANGER
-	
IORZ	HORIZONTAL
łR	HOUR
IT	HEIGHT
D	INSIDE DIAMETER
NSUL	INSULATION
NT	INTERIOR
Т	JOINT
-	
(IT	KITCHEN
AV	LAVATORY
.KR	LOCKER
.T	LIGHT
. 1	

Area Schedule (Gross Building)				
Building Name	Area Type	Level	Area	Perimeter
COMMONS STRUCTURE	Gross Building Area	FIRST FLOOR T.O. SLAB	1329 SF	145' - 10"
COMMONS STRUCTURE	Gross Building Area	SECOND FLOOR T.O. SUBFLOOR	823 SF	113' - 10"
			2151 SF	
NE STRUCTURE	Gross Building Area	FIRST FLOOR T.O. SLAB	2547 SF	232' - 10"
NE STRUCTURE	Gross Building Area	SECOND FLOOR T.O. SUBFLOOR	2415 SF	236' - 10"
NE STRUCTURE	Gross Building Area	THIRD FLOOR T.O. SUBFLOOR	1309 SF	150' - 8"
			6270 SF	
NW STRUCTURE	Gross Building Area	FIRST FLOOR T.O. SLAB	2295 SF	246' - 10"
NW STRUCTURE	Gross Building Area	SECOND FLOOR T.O. SUBFLOOR	2462 SF	256' - 10"
NW STRUCTURE	Gross Building Area	THIRD FLOOR T.O. SUBFLOOR	1991 SF	208' - 10"
			6748 SF	
SE STRUCTURE	Gross Building Area	FIRST FLOOR T.O. SLAB	1792 SF	174' - 7"
SE STRUCTURE	Gross Building Area	SECOND FLOOR T.O. SUBFLOOR	1469 SF	171' - 4"
SE STRUCTURE	Gross Building Area	THIRD FLOOR T.O. SUBFLOOR	580 SF	96' - 8"
			3841 SF	
SW STRUCTURE	Gross Building Area	FIRST FLOOR T.O. SLAB	2671 SF	228' - 10"
SW STRUCTURE	Gross Building Area	SECOND FLOOR T.O. SUBFLOOR	1731 SF	202' - 11"
			4403 SF	
Grand total			23413 SF	

ARRIER STICAL STABLE E FINISH FLOOR OXIMATE

MAX MECH

MEMB

MTL

MFR

MFR MH MIN MISC M.O. MUL (N)

Ν

N.I.C.

NO NOM NTS OC OD O.F.A.C.I.

O.F.C.I.

0.F.O.I.

OPNG

PL PLAS

R

RAD RD REF

REFR REINF REQ

RESIL

SCHED

SECT SBFLR SF

SHT SHTG SIM SKYLT SPEC SQ S/S ST STA STB STD STL STOR STRL

SUSP SYM TB

T.O.

typ Uno Vif

W/ WP WRB

T.O. PL

RM RO

S SE

PLYWD PT PTN

MAXIMUM MECHANICAL

MEMBRANE

MANHOLE

MINIMUM

MIRROR

NEW

NORTH

NUMBER

OPENING PLATE PLASTER

PARTITION

RADIUS ROOF DRAIN REFERENCE

REFRIGERATOR

ROOM ROUGH OPENING

SOUTH STRUCTURAL ENGINEER

REINFORCED

REQUIRED

SCHEDULE

SHEATHING SIMILAR

SKYLIGHT SPECIFICATION

SQUARE STAINLESS STEEL

SECTION SUBFLOOR SQUARE FEET

SHEET

STONE

STATION

STEEL

TOP OF

TYPICAL

WITH

STONE BASE

STANDARD

STORAGE STRUCTURAL

SUSPENDED

SYMMETRICAL TOWEL BAR

TOP OF PLATE

VERIFY IN FIELD

UNLESS NOTED OTHERWISE

WATERPROOF,WATERPROOFING WEATHER RESISTANT BARRIER

RESILIENT

RISER

NOMIDER NOMINAL NOT TO SCALE ON CENTER

MANUFACTURER

MISCELLANEOUS MASONRY OPENING MULLION

NOT IN CONTRACT

OUTSIDE DIAMETER OWNER FURNISHED &

ASSEMBLED, CONTRACTOR INSTALLED

OWNER FURNISHED, CONTRACTOR INSTALLED

OWNER FURNISHED,

OWNER INSTALLED

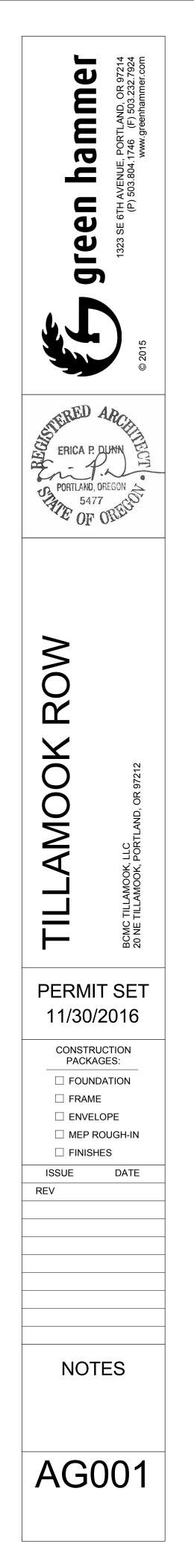
PLYWOOD PRESSURE TREATED

METAL

ROL JOINT MIC TILE BASE

ST PROOF R REINFORCED PLASTIC T, FEET

UM WALL BOARD



GOVERNING CODES

NFPA

PROJECT DESCRIPTION

ANSI A117.1

SITE AND ZONING INFORMATION

BUILDING

PLUMBING

ENERGY

SOLAR

TILLAMOOK.

PROJECT ADDRESS:

LEGAL DESCRIPTION:

BASE ZONING OF SITE:

LAND USE CASE FILE:

PROPERTY ID:

SITE AREA:

OVERLAY:

DENSITY:

FIRE

ELECTRICAL

ACCESSIBILITY

MECHANICAL

SEE SHEET A004 - FIRE LIFE SAFETY PLANS

F	IR	E

FIRE RI

SEPARATION DISTANCES (TABLE 602): SEE SHEET A004, FIRE LIFE SAFETY PLANS

EXTERIOR WALL OPENING PROTECTION (TABLE 705.8): SEE SHEET A004, FIRE LIFE SAFETY PLANS

HORIZONTAL ASSEMBLIES SEPARATING DWELLING UNITS IN THE SAME BUILDING SHALL BE A MINIMUM OF 1-HOUR FIRE RESISTANCE RATED CONSTRUCTION.

SHAFT ACCESS: 1 HR DOORS IN OTHER FIRE BARRIERS: 1 HR FIRE DOORS SHALL BE SELF-CLOSING OR AUTOMATIC CLOSING

DRAFTSTOPPING SHALL BE PROVIDED IN FLOOR/CEILING SPACES AT FIRE PARTITIONS (PARTY WALLS) BETWEEN DWELLING UNITS.

PROPERTY LINE SETBACKS: SEE SHEET A004 FOR WALL AREA CALCS

N/A

MAXIMUM

OREGON STRUCTURAL SPECIALTY CODE (OSSC)

OREGON MECHANICAL SPECIALTY CODE (OMSC)

OREGON PLUMBING SPECIALTY CODE (OPSC)

OREGON FIRE CODE (OFC)

OREGON SOLAR CODE

OREGON STRUCTURAL SP. CODE

PROJECT INCLUDES 16 NEW APARTMENT UNITS AND COMMON SPACES IN 5 BUILDINGS ORGANIZED AROUND A CENTRAL COURTYARD. NET ZERO ENERGY

PERFORMANCE IS TARGETED. UNITS INCLUDE (3) ONE-BEDROOM UNITS, (2)

STRUCTURES INCLUDE GARBAGE/RECYCLING AND COVERED BIKE PARKING AS

PEDESTRIAN ENTRY AND PRIMARY VEHICULAR ENTRY ARE LOCATED ALONG NE

16, 20 NE TILLAMOOK ST

E25' OF LOT 1 AND 2, W 40' OF N100' OF LOT 4,

PROVIDED:

16

S 50' OF LOT 4, E 10' OF N 100' OF LOT 4,

R102346, R102348, R102349, R102350,

a (ALTERNATIVE DESIGN DENSITY)

PORTLAND, OR 97212

ALBINA, BLOCK 23

LOT 5, 6, AND 7

R102351, R102352

R2 (RESIDENTIAL 2,000)

32,500SF

TWO-BEDROOM UNITS, AND (11) THREE-BEDROOM UNITS. ADDITIONAL

WELL AS A SURFACE PARKING LOT FOR 7 PARKING SPACES. PRIMARY

OREGON ELECTRICAL SPECIALTY CODE (OESC)

OREGON ENERGY EFFICIENCY SP. CODE (OEESC)

2014

2014

2014

2014

2014

2014

2013

2014

2009

2010

PROPERTY LINE SETBACKS: SEE	SHEET A004 FOR WA	L AREA CALCS	
FRONT(NORTH): REAR (SOUTH) BLDG C/D:	MIN REQ'D: 10 FT 8 FT (MAX)	PROVIDED: 10 FT >10 FT	BUIL
REAR (SOUTH) STORAGE: SIDE (WEST): SIDE (EAST) BLDG B: SIDE (EAST) BLDG C:	6 FT	5 FT >20 FT 6 FT 5 FT	AUTOI WITH 2 903.2.8
SITE LANDSCAPE AREA:	REQUIRED: 30% OF SITE	PROVIDED: 44%	FIRE A
	(9750 SF)	(14,377 SF)	SMOK
COURTYARD HARDSCAPE:	REQUIRED: < 30% 25%	PROVIDED:	SLEEP USED
		(1,926 SF OF 7,633 SF)	STANE
MAX BUILDING COVERAGE:	ALLOWED: 50% (16,250 SF)	PROVIDED: 41% (13,245 SF)	FIRE S
MAX BUILDING LENGTH:	ALLOWED: 100 FT	PROVIDED: 81'-6"	MEAN
PARKING INTERIOR LANDSCAPE:	REQUIRED: NONE (FEWER THAN	PROVIDED: 10 PARKING SPACE)	STAIRW
LANDSCAPE SCREENING:	REQUIRED: L3 AT PARKING	PROVIDED L3 AT PARKING	ENCLOS ONLY TV EXCEPT WIDTH:
PARKING AND LOADING: (TABLE 266-1)	REQUIRED: NONE	PROVIDED: 7 (INCLUDING 1 ADA)	LESS TH DIMENS
BIKE PARKING LONG TERM: SHORT TERM:	REQUIRED: 19 2	PROVIDED: 50 4	
TREE PRESERVATION TOTAL NON-EXEMPT TREES TOTAL PRESERVED TREES O SEE SHEET A100 FOR TREE	OVER 12" DIAMETER =	1	HANDR
TREE DENSITY TOTAL SITE AREA = 32,500SF			
REQUIRED TREE DENSITY = PROVIDED TREE DENSITY = 33 SMALL TREES - SEE L100	9,900SF	E	RAMPS
(6) BETULA NIGRA 'CUL (3) CORNUS NUTALLII = (9) GINKO BILOBA 'AUT	LY' HERITAGE = 1,80 = 90	00SF 00SF 00SF	SLOPE:

2,700SF 1,500SF (5) LAGERSTROEMIA X NATCHEZ = (8) STEWARTIA PSEUDOCAMILLIA = 2,400SF (2) ACER JAPONICUM = 600SF

LANDINGS:

RESISTIVE BUILDING ELEMENTS

RESISTANCE RATING REQUIREMENTS (TABLE 601):			
BUILDING ELEMENT:	RATING REQUIRED:		
STRUCTURAL FRAME:	0 HR		
BEARING WALLS - EXTERIOR :	0 HR		
BEARING WALLS - INTERIOR:	0 HR		
NONBEARING WALLS - INTERIOR:	0 HR		
FLOOR CONSTRUCTION:	0 HR		

ROOF CONSTRUCTION:	0 HR
ATION DISTANCES (TABLE 602).	

VERTICAL SEPARATION OF OPENINGS (705.8.5):

VERTICAL SEPARATION OF OPENINGS NOT REQUIRED BY USE OF EXCEPTION 1 1. 3 STORIES OR LESS IN HEIGHT

FIRE PARTITIONS (708):

FIRE PARTITIONS SHALL HAVE A FIRE RESISTANCE RATING OF NOT LESS THAN 1 HOUR. DRAFTSTOPPING TO CONTINUE THROUGH ATTIC, SEPARATING ATTIC SPACE INTO MAX 3000 SF AREA, AND COMBINING THE ATTICS OF NO MORE THAN TWO DWELLING UNITS.

HORIZONTAL ASSEMBLIES (711.3):

OPENING PROTECTIVES (SECTION 716):

CONCEALED SPACES (718.3):

FIRE RESISTIVE INTERIOR FINISHES (TABLE 803.5):

SPRINKLERED: CLASS C FINISHES FOR ALL EXIT STAIRWAYS/ENCLOSURES AND ALL ROOMS AND ENCLOSED SPACES.

_DING FIRE PROTECTION + SUPPRESSION

DMATIC FIRE SPRINKLERS: ALL R -2 OCCUPANCY BUILDINGS WILL BE EQUIPED AN AUTOMATIC FIRE SPRINKLER SYSTEM IN ACCORDANCE WITH NFPA 13R PER 2.8 AND 903.3.1.2.

ALARM: MANUAL FIRE ALARM SYSTEM REQUIRED PER 907.2.9.1

KE ALARM: REQUIRED ON THE CEILING OR WALL OUTSIDE EACH SEPARATE PING AREA IN THE IMMEDIATE VICINTY OF BEDROOMS, REQUIRD IN EACH ROOM D FOR SLEEPING PURPOSES. REQUIRED IN EACH STORY WITHIN A DWELLING UNIT.

IDPIPE SYSTEM: NOT REQ'D

SPRINKLER AND FIRE ALARM PERMITS TO BE OBTAINED SEPARATELY

ANS OF EGRESS

WAYS (1009)

SURE: AL	L INTERIOR STAIRWAYS ARE EITHER WITHIN AN R-2 DWELLING OR SERVE
WO STOF	RIES AND THEREFORE DO NOT REQUIRE ENCLOSURE PER 1009.3,
TION 1 & 2	2.
: ALL STA	IRWAYS MIN WIDTH = 36" PER 1009.4 EXCEPTION 1. ALL STAIRS SERVE
HAN 50 O	CCUPANTS.
SIONS:	INTERIOR STAIRS WITHIN AN R-2 DWELLING:
	MAX RISER HEIGHT = 7 3/4"
	MIN TREAD DEPTH = 10"
	NOSING: 3/4" - 1 1/4" (REQ'D FOR TREAD DEPTH < 11")
	ALL OTHER STAIRS:
	MAX RISER HEIGHT = 7" (MIN 4")
	MIN TREAD DEPTH = 11"
RAILS:	ONE SIDE ONLY WITHIN DWELLING UNITS (1009.15, EXCPT 2)
	BOTH SIDES, ALL OTHER LOCATIONS
	34 - 38" ABOVE NOSINGS
	PROFILE: 1 1/2" DIAM CIRCULAR OR 1" X 2" RECTANGULAR
	1 1/2" MIN CLEARANCE FROM WALL, 4 1/2" MAX PROJECTION
	EXTENSION AT TOP: 12" HORIZONTAL
	EXTENSION AT BOTTOM: 12" SLOPED WITH RETURN TO WALL OR FLOOR
(4040)	
<u>6 (1010)</u>	
	MIN 1:12 FOR MEANS OF EGRESS, OTHERWISE MIN 1:8.
	MAX CROSS-SLOPE 2%
	30" MAX

36" MIN LENGTH WITHIN NON-ACCESSIBLE R-2 DWELLING UNITS

60" MIN LENGTH FOR ACCESSIBLE ROUTE

48" MIN LENGTH FOR NON ACCESSIBLE ROUTE

REQ'D BOTH SIDES OF RAMPS WITH >6" RISE

MEANS OF EGRESS - CONT.

GUARDS (1013)

WHERE REQ'D	ELEVATION CHANGES >30"
HEIGHT:	42" MIN EXCEPT AS FOLLOWS
	36" MIN WITHIN R-2 DWELLING
	34" MIN FOR STAIRS WITHIN R-
OPENINGS:	4 3/8" OPENINGS ALLOWED WI
WINDOW SILLS:	36" MIN SILL HEIGHT IF 6 FT AB

EXIT ACCESS (1014)

COMMON PATH	I OF EGRESS TRAVEL:
USE	MAX ALLOWED

B,S	100 FT (OCCUP<30)
R-2	125 FT (NFPA 13R SPRINKLER)

EXIT & EXIT ACCESS DOORWAYS (1015)

ONE REQ'D FROM R-2 DWELLING UNITS WITH OCCUP LOAD < 20 & NFPA 13R SPRINKLER ONE REQ'D FROM GROUP B AND S SPACES WHERE OCCUPANCY < 49

EGRESS BALCONIES (1019)

WALL SEPARATION: UNPROTECTED OPENINGS ALLOWED ADJACENT TO UNRATED EXTERIOR WALLS (1018.5, EXCPT 5). LOCATION: MIN 10' FIRE SEPARATION DISTANCE

EXTERIOR EXIT STAIRWAYS AND RAMPS (1026)

LOCATION: MIN 10' FIRE SEPARATION DISTANCE (SUBJECT TO APPEAL) **PROTECTION:** NOT REQ'D SINCE NOT REQ'D TO BE ENCLOSED PER 1009.3

EMERGENCY ESCAPE & RESCUE (1029)

MIN NET CLEAR AREA:	5.7
MIN NET CLEAR HEIGHT:	24"
MIN NET CLEAR WIDTH:	20"
MAX HEIGHT FROM FLOOR:	44"

ENERGY CODE REQUIREMENTS

THE DEVELOPMENT IS A NET-ZERO ENERGY PROECT INCLUDING HIGHLY INSULATED WALLS. TRIPLE-PANE WINDOWS, STRINGENT AIRTIGHTNESS AND ENERGY-RECOVERY VENTILATION.

COMPLIANCE PATH: PRESCRIPTIVE PATH

SECTION 502:

BUILDING ELEMENT:	MIN. ALLOWE
ROOF (ATTIC)	R-38
WALLS (WOOD FRAMED)	R-21
	D 7 Foi

WALLS (BELOW GRADE)	R-7.5ci		
FLOORS (UNHEATED SLAB)	R-10 FOR 24" BELOW		
WINDOWS AND DOORS (>50% GLAZED)			
	U= 0.35		

WINDOW/WALL RATIO SKYLIGHTS	
OPAQUE DOOR, SWING OPAQUE DOOR, ROLL UP	

SHGC = 0.400.3 CFM/SF 30% MAX U=0.60 SHGC = 0.40 U=0.70 U=0.50

0.4 CFM/SF

A CONTINUOUS AIR BARRIER IS PROVIDED TARGETING 0.08 CFM/SF @ 50PA WHOLE BUILDING. THE AIR BARRIER CONSISTS OF TAPED PLYWOOD SEAMS AT ROOF AND WALLS, TAPED TO A SEALED CONCRETE SLAB. ALL PENETRATIONS OF THE AIR BARRIER SHALL BE SEALED WITH AN APPROVED TAPE OR SEALANT.

PLUMBING FIXTURES

OCCUPANCY	OCCUP LOAD	WATER CLOSET
FLOOR 1 SMALL ASSEMBLY BUSINESS (CRAFT/OFFICE) STORAGE FLOOR 1 - REQUIRED FLOOR 1 - PROVIDED	38 6 3	38/75 = 0. 6/25 = 0.2 <u>3/100 = 0.</u> 0.78 1
FLOOR 2 FITNESS	19	19/25 = 0.

*ALL RESIDENTIAL DWELLING UNITS (R-2) HAVE AT LEAST ONE WATER CLOSET, LAVATORY, AND BATHTUB.

1

RADON CONTROL

FLOOR 2 - PROVIDED

SEE RADON CONTROL PLAN

UNITS R-2 DWELLING UNITS (MAX 38" IF HANDRAIL) **THIN R-2 DWELLING UNITS** BOVE GRADE (OR PROVIDE GUARD)

PROVIDED 77 FT <60 FT

SF (5.0 SF AT GRADE LEVEL)

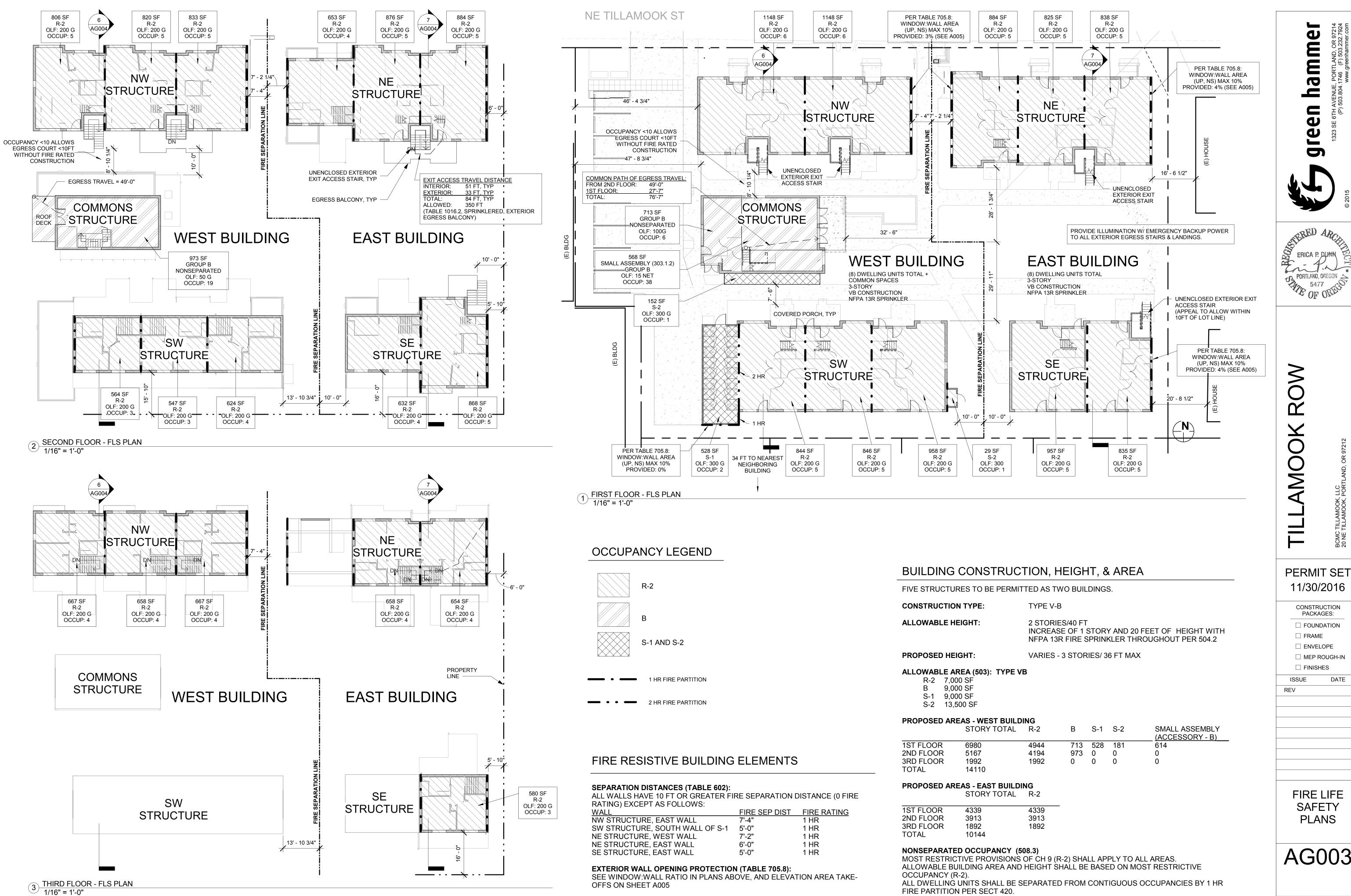
/ED:

PROVIDED: R-5.15 MIN R-29.6 NO WALLS BELOW GRADE R-16.7ci U=0.14 SHGC = 0.50, 0.30 VARIES, 17% MAX

NO SKYLIGHTS U=0.70 U=0.50

LAVATORY FOUNTAIN 38/200 = 0.19 0 (DINING) .51 .24 6/40 = 0.15 .03 3/100 = 0.03 0.37 19/40 = 0.48

C dreen hammer	© 2015
PORTLAND, 547 OF	(Se.) 4
TILLAMOOK ROW	BCMC TILLAMOOK, LLC 20 NE TILLAMOOK, PORTLAND, OR 97212
PERMI 11/30/ CONSTRU PACKA D FOUNI FRAMI FRAMI ENVEL MEP F FINISH ISSUE REV	2016 UCTION GES: DATION E LOPE
ZONII	
AG	002



WALL	FIRE SEP DIST	FIRE RATING
NW STRUCTURE, EAST WALL	7'-4"	1 HR
SW STRUCTURE, SOUTH WALL OF S-1	5'-0"	1 HR
NE STRUCTURE, WEST WALL	7'-2"	1 HR
NE STRUCTURE, EAST WALL	6'-0"	1 HR
SE STRUCTURE, EAST WALL	5'-0"	1 HR

E AREA (503):	٦
7,000 SF	
9,000 SF	
9,000 SF	
13,500 SF	
	7,000 SF 9,000 SF 9,000 SF

1ST FLOOR	6980
2ND FLOOR	5167
3RD FLOOR	1992
TOTAL	14110

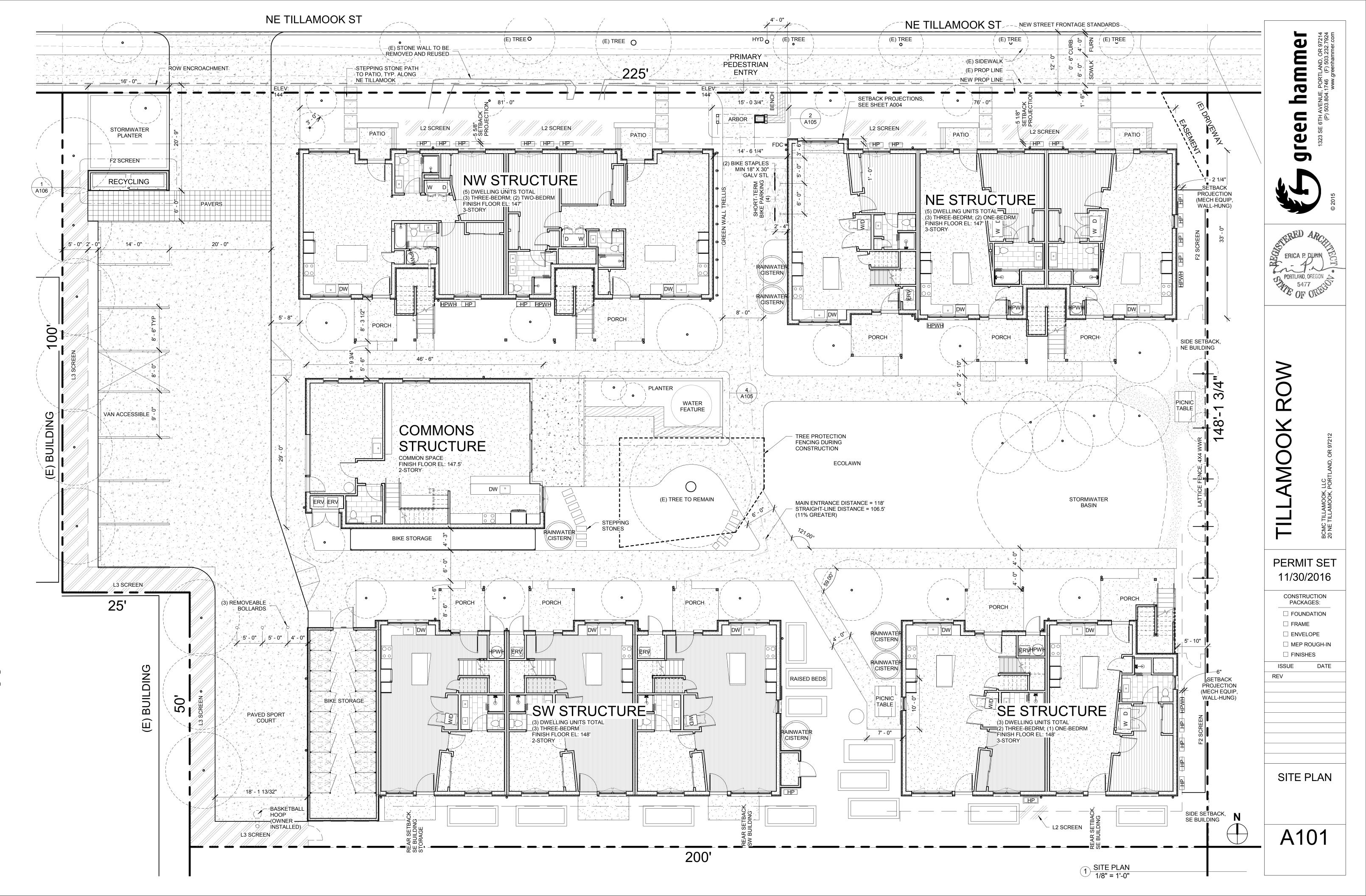
1ST FLOOR	4339
2ND FLOOR	3913
3RD FLOOR	1892
TOTAL	10144

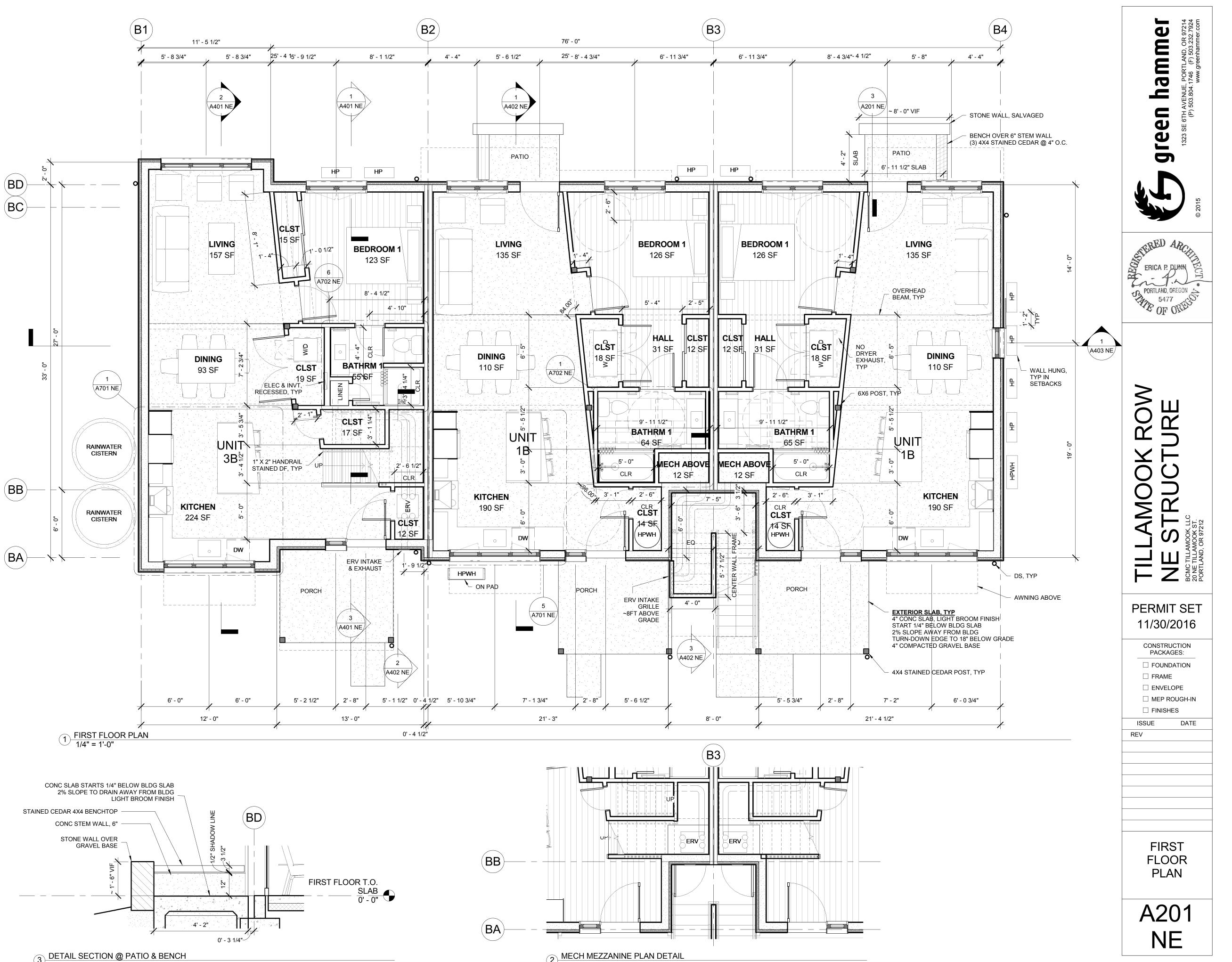
FIRE PARTITION PER SECT 420.

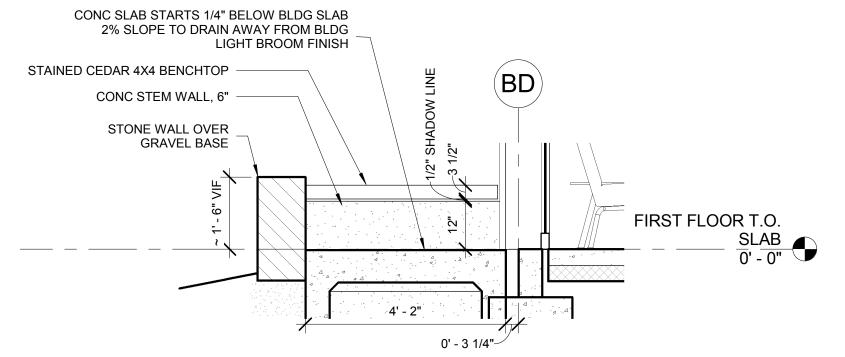
BUILDI DTAL	NG R-2	В	S-1	S-2	SMALL ASSEMBLY (ACCESSORY - B)
	4944	713	528	181	614
	4194	973	0	0	0
	1992	0	0	0	0

4339
3913
1892

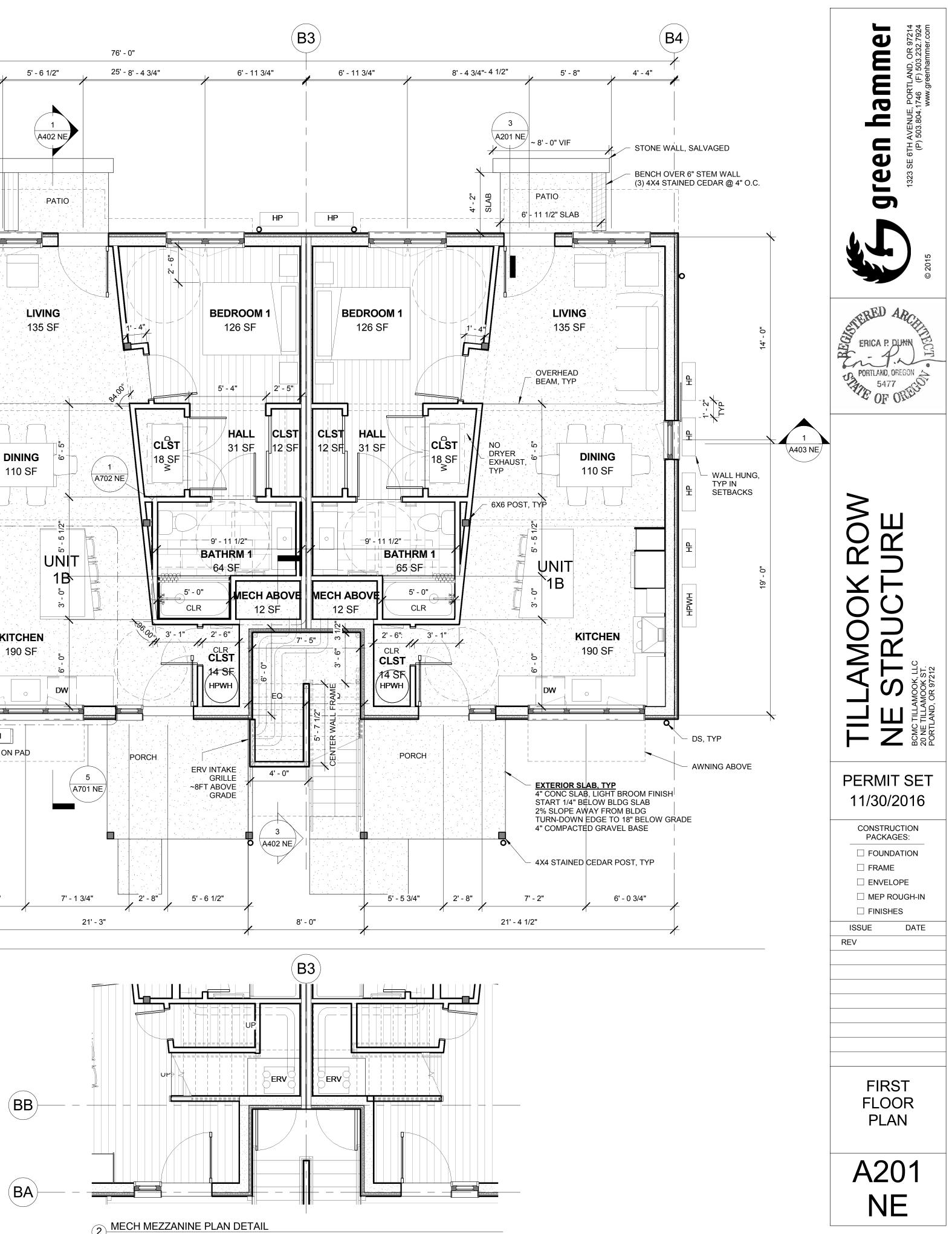
F green hamr	1323 SE 6TH AVENUE, PORTLAND (P) 503.804.1746 (F) 50 www.greenh
PORTLAND, OF	S102 © 2015
TILLAMOOK ROW	BCMC TILLAMOOK, LLC 20 NE TILLAMOOK, PORTLAND, OR 97212
PERMIT 11/30/2 CONSTRUC PACKAG FOUND/ FRAME ENVELC MEP RC FINISHE ISSUE REV	2016 CTION GES: ATION DPE DUGH-IN
FIRE L SAFE PLAN	TY NS



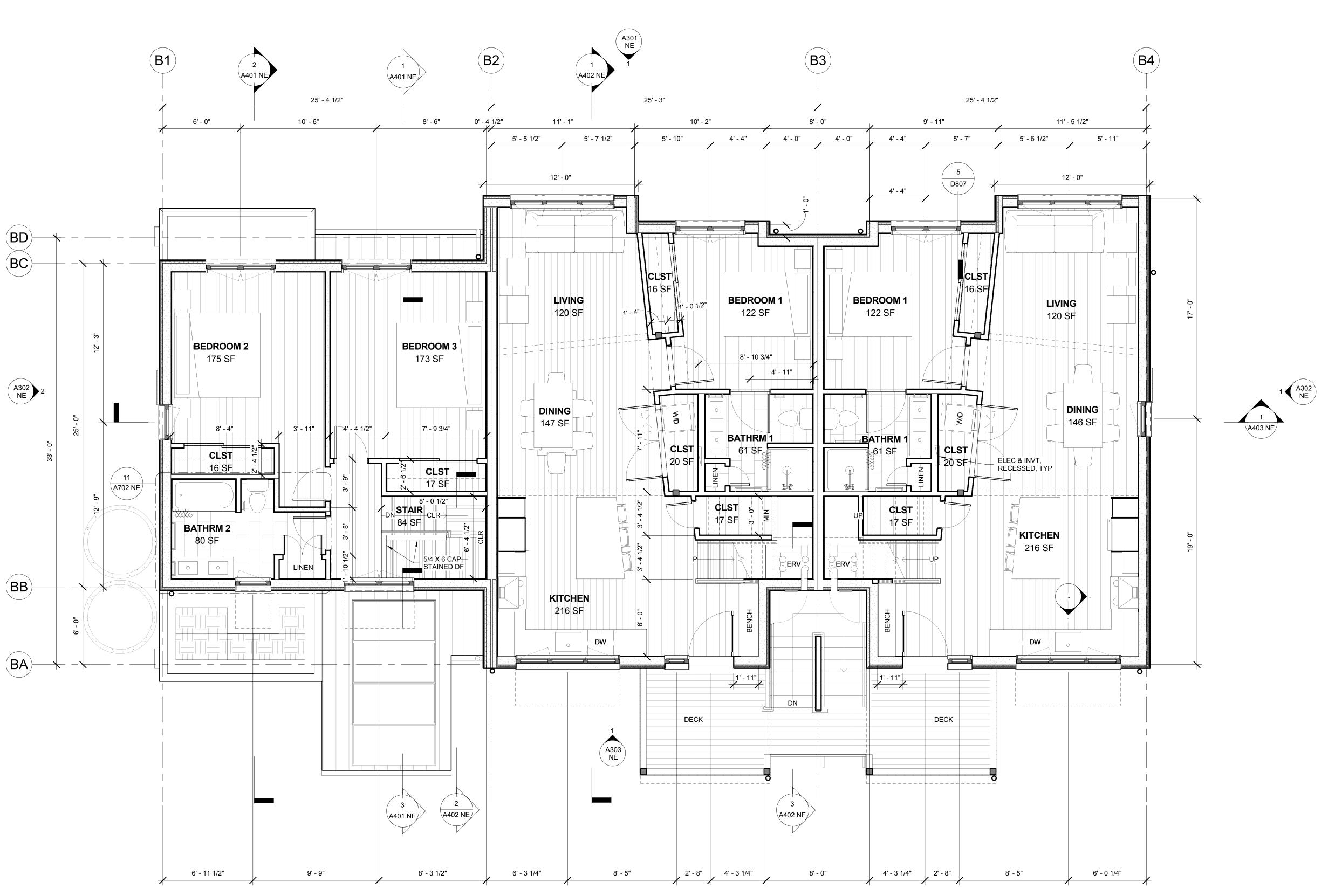




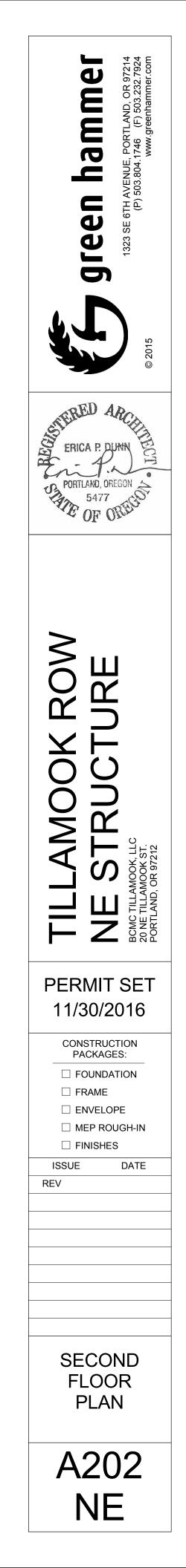
3 DETAIL SECTION @ PATIO & BENCH 1/2" = 1'-0"

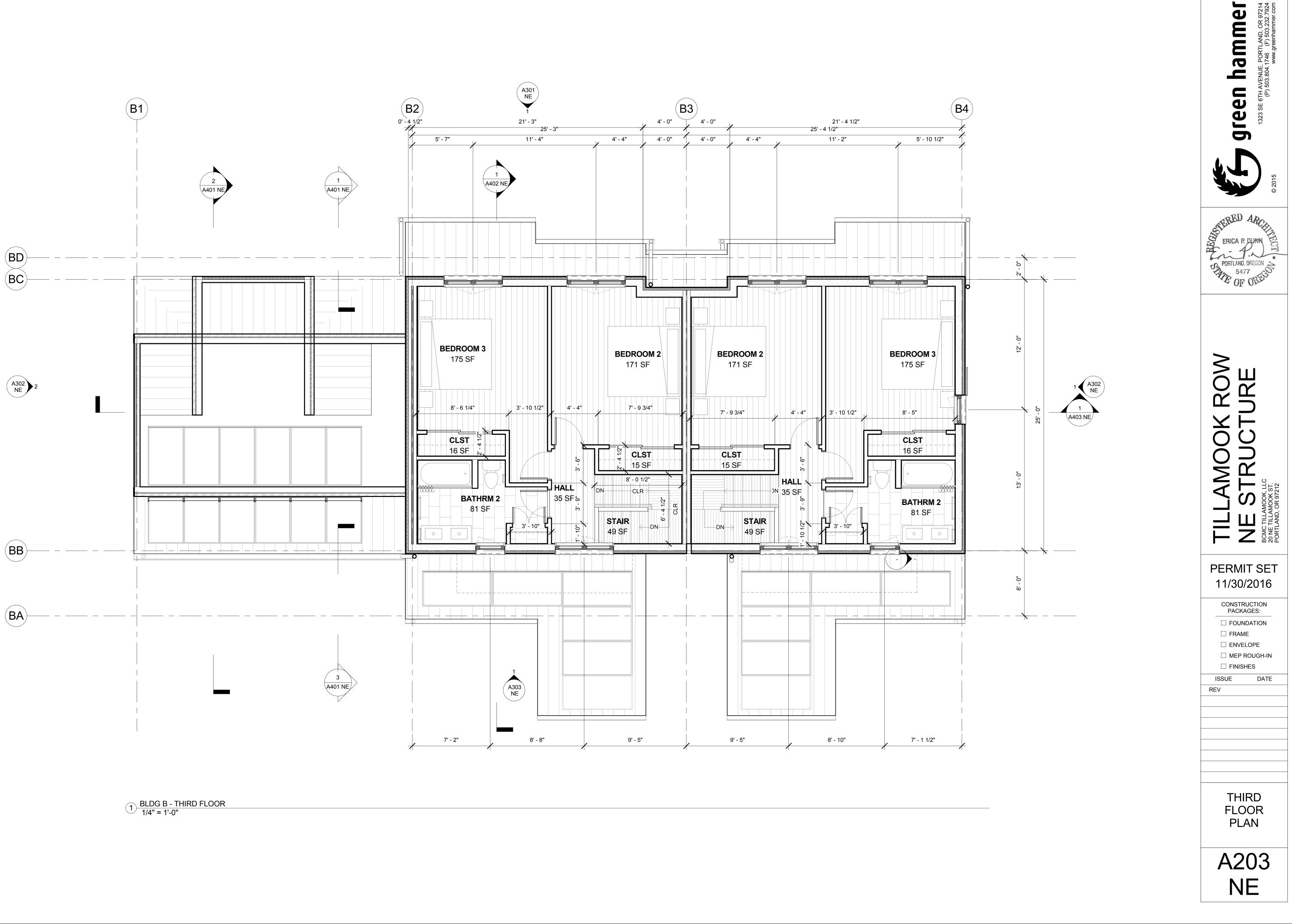


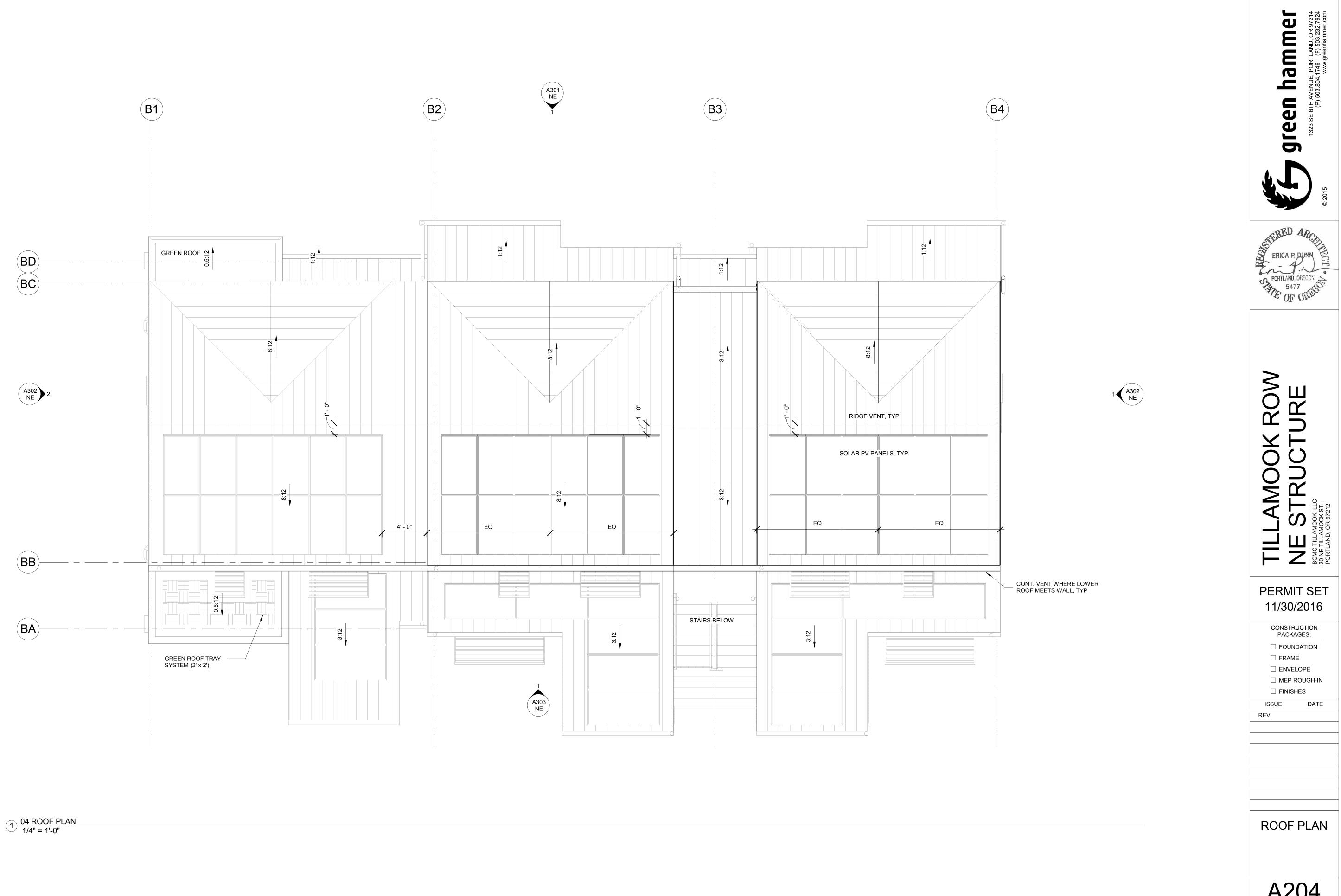
2 MECH MEZZANINE PLAN DETAIL 1/4" = 1'-0"



1 BLDG B - SECOND FLOOR 1/4" = 1'-0"









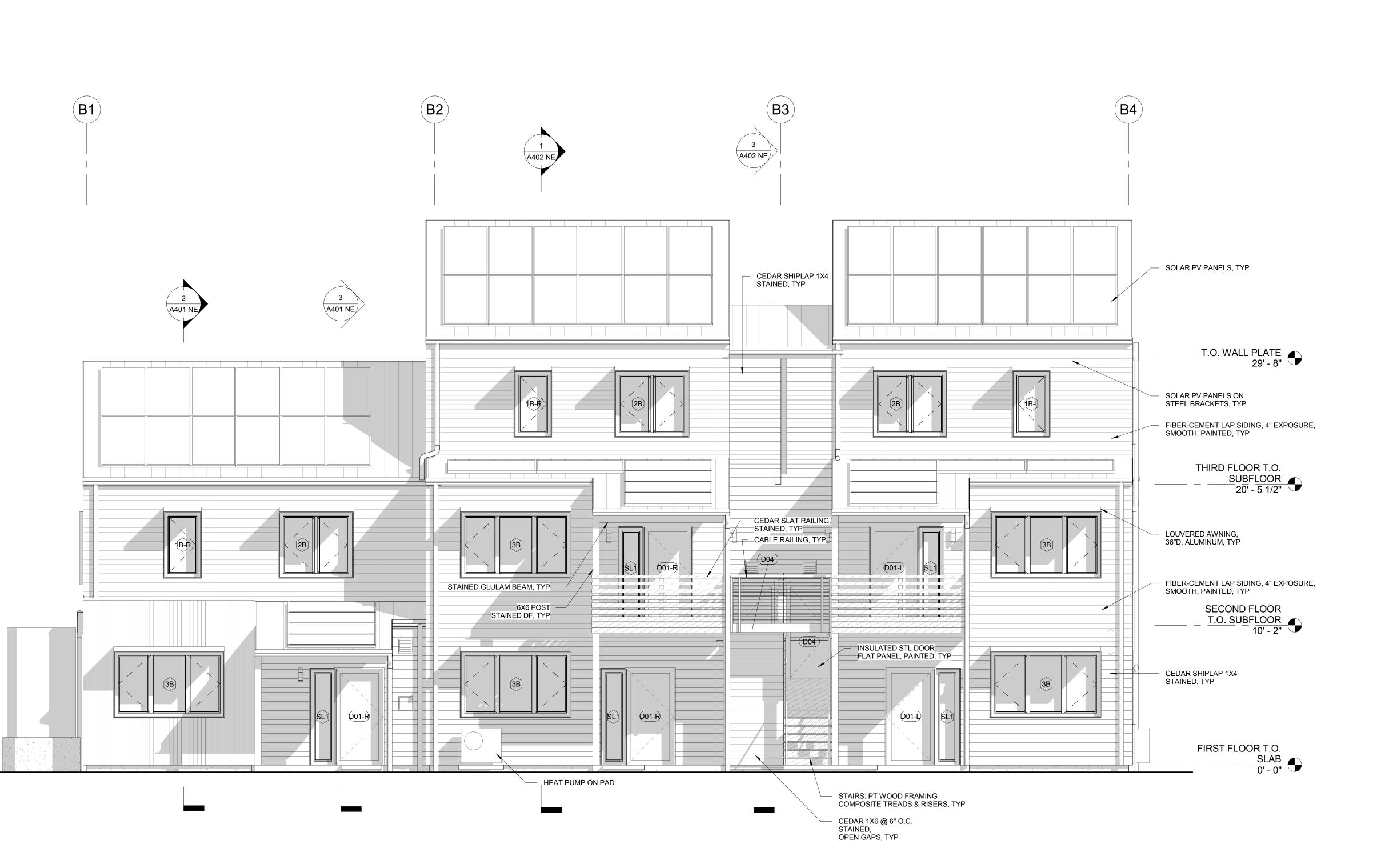


1 <u>NORTH</u> 1/4" = 1'-0"

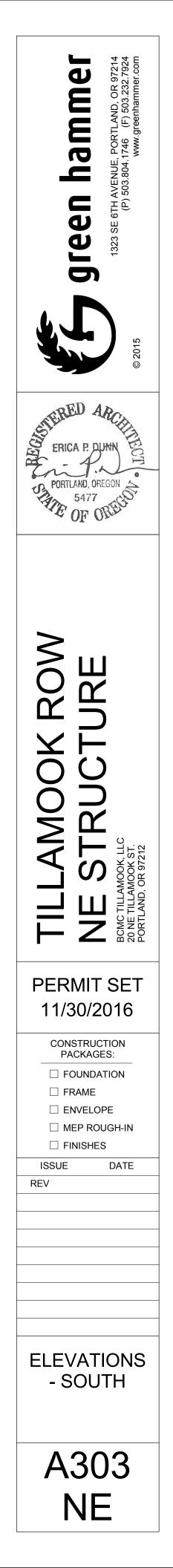
	© 2015
	PORTLAND, OREGON A 5477 OF ORDIO
— STANDING SEAM METAL ROOF, TYP	S S S S S S S S S S S S S S S S S S S
HALF-ROUND GUTTER GALV STL, TYP THIRD FLOOR T.O. 	JCTUI
LOW ROOF 19' - 4 1/2" — FIBER-CEMENT LAP SIDING, 4" EXPOSURE, SMOOTH, PAINTED, TYP — GALV STL FLASHING	LAMOOK, LLC LAMOOK, LLC LAMOOK ST. UD, OR 97212
SECOND FLOOR T.O. SUBFLOOR 10' - 2"	
 VERT CEDAR SHIPLAP 1X6 STAINED, TYP 	PERMIT SET 11/30/2016
	CONSTRUCTION PACKAGES:
BAY CANTILEVERS OVER FOUNDATION	□ FINISHES ISSUE DATE REV
	ELEVATIONS - NORTH
	A301 NE



A302 NE



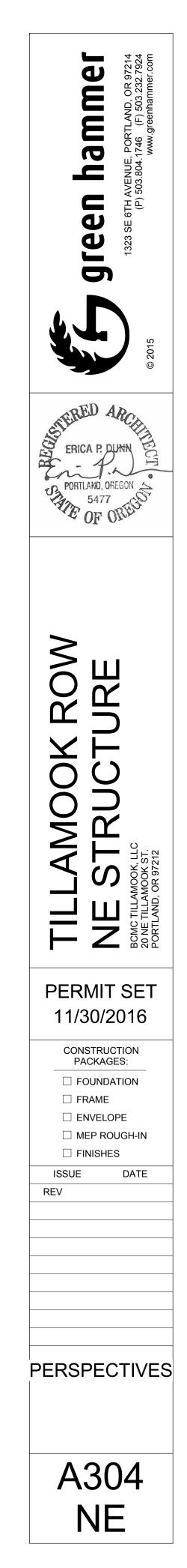
1 <u>SOUTH</u> 1/4" = 1'-0"

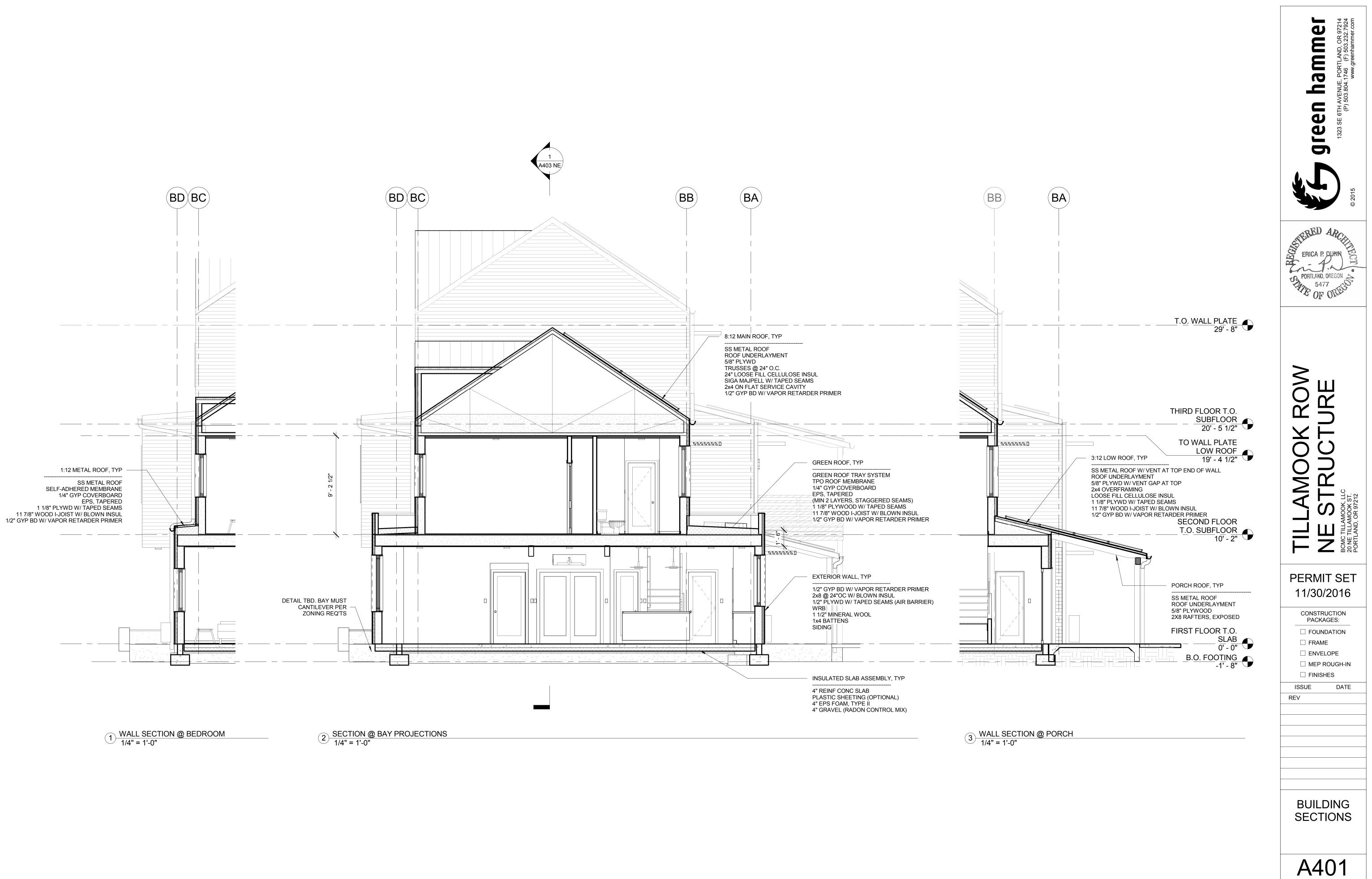




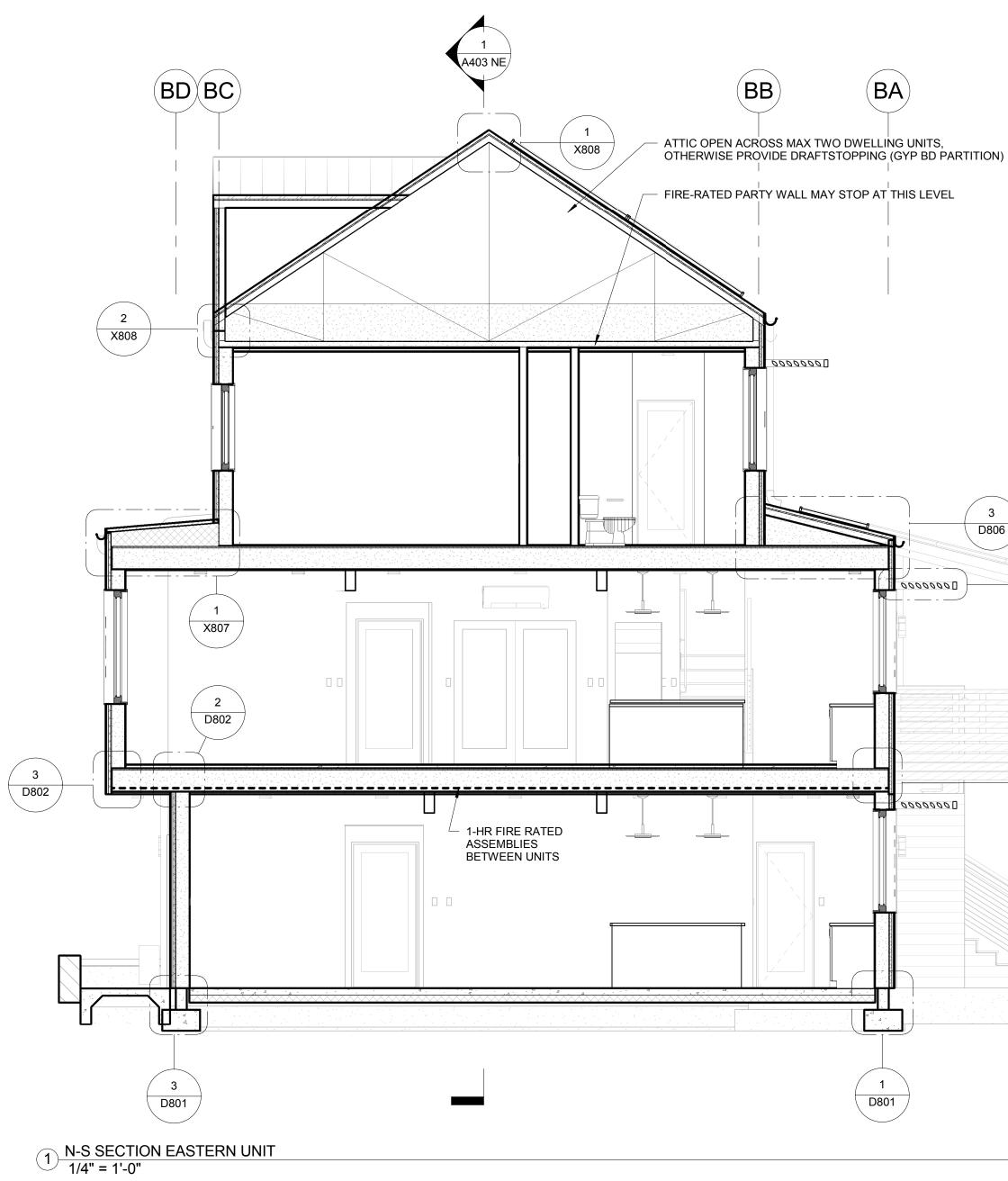
1 Perspective - NE



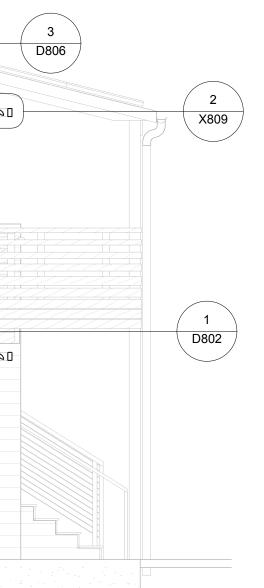


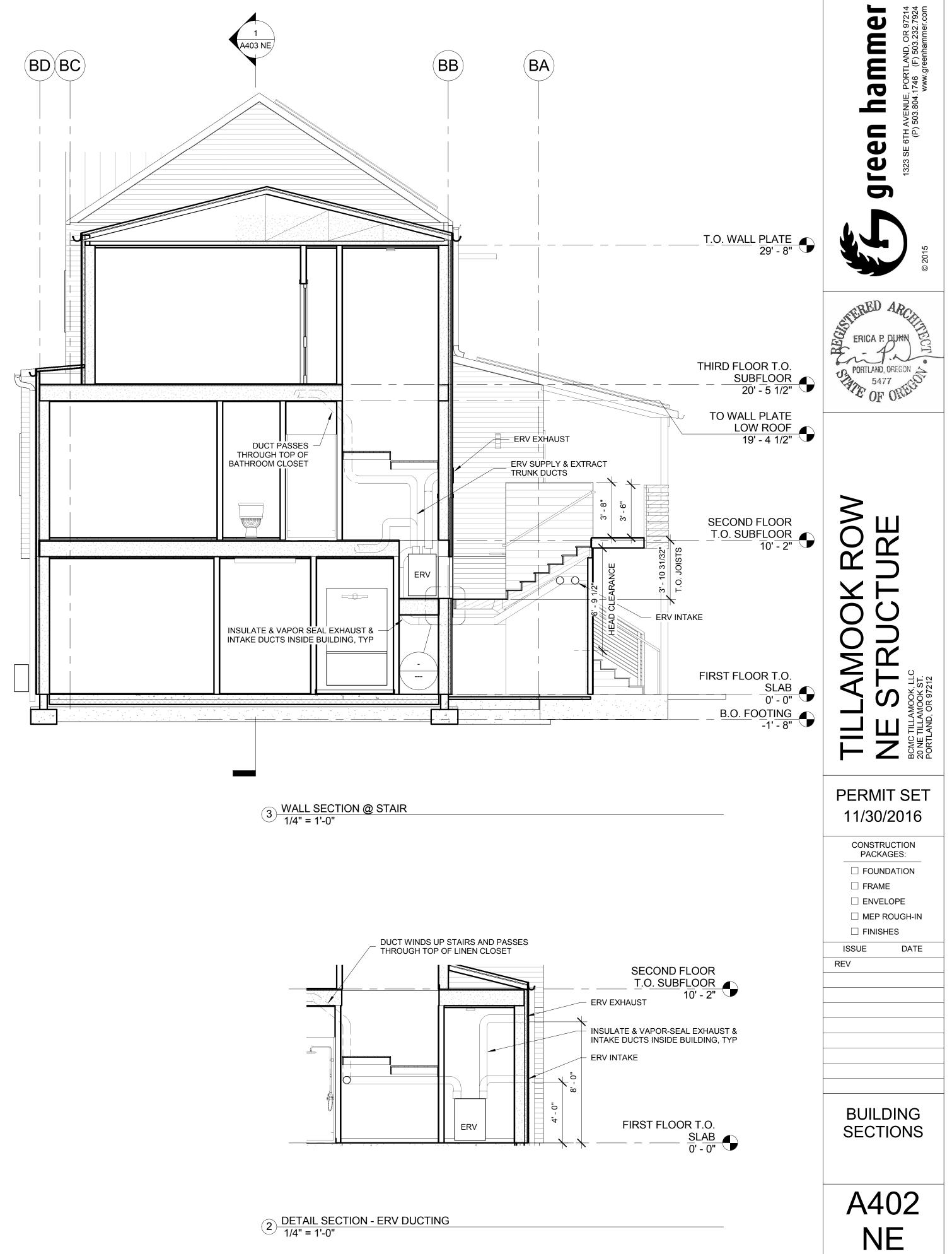


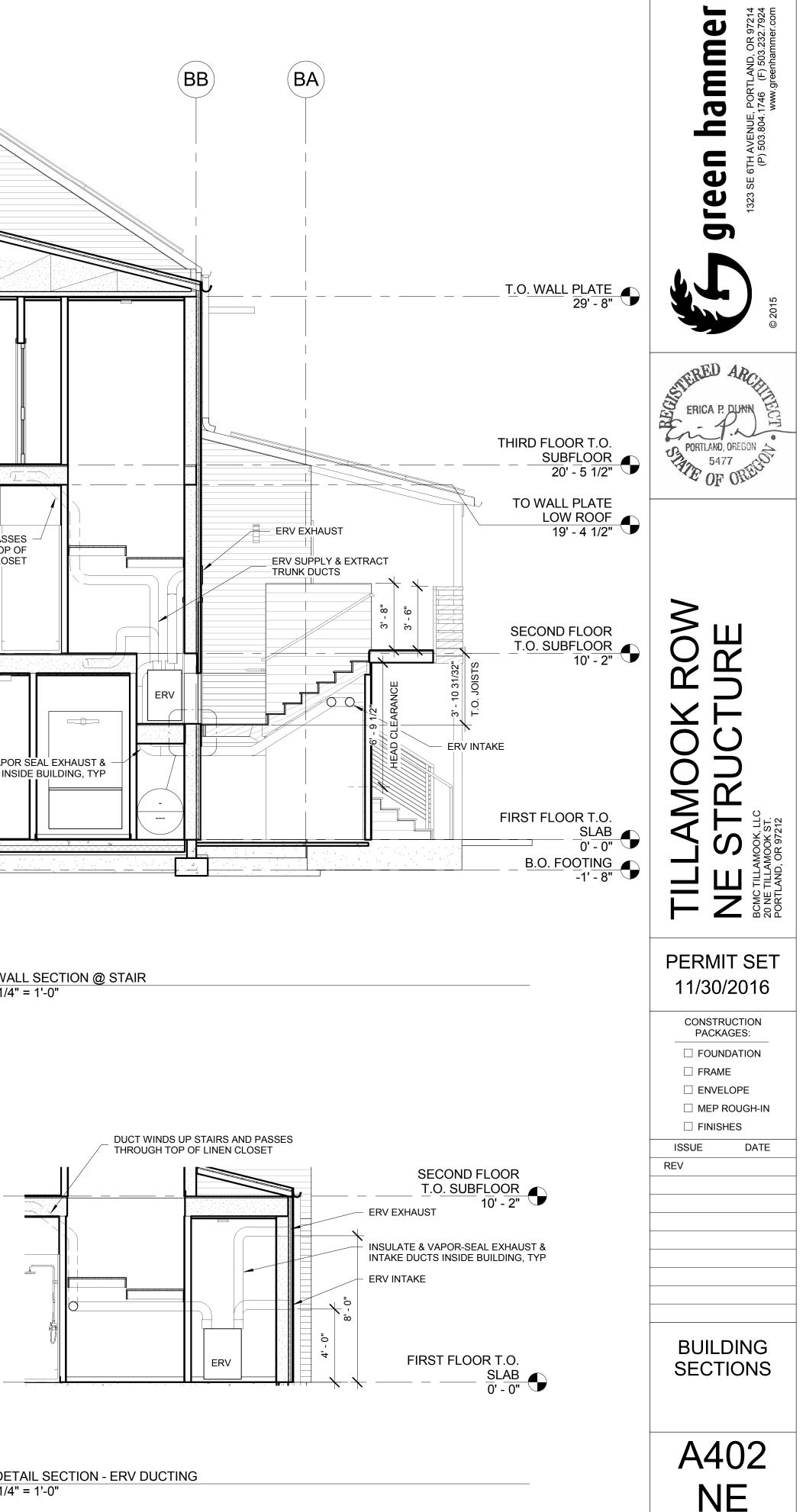
NE

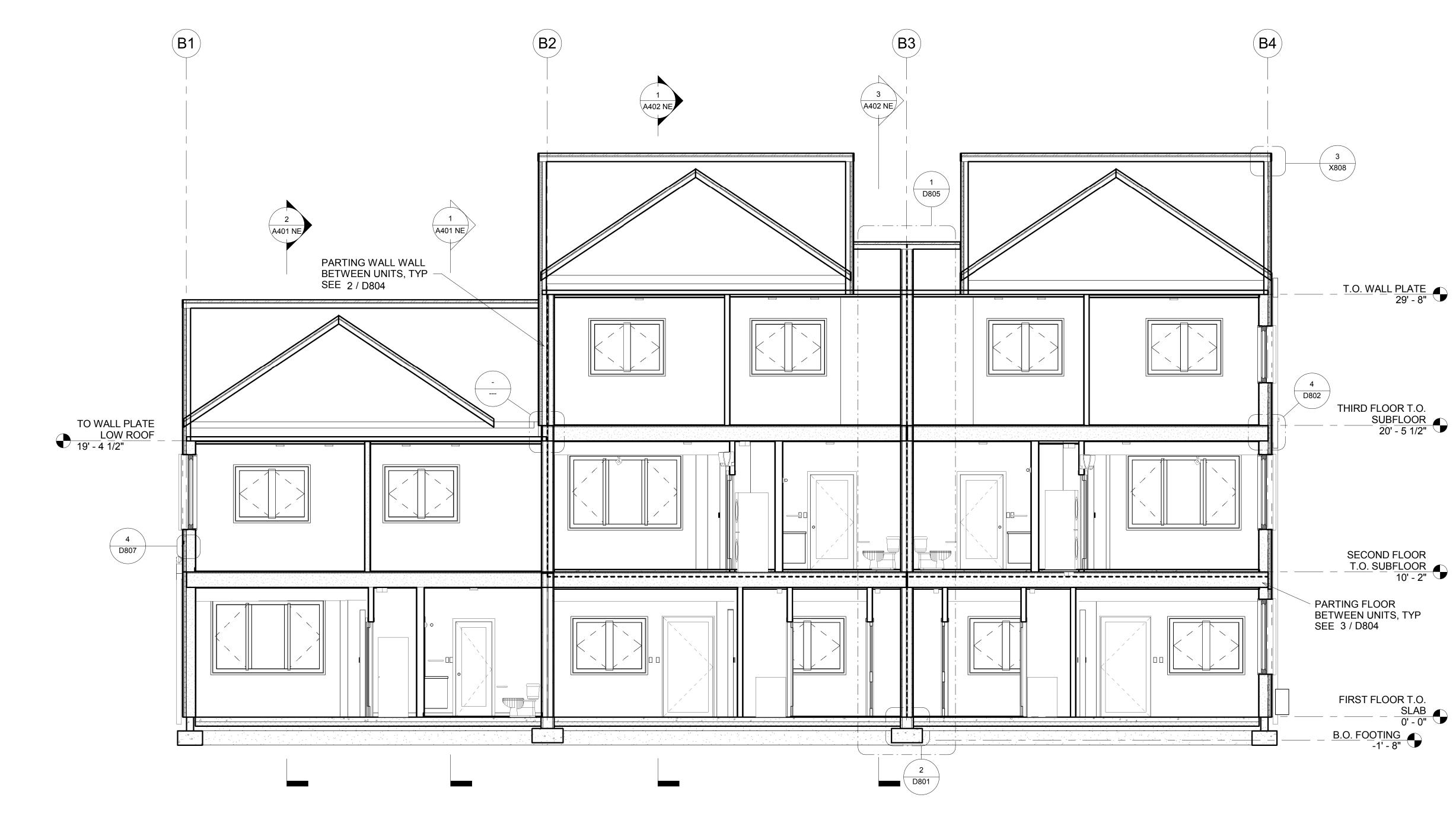


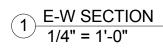


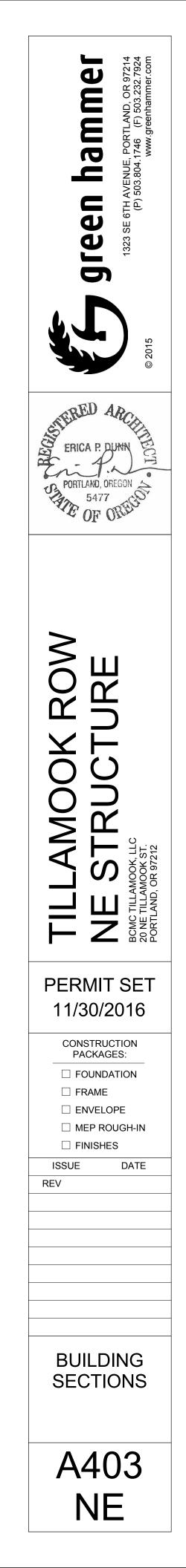


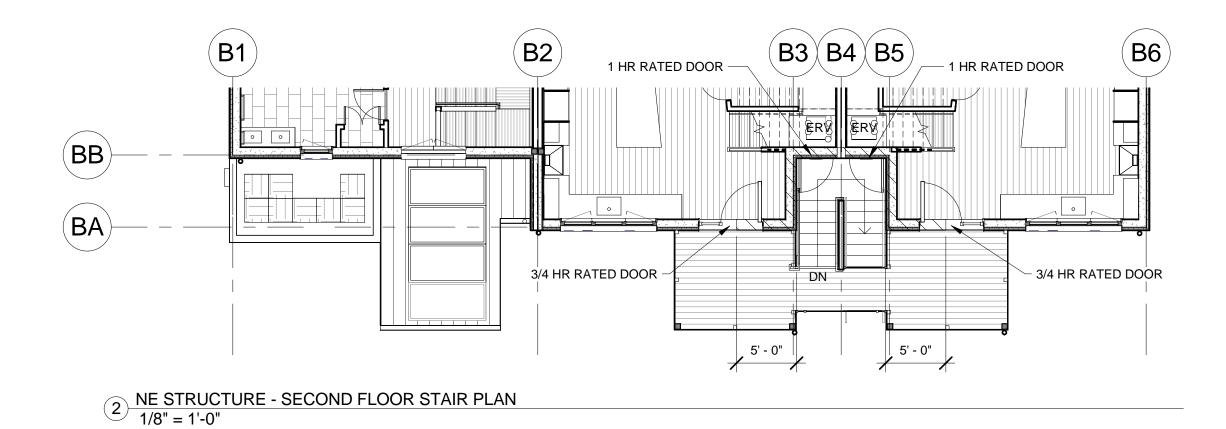


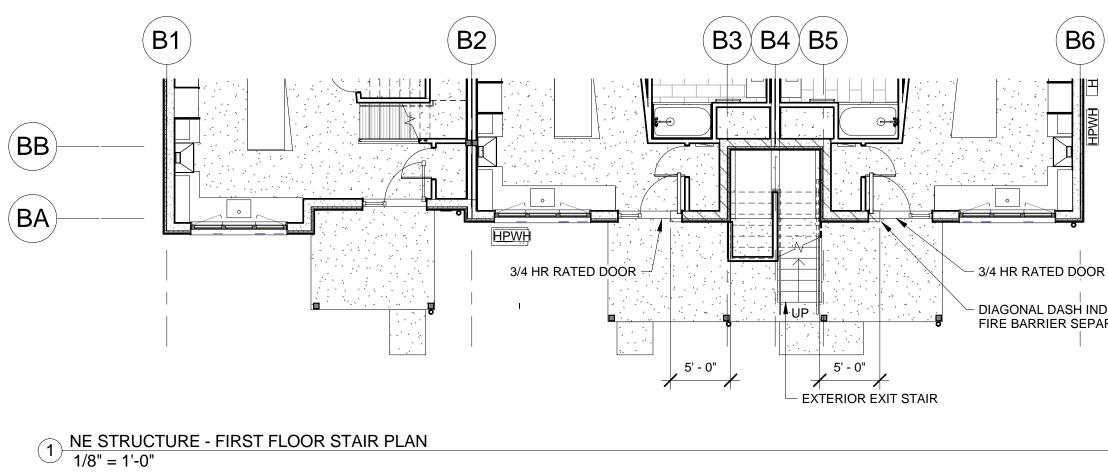








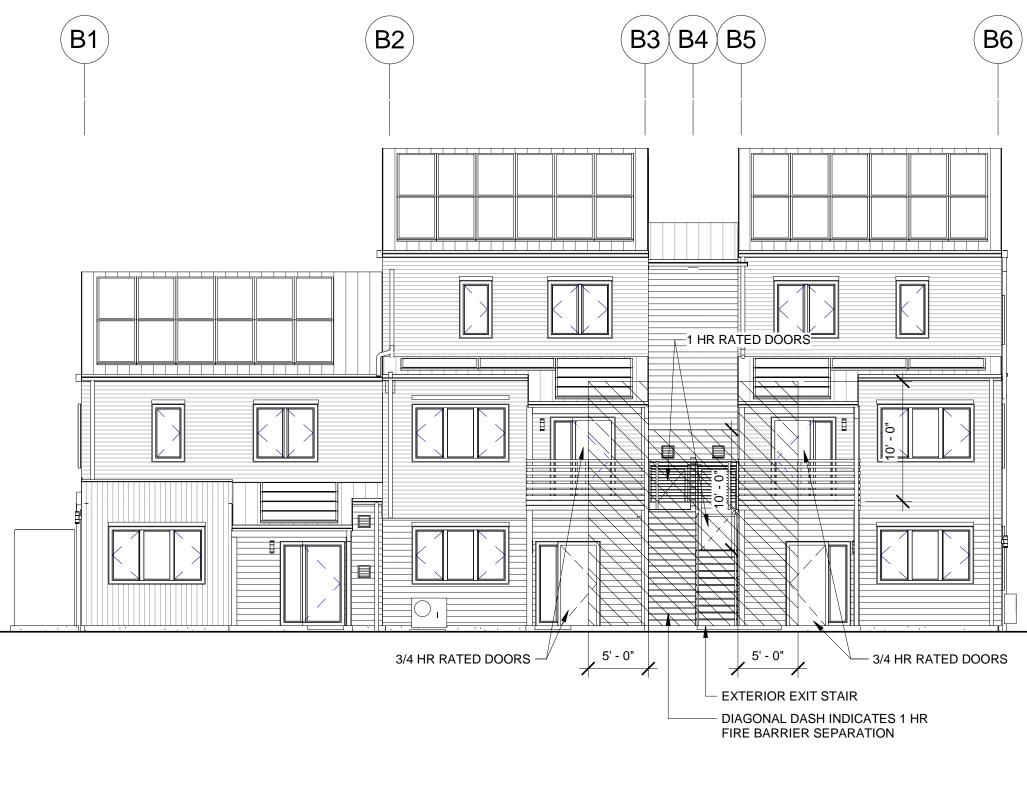




2/17/2017 4:44

DIAGONAL DASH INDICATES 1 HR FIRE BARRIER SEPARATION, TYP



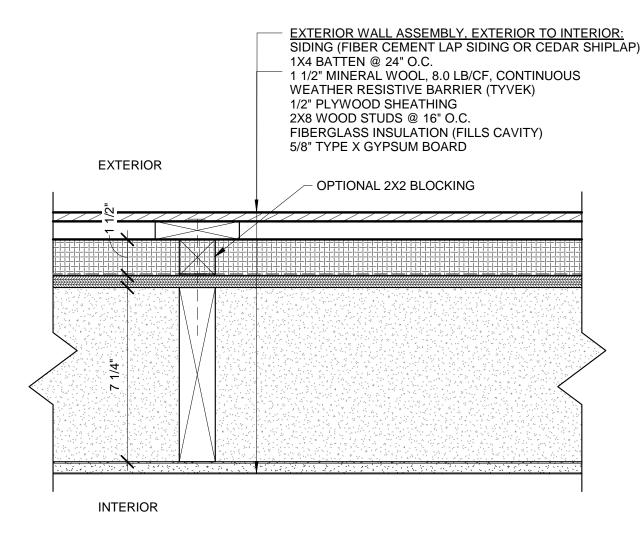


 $1 \frac{\text{NE STRUCTURE - SOUTH ELEVATION}}{1/8" = 1'-0"}$

Σ

2/17/2017 4:44:09





EXTERIOR WALL PLAN SECTION 3" = 1'-0"

OSSC 722.6.2 - WOOD WALL ASSEMBLY FIRE RESISTANCE CALCULATION

REQUIRES

722.6.2.3 prescribes 20 minutes of fire resistance for 2x4 wood studs at 16"o.c. 722.6.2.5 prescribes 15 minutes of fire resistance to various types of insulation filling a stud cavity.

PROPOSED

Apply 20 minutes of fire resistance to 2x8 wood studs at 16"o.c.

Apply 15 minutes of fire resistance to a 1 1/2" layer of continuous mineral wool insulation (8.0 lb/cf) on the exterior side of the stud wall, as shown in the wall assembly attached.

The assembly would then have the following fire resistance as calculated per OSSC 722.6.2.1:

FIRE EXPOSURE FROM INTERIOR:

5/8" TYPE X GYPSUM BOARD	40 MIN	TABLE 722.6.2
2x8 WOOD STUDS 16" O.C.	20 MIN	TABLE 722.6.2
GLASS FIBER CAVITY INSULATION	15 MIN	TABLE 722.6.2
TOTAL	75 MIN	

FIRE EXPOSURE FROM EXTERIOR:

15 MIN	TABLE 722.6.2
10 MIN	TABLE 722.6.2
20 MIN	TABLE 722.6.2
15 MIN	TABLE 722.6.2
60 MIN	
	10 MIN 20 MIN 15 MIN

Mineral wool to be held in place by 1x4 battens fastened to wall with #8 screws at 24" O.C. max, with min 1" embedment into studs.

REASON

Using larger wood studs (i.e. 2x8 instead of 2x4) is acceptable for UL ratings without reducing the assembly fire resistance rating.

Mineral wool proposed is a Non-Combustible material with a Flame Spread rating of 0 and a melting point of 2,150 degrees F (see attached data sheet). A continuous 1 1/2" thick layer of this material would have at least a 15 minute fire resistance, which is equivalent to, for example, a layer of 19/32" plywood per Table 722.6.2 (1). By contrast plywood is a combustible material with a flame spread rating of approximately 100. Further, 1 1/2" of 8.0 pcf mineral wool results in 1.0 psf density of mineral wool material, whereas 722.6.2.5 prescribes 15 minutes of fire resistance to 3.3 pcf mineral wool within a 2x4 stud cavity (which is not continuous) which achieves 0.96 psf density of mineral wool material.

A desired option is to allow 2x2 blocking to break the mineral wool, similar to studs breaking stud cavity insulation, to help keep the siding in a uniform plane.

A similar appeal was approved by the City of Seattle, substituting a continous layer of 1 1/4" mineral wool insulation (8 lb/cf) for a layer of 5/8" Type X gypsum board. See attached.

2 (1) 2 (2) 2 (5)

> (5) (1) (2)

> (5)





General Product Information:

ROXUL® products are mineral wool fibre insulations made from basalt rock and slag. This combination results in a noncombustible product with a melting point of approximately 2150°F (1177°C), which gives it excellent fire resistance properties. ROXUL mineral wool is a water repellent yet vapour permeable material.

Compliance and Performance:

Technical Product Information



BOARD INSULATION 07210* BOARD INSULATION 07 21 13**

Description & Common Applications:

The COMFORTBOARD[™] IS product is a rigid mineral wool insulation sheathing board that is non-combustible, water repellent, fire resistant and sound absorbent. This product is an exterior non-structural insulation sheathing board for high performance residential wall systems.

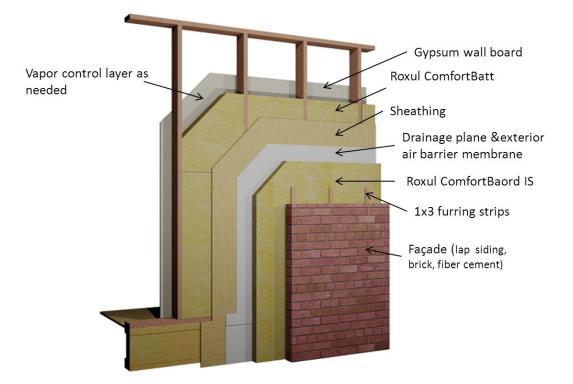
ASTM C 612 CAN/ULC-S702 CCMC Evaluation Listing	Mineral Fiber Block and Board Thermal Insulation Mineral Fibre Thermal Insulation for Buildings	Type IVB, Complies Type 1, Complies 13573-L
Fire Performance: ASTM E 136 CAN/ULC-S114 ASTM E 84 (UL 723) CAN/ULC-S102	Behaviour of Materials at 750°C (1382°F) Test for Non-Combustibility Surface Burning Characteristics Surface Burning Characteristics	Non-Combustible Non-Combustible Flame Spread = 0 Smoke Developed = 0 Flame Spread = 0
Moisture Resistance: ASTM C 1104	Moisture Sorption	Smoke Developed = 0 0.05 %
Water Vapour Permea	ance: Water Vapour Transmission, Desiccant Method	1768 ng/Pa.s.m² (31 perm)
Fungi Resistance: ASTM C 1338	Determination of Fungi Resistance	Passed
Thermal Resistance: ASTM C 518 (C 177)	R-value/inch @ 75°F RSI value/25.4 mm @ 24°C	4.0 hr.ft².F/Btu 0.70 m²K/W
Corrosive Resistance ASTM C 665 ASTM C 795 ****	Corrosiveness to Steel Stainless Steel Stress Corrosion Specification as per Test Methods C871 and C692: U.S. Nuclear Regulatory Commission, Reg. Guide #1.36: U.S. Military Specifications MIL-I-24244 (all versions including B and C)	Non-corrosive Non-corrosive

Acoustical Performance:

ASTM C 423 CO-EFFICIENTS AT FREQUENCIES							
Thickness	125 Hz	250 Hz	500 Hz	1000 Hz	2000 Hz	4000 Hz	NRC
1.5"	0.21	0.64	0.92	1.00	0.95	1.01	0.90
2.0"	0.43	0.78	0.90	0.97	0.97	1.00	0.90
3.0"	0.75	0.82	0.89	0.94	1.00	1.00	0.90

*MASTER FORMAT 1995 EDITION **MASTER FORMAT 2004 EDITION





Compressive Strength:

ASTM C 165	at 10 %	745 psf (35.5 kPa)
	at 25 %	1270 psf (61 kPa)

8.0 lb/ft³

Density:

ASTM C 612-00 - Actual

128 kg/m³

Dimensions:

24" (width) x 48" (length) 610 mm x 1219 mm

36" (width) x 48" (length) 610 mm x 1219 mm

48" (width) x 96" (length) 1219 mm x 2438 mm

Thickness:

Product is available in 1.25" 1.5" 2" 3" For additional sizes, please contact our customer service representatives.

Key Application Qualifiers:

- Good compressive strength
- Low moisture sorption
- Durability
- Fire resistance
- Excellent thermal resistance
- Non-corrosive
- Chemically inert
- CFC and HCFC free product and process
- Made from natural & recycled materials

Other ROXUL Products:

Please consult ROXUL for all your insulation needs. We have an extensive range of products for all applications from pipe insulation to commercial products to residential batts. ROXUL invites all inquiries and will act promptly to service all of your requirements.

Note:

As ROXUL Inc. has no control over installation design and workmanship, accessory materials or application conditions, ROXUL Inc. does not warranty the performance or results of any installation containing ROXUL Inc's. products. ROXUL Inc's. overall liability and the remedies available are limited by the general terms and conditions of sale. This warranty is in lieu of all other warranties and conditions expressed or implied, including the warranties of merchantability and fitness for a particular purpose.

ROXUL INC. www.roxul.com Milton, Ontario Tel: 905-878-8474 Tel: 1-800-265-6878 Fax: 905-878-8077 Fax: 1-800-991-0110 Revised: October 27, 2014 Replaces: July 04, 2013

City of Seattle Department of Planning and Development www.seattle.gov/dpd 700 Fifth Avc, Suite 2000, P.O. Box 34019, Seattle Code Modification	e, WA 98124-4019
Date Requested: December 20, 2011	Project Information:
Contact Information:	A/P Number: <u>6256329</u> Address: 2401 NE BLAKELEY ST Seattle, WA
Name: Arriv Hartwell	Code Edition: 2006 Seattle Building Code
Mailing Address: 1301 Fitst Avenue Sulte 301	
Seattle, WA 98101	Structure Information:
	Project Description:
Phone Number: 206.902.5524	Exterior cladding & window replacement.
Fax Number: 206.467.0627	
E-mail Address: ahartwell@gglo.com	Occupancy Group(s)/ Character;
Relationship to Project:	R-1 / A-3 (based on original UBC permit) Type of Constructi o n: <u>Type V, 1-hour</u>
O Owner	Number of Stories: _ 4
O Design Professional	Basements/ Mezzanines: 0
O Contractor	Sprinkler Location: None

Code Modification Request:

Ref. SBC 104.9. A code modification is a walver of a code requirement, and is intended to provide flexibility to the building official where there are practical difficulties meeting specific code requirements so long as the intent of the code is accomplished.

The requestor is expected to demonstrate:

- 1. There are practical difficulties involved in strictly conforming to the provisions of the code; and
- 2. The modification conforms with the intent and purpose of the code; and
- 3. Together with other safety features of the building or other relevant circumstances, the modification will provide a reasonable level of strength, effectiveness, fire resistance, durability, safety, accessibility and sanitation.

When engaged for the project, the registered design professional in responsible charge shall submit the request for a code modification under their seal and signature, including a statement that in their professional opinion, the proposal is in conformance with the intent and purpose of the code and the modification will provide a reasonable level of strength, effectiveness, fire resistance, durability, safety, accessibility and sanitation.

Please attach plans showing your proposal.

Code Alternate Request:

Ref. SBC 104.10. A code alternate is intended to provide for introduction of alternate materials, systems and methods for which the code did not anticipate, provisional upon the alternate complying with the code and providing an equivalent solution. Essentially, a code alternate is intended to meet a performance standard rather than a prescriptive standard.

The requestor is expected to demonstrate that the alternate does not conflict with the code and together with other safety features of the building or other relevant circumstances, will provide an equivalent level of strength, effectiveness, fire resistance, durability, safety, accessibility and sanitation.



Construction Review & Inspection Quality Jourthan Sin, Principal Engineer

9604986902 ,ON XA1

DEC-29-2011 THU 08:49 AM Sealtle DPD

P, 02

When engaged for the project, the registered design professional in responsible charge shall submit the request for a code alternate under their seal and signature, including a statement that in their professional and signature, including a statement that in their professional and signature is equivalent to the code provisions.

Please attach plans showing your proposal.

Washington State Seal and Signature 7229	
REGISTERED	
AFF AD	
JAMES BRADLET STATE OF WASHINGTON	

7	DPD Use OFAEC 29 2011
OApproved	APPROVED Subject to Errors And Omissions
O Approved with Amendment O Denied	BYKaveh Aminian
Reasons: <u>PER PROFOSIONAN OF RE</u>	
SEC. 721, pot SBC 200	6 FIRE RESISTIVE EQUEVALONICY
	E OF THE MOTERIAL FOR

AND

Description of Alternate/ Modification (include reason for request):

In order to acheive a 1-hour fire rating from both interior and exterior sides, a new exterior wall assembly is proposed for this renovation project. Please refer to the attached Letter of Explanation for a description of materials proposed.

Description of Code Requirement (include section):

Please refer to the attached Letter of Explanation.

Justification (attach copies of any reference, test reports, expert opinions, etc.): Please refer to attached product cutsheets for Roxul ComfortBoard showing fire-resistive properties.



63

Construction Review & Inspection Quality Jonathan Siu, Principal Engineer

FAX NO, 2063864039

DEC-29-2011 THU 08:49 AM Seattle DPD

December 20, 2011

Mr. Kaveh Aminian City of Seattle Department of Planning & Development 700 Fifth Avenue, Suite 2000 Seattle, WA 98124-4019

Re: Code Modification Request, 1-Hour Wall Assembly Blakeley Manor Rehabilitation, DPD Project No. 6256329 2401 NE Blakeley Street, Seattle, WA 98105

Dear Mr. Aminian,

Please find the following information pertaining to this Code Modification Request:

Pertaining to the Description of Alternate/Modification

Blakeley Manor is an existing four-story stucco-sided apartment building operated by the Seattle Housing Authority which will soon undergo renovation. The scope of work includes removal of the existing stucco and lath finish and replacement with 15/32" exterior plywood for shear, a liquid applied weather and air resistive barrier system, an exterior layer of mineral wool for added thermal insulation, and a rainscreen siding system using cementitious lap or panel siding over 2x4 PT furring strips. The existing wood stud framing, batt insulation, and interior GWB remain in place unless damaged.

The replacement wall assembly was reviewed by the DPD as part of our permit set and is the same assembly used on several other permitted SHA renovation projects: 6255337, 6256140, and 6251153. These projects' permits were issued under the 2006 SBC. During a courtesy field inspection at Nelson Manor (6255337), Warren Parker labeled the assembly as "failed" because it was not rated from both interior and exterior sides as required per 704.9, 2006 SBC - ie, it did not have an exterior layer of GWB.

Initially we were hoping to prove this assembly's fire resistivity from the exterior face by calculating its fire resistance per Section 720 and sub sections of the 2006 SBC for a "Prescriptive Fire Resistance" approach. According to Section 721.6 Wood Assemblies and Tables 721.6.2(1), 721.6.2(2) and 721.6.2(5) our proposed assembly would be allowed the following cumulative fire resistance ratings for the individual components:

1) As calculated from inside out:

Existing 5/8" interior Type X GWB	40 minutes	Table 721.6.2(1)
Existing 2x6 wood stud framing @ 16"	20 minutes	Table 721.6.2(2)
o.c.		
Glass fiber batt insulation	15 minutes	See Section 721.6.2.5 & Table 721.6.2(5) – Not needed for FR rating
15/32" exterior plywood	10 minutes	Table 721.6.2(1)
TOTAL	85 minutes	Meets reqs of 1-hr wall from interior

2) As calculated from outside in:

Fiber Cement Siding	0 minutes	According to James Hardie representative
1 ¼" Thick Mineral Wool (density = 4.4 pcf)	15 minutes	Table 721.6.2(5)
15/32" exterior plywood	10 minutes	Table 721.6.2(1)
Glass fiber batt insulation	15 minutes	See Section 721.6.2.5 & Table 721.6.2(5). May be needed for FR rating.
Existing 2x6 wood stud framing @ 16" o.c.	20 minutes	Table 721.6.2(2)
TOTAL	60 minutes	Meets reqs. of 1-hr wall from exterior

However, you had expressed concerns about this assembly since the proposed layer of mineral wool was discontinuous between the furring strips. Therefore, we have revised the wall assembly detail to show a continuous 1 ¼" thick higher density mineral wool layer, Roxul's ComfortBoard IS, installed over the sheathing. The new proposed mineral wool will increase density and weight from 4.4 PCF to 8.0 PCF. The furring strips will be installed through the mineral wool to the existing studs. The continuous mineral wool will provide enhanced fire resistance and the increased density will improve thermal performance while eliminating thermal bridging. We believe this assembly meets the intent of Section 721, Calculated Fire Resistance, by providing a 1-hour rated wall as tested from the exterior face.

Code Modification Request Blakeley Manor Rehabilitation, 6256329 December 20, 2011 Page **3** of **3**

Enclosed with this document is a cut-sheet of Roxul's ComfortBoard IS product, the mineral wool we prefer to use. Also please find a detail of the revised, proposed wall assembly.

It is my professional opinion that the proposed wall assembly code modification for Blakeley Manor meets the intent of the 2006 Seattle Building Code. This opinion is true and sound to my best information, knowledge, and belief.

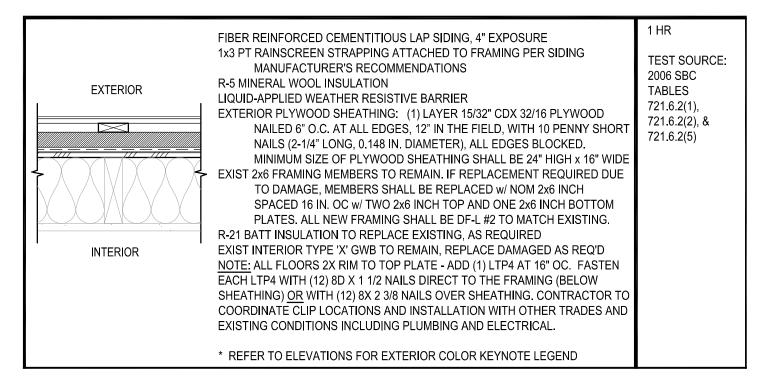
Sincerely,

GGLO, LLC

James Bradley, AIA Principal

Att: Exhibit A – Revised Wall Assembly Exhibit B – Roxul ComfortBoard IS Technical Data Exhibit C – Roxul Deflection Test Report

EXHIBIT A: REVISED WALL ASSEMBLY





General Product Information:

Compliance and Performance:

ROXUL® products are mineral wool fibre insulations made from basalt rock and slag. This combination results in a noncombustible product with a melting point of approximately 2150°F (1177°C), which gives it excellent fire resistance properties. ROXUL mineral wool is a water repellent yet vapour permeable material.

Technical Product Information



BOARD INSULATION 07210* BOARD INSULATION 07 21 13**

Description & Common Applications:

The ComfortBoard[™] IS product is a rigid mineral wool insulation sheathing board that is non-combustible, water repellent, fire resistant and sound absorbent. This product is exterior non-structural insulation sheathing for high performance residential wall systems.

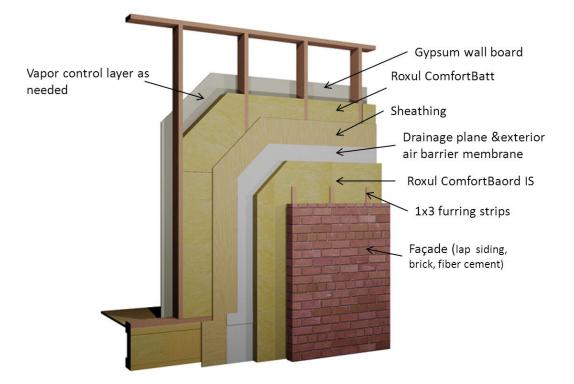
Compliance and Perf	ormance:	
ASTM C 612 CAN/ULC –S702	Mineral Fiber Block and Board Thermal Insulation Mineral Fibre Thermal Insulation for Buildings	Type IVB, Complies Type 1, Complies
Fire Performance:		
ASTM E 136	Behaviour of Materials at 750°C (1382°F)	Non-Combustible
CAN/ULC S114	Test for Non-Combustibility	Non-Combustible
ASTM E 84(UL 723)	Surface Burning Characteristics	Flame Spread = 5
		Smoke Developed = 10
CAN/ULC S102	Surface Burning Characteristics	Flame Spread = 5
		Smoke Developed = 10
Moisture Resistance:		
ASTM C 1104	Moisture Sorption	0.05%
Water Vapour Permea	ance:	
ASTM E 96	Water Vapour Transmission, Desiccant Method	1768 ng/Pa.s.m2(30.9 perm)
		5
Fungi Resistance		
ASTM C1338	Determination of Fungi Resistance	Passed
ASTM C1350	Determination on ungritesistance	1 23360
Thermal Resistance:		
	R-value/inch @ 75°F	4.0 hr.ft².F/Btu***
ASTM C 518 (C 177)	RSI value/25.4 mm @ 24°C	4.0 m.i.e.r/Biu 0.72 m²K/W
		0:72111-10/00
Corrosive Resistance	:	
ASTM C 665	Corrosiveness to Steel	Pass
ASTM C 795 ****	Stainless Steel Stress Corrosion Specification as per Test	Conforms
	Methods C871 and C692: U.S. Nuclear Regulatory Commission,	
	Reg. Guide #1.36: U.S. Military Specifications MIL-I-24244 (all	
	versions including B and C)	

Acoustical Performance

ASTM C423 CO-EFFICIENTS AT FREQUENCIES							
Thickness	125 Hz	250 Hz	500 Hz	1000 Hz	2000 Hz	4000 Hz	NRC
1.5"	0.21	0.64	0.92	1.00	0.95	1.01	0.90
2.0"	0.43	0.78	0.90	0.97	0.97	1.00	0.90
3.0"	0.75	0.82	0.89	0.94	1.00	1.00	0.90

*MASTER FORMAT 1995 EDITION **MASTER FORMAT 2004 EDITION *** at the time of manufacturing





Compressive Strength:

ASTM C 165	at 10%	743 psf (35.6 kPa)
	at 25%	1269 psf (60.8 kPa)

8.0 lbs/ft³

Density:

ASTM C 612-00 - Actual

128 kg/m³

Dimensions:

24" (width) x 48" (length) 610 mm x 1219 mm

36" (width) x 48" (length) 610 mm x 1219 mm

48" (width) x 96" (length) 1219 mm x 2438 mm

Thickness:

Product is available in 1.25" 1.5" 2" 3" For additional sizes, please contact our customer service representatives.

Key Application Qualifiers:

- · Good compressive strength
- Low moisture sorption
- Durability
- Fire resistance
- Excellent thermal resistance
- Non-corrosive
- Chemicallyinert
- CFC and HCFC free product and process
- Made from natural & recycled materials

Other ROXUL Products:

Please consult ROXUL for all your insulation needs. We have an extensive range of products for all applications from pipe insulation to commercial products to residential batts. ROXUL invites all inquiries and will act promptly to service all of your requirements.

Note:

As ROXUL Inc. has no control over installation design and w orkmanship, accessory materials or application conditions, ROXUL Inc. does not w arranty the performance or results of any installation containing ROXUL Inc's. products. ROXUL Inc's. overall liability and the remedies available are limited by the general terms and conditions of sale. This w arranty is in lieu of all other w arranties and conditions expressed or implied, including the w arranties of merchantability and fitness for a particular purpose.

ROXUL INC. www.roxul.com Milton, Ontario Tel: 905-878-8474 Tel: 1-800-265-6878 Fax: 905-878-8077 Fax: 1-800-991-0110 Revised: Nov 1, 2011



March 3, 2011

Mark Bromiley Roxul Inc. 420 Bronte St. S. Suite 105 Milton, Ontario, L9T 0H9

Via email: mark.bromiley@roxul.com

Re: Roxul – Exterior Insulation Deflection Testing

Background

As society demands more energy efficient buildings, codes and builders are responding by increasing the R-value of the building enclosure, in particular the above-grade wall. Given than the cavity of the standard 2x6 wood frame wall used in low-rise housing is already filled with insulation, the clear path forward to higher R-values is to add layers of exterior insulation. Although other solutions are possible, exterior insulation layers have the benefits that:

- 1. At thicknesses of up to 1.5", exterior insulation has long been used by the industry, and hence there is experience with it installation and detailing,
- 2. Thermal bridging through framing members, floor joists, lintels, etc. is very significantly reduced, increasing the wall R-value significantly,
- 3. The risk of cold-weather condensation within the moisture-vulnerable wood framing is significantly reduced, and potentially eliminated,
- 4. A range of target R-values can be easily reached as similar details can be used for the design of walls that have 2, 3, 4 or even 6" of insulation,
- 5. The marginal cost of increasing framing thickness and/or building double-walls usually outweighs the marginal cost of adding insulating sheathing layers.

Highly-permeable insulation like Roxul has the added benefit that it allows very fast outward drying during cold weather: this dries the wood-frame cavity very quickly, even if the framing is wet from construction or becomes wet because of incidental water leaks.

A major impediment to the wide-spread adoption of exterior sheathing behind direct applied claddings such as vinyl, wood, fibre cement, stucco and adhered veneer, is the lack of information about the structural performance of claddings installed over insulating sheathing. Foam plastic insulations, which have much higher compressive strengths (often 15 to 25 psi @10% deformation) than most Roxul products (often 1 to 5 psi) are seen as better products for this application. The concern is that the insulation is not or stiff strong enough to suspend claddings and deformations may occur causing cracking, and other issues. Very little testing has been conducted to show the strength and stiffness of insulation supporting cladding and no testing results of Roxul insulation is available.

The most common method of attaching cladding over thick insulation is to use wood furring (strapping) attached with screws through the insulation to the framing as shown in Figure 1.

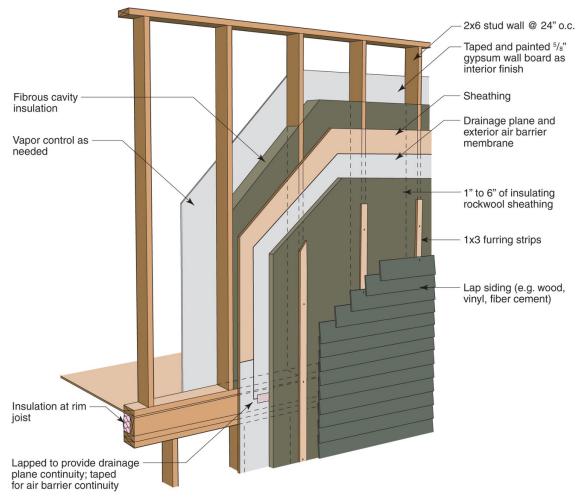


Figure 1: Typical application of semi-rigid Roxul insulation over wood framing

Objective

The objective of this study is to quantify the relationship between cladding gravity loads and deflection under cladding weights of up to 30 pound per square foot. These results are intended to be used to provide guidance to designers, builders, and code officials involved in projects using Roxul brand semi-rigid rockwool sheathing.

Scope

This report summarizes the results of load deflection testing deflection of strapping over six types of Roxul exterior insulation as shown in Table 1. These walls were tested on 24" oc framing, with strapping attachment screws at vertical spacings of 16" oc. Other variables such as 16" oc framing, different screw sizes and spacings were outside the

scope of the testing program. This study was designed to simulate walls providing the least support practically likely (thin screws wide spacing of studs and fasteners) and hence the highest likely deflections. If improved construction standards are used, such as stronger screws and/or more frequent screw spacing, the amount of deflection would decrease. This is meant to be a type of worst case, yet realistic, scenario.

Insulation Product	Approximate Density (lb/ft ³)
1.25" Cavity Rock MonoDensity	4.1
3" Cavity Rock DualDensity	3.4 / 6.2
1.25" RB60	6.0
1.25" RB80	8.0
3" RB80	8.0
1.25" Drainboard	8.0
1" Type IV extruded polystyrene	2.0

Table 1: Roxul insulation types to be tested

Testing Apparatus

To conduct the testing, a 2x wall frame with 24" stud spacing was securely fastened to a concrete block wall in the laboratory. OSB sheathing and a house wrap were installed over the sheathing. The different types of Roxul insulation were installed over the house wrap, and held in place by screws driven through nominal 1x3 strapping (actual dimension ³/₄"x 2.5") connected directly to the wood framing (Figure 2). The strapping was attached with screws spaced vertically at 16" oc. Given the 24" spacing of the framing, this is 2.67 square feet per fastener (or about 4 connectors per square meter).

Figure 3 presents photographs of the screws used for strapping attachment for both 1.25" thick insulation and 3" thick insulation. To attach strapping over 1.25" thick insulation, 3" deck screws were used. For the first tests the strapping over 3" thick insulation was attached using $\#9 \times 5$ " trim head bronze wood screws were used (middle screw in Figure 3). After inspection of the screws following the first test, this screw showed considerable permanent deflection, and the smaller diameter heads pulled deep into the wood of the furring strip. Hence, subsequent test of 3" thick insulation used $\#10 \times 5$ " wood screws with standard head sizes. These screws showed a marked improvement in performance.

Roxul – Exterior Insulation Deflection Testing – February 2011



Figure 2 : Roxul insulation attached to wall frame ready for test



Figure 3 : Strapping attachment screws

A 2 tonne-capacity hydraulic ram was used to apply force to a metal angle in contact with the bottom edge of both strapping pieces (Figure 4). To measure the applied force a 1000 lbf (4500 N) strain gauge load cell (with ± 0.4 lbf rated accuracy) was placed between the angle and the ram.

Deflection gauges (with a resolution of 1/1000" or 0.025 mm) were used to measure the movement of the wall sheathing and the strapping on both the left and right side. Metal

clips were attached to the strapping to allow deflection gauges to measure the strapping movement.

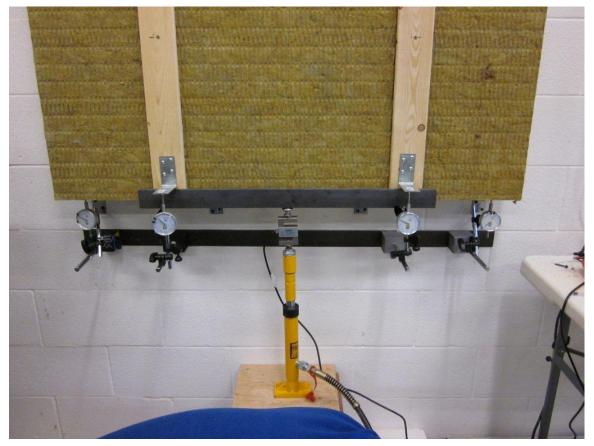


Figure 4: Hydraulic Ram with load cell and deflection gauges measuring strapping movement (sheathing deflection gauges not shown)

Loads were applied in increments of 100 lbs between 100 lbs and 1,000 lbs. The four deflection readings were recorded at each increment. Each load increment was applied over about 30 to 60 seconds and the readings taken with 30 seconds. All of the tests were conducted three times on the same test specimen. The wall was loaded to 1000 lbs, unloaded, and reloaded two more times.

Results and Analysis

The average deflection was calculated by determining the average of the deflection of the right and left strapping pieces and subtracting any movement measured in the wall frame. In general, the framing moved very little (about 10% of the total deflection).

For all of the specimens, the first time the wall was loaded the deflection was significantly larger and than the last two tests. The second pair of tests showed good repeatability. It is assumed that this behavior is due to the wall assembly "seating" itself or "settling in". The amount of seating could be increased by attaching the initial torque during installation of the screws: controlling the amount of screw torque was a challenge as it was not always easy to achieve perfectly plumb strapping.

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The results of load and deflection can be compared to spatial mass density of typical claddings shown in Table 2. These weights are meant to be representative of all similar claddings although some cladding types might be outside of the range listed. The testing was conducted to approximately twice the weight of the heaviest cladding in the table, adhered stone veneer (i.e., 15 psf x 4 x 8 x 2 = 960 pds). These ranges of cladding weights are shown in the analysis graph as shaded areas in Figure 5.

Cladding Type	Typical mass density range (psf)	Equivalent weight for 4'x8' test panel (lbs)
Vinyl siding	0.6-1.0	20-32
Wood siding	1.0-1.5	32-48
Fiber cement siding	3-5	96-160
Cement stucco	10-12	320-384
Adhered stone veneer	12-15	384-480

Table 2 : Approximate cladding weights

Figure 5 plots the load-deflection curves for 3" CavityRock. As this graph is representative of all of the insulations tested, the remaining load-deflection graphs are attached in the appendix, and the results are summarized in Table 3. As can be seen, the load-deflection curve has a degree of curvature to it, but it largely linear for the first 100-200 pounds (eg. the load imposed by lap siding).

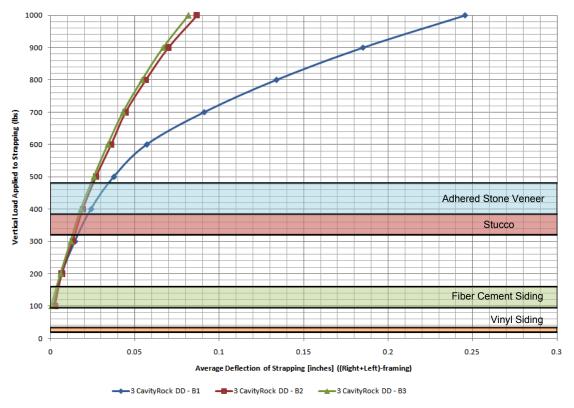


Figure 5: Deflection Testing of 3" CavityRock

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Table 3 shows the deflection results for all three 1000lb loadings on each test system in the order of least average deflection to greatest average deflection. The average deflection was calculated from all three loadings and used to determine the performance order. If the average was taken of the second and third repeatable deflection on each wall, the relative ranking of performance would not change.

Insulation	Density [lb/ft ³]	Compressive Strength (@25%) [kPa]	1 st Loading [inches]	2 nd Loading [inches]	3 rd Loading [inches]	Average [inches]
1" XPS	-	-	0.068	0.0355	0.0345	0.0460
1 ¼" RB80	8	60.8	0.089	0.034	0.030	0.0506
3" RB80	8	60.8	0.094	0.038	0.027	0.0529
3" RB60	6	28.1	0.117	0.044	0.041	0.0672
1 ¼" CavityRock MD	4.1	-	0.134	0.076	0.069	0.0927
3" CavityRock MD	6.2 / 3.4	-	0.246	0.087	0.082	0.1379
1 ¼" CavityRock with no OSB sheathing	4.1	-	0.166	0.136	0.1335	0.1452
1 ¼" DrainBoard	8	35	0.265	0.090	0.092	0.1486

Table 3 :	Summary	of Deflection	Results at 1000	bs
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Table 4 summarizes the measured data into what is a more useful format. For each of the product types the initial deflection measured is used to predict the deflection in service for three typical cladding types. Given that measurements of less than 0.010" are difficult to measure repeatedly or reliably, and that such a deflection is negligible in service, any deflections of less than 0.01" (0.25 mm) have been simply entered as "<0.01" in the table.

Insulation & Thickness	Vinyl Siding (1 psf)	Fiber Cement Siding (4 psf)	Stucco 3/4" (12 psf)
1.25" Cavity Rock MonoDensity	<0.01	0.012	0.050
3" Cavity Rock DualDensity	<0.01	<0.01	0.020
3" RB60	< 0.01	< 0.01	0.014
1.25" RB80	< 0.01	< 0.01	0.010
3" RB80	< 0.01	<0.01	< 0.01
1.25" Drainboard	< 0.01	<0.01	0.045
1" Type IV extruded polystyrene, no OSB	<0.01	<0.01	0.120
1.25" Cavity Rock MonoDensity, no OSB	<0.01	0.015	0.060

Table 4: Estimated Deflection (inches) in Service for Typical Cladding Loads

Note: Assumes studs at 24" o.c. or closer, and minimum #10 fasteners at maximum 16" vertical spacing through nominal 1x3 furring strips. Deflection is based on the initial loading, and assumes that no creep occurs over long-term. Wind suction pressure may control the design of the fastening in high wind areas, not vertical deflection.

Summary and Conclusions

- All of the insulations tested showed very little deflection (less than 0.01" or 0.25 mm) at the loads imposed by lap siding (of wood, vinyl, or fiber cement)
- The least amount of deflection was experienced by RB80, with a density of 8lb/ft³ and the highest rated compressive strength of the Roxul insulations tested.
- The 1" Type 4 extruded polystyrene was no stiffer than the RB80
- If the strapping and insulation are not attached tightly to the wall sheathing, the initial deflection can be expected to be larger than if the insulation is firmly clamped, and the cladding attached with nail guns or other techniques that caused settling.
- All six materials tested resulted in very similar patterns of deflection. The first loading produced the largest amount of deflection for each wall, and the second and third tests were very similar and repeatable with much less deflection, approximately half as much as the initial loading.

Note that these tests were conducted to simulate some of the worst-case realistic scenarios for deflection (i.e., 24" o.c. strapping, and 16" vertical spacing between screws). This is equivalent to only 4 fasteners per square meter. Also, the screws used were the lowest quality, length and thickness that would be reasonable for this

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application. Using more screws, more often would likely decrease deflection, but more testing is required to determine the amount that the deflection could be decreased.

Recommendations

It is recommended that field trials be conducted to gain feedback from installers in the field. It was noted that some care was required when installing the screws to attach the fastening so as to ensure a plumb strapping: excess or insufficient screw torque could cause the strap to be bent.

In practice, recommending screw attachments at 12" o.c for 24" o.c framing and 16" for 16" o.c framing would provide some additional safety factors.

Despite the very favourable results achieved, it is recommended that field testing, in a test facility or on a jobsite, should be conducted to assess the potential for stucco or adhered veneer cracking over a 1-2 year test period before proceeding with wider deployment.

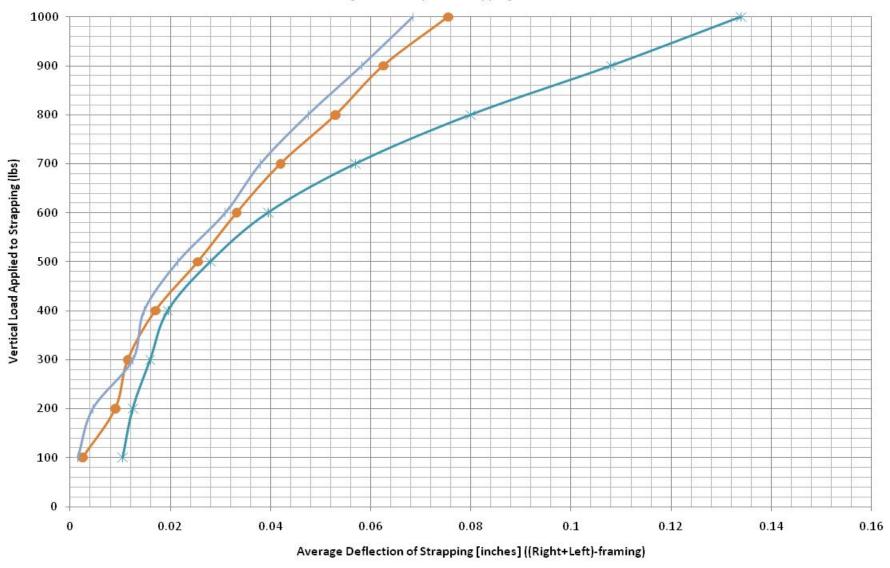
If you have any questions or comments about any part of this report, please do not hesitate to call or email.

Sincerely

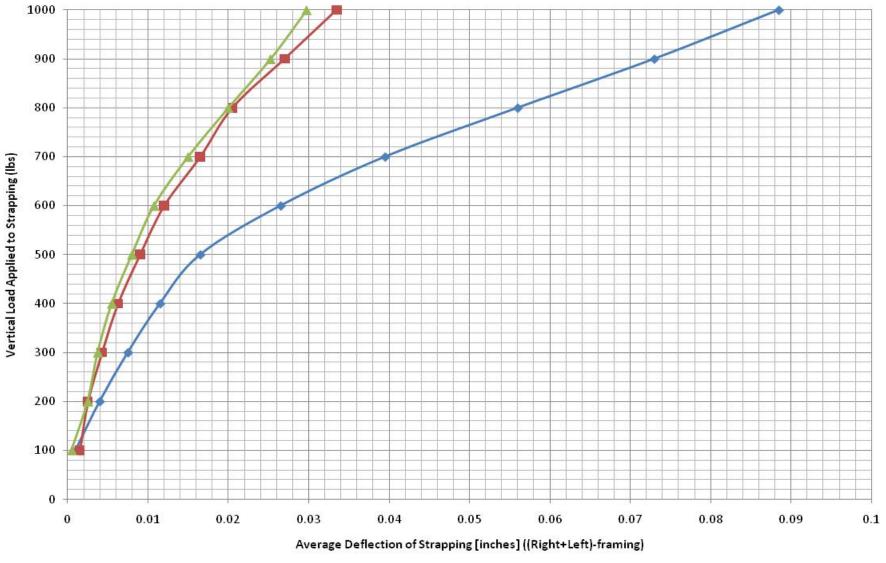
Jonathan Smegal, MASc. Associate EIT

John Strant

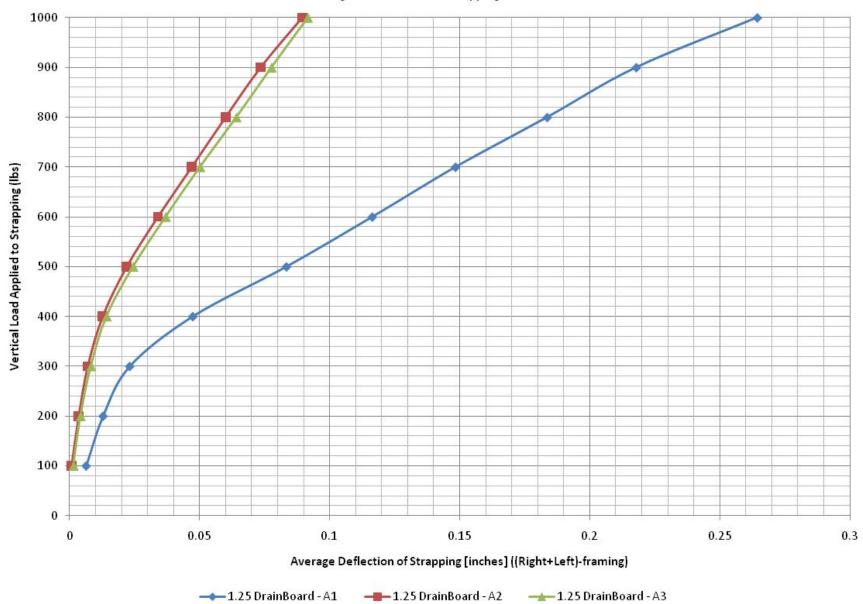
John Straube, Ph.D. P.Eng. Principal



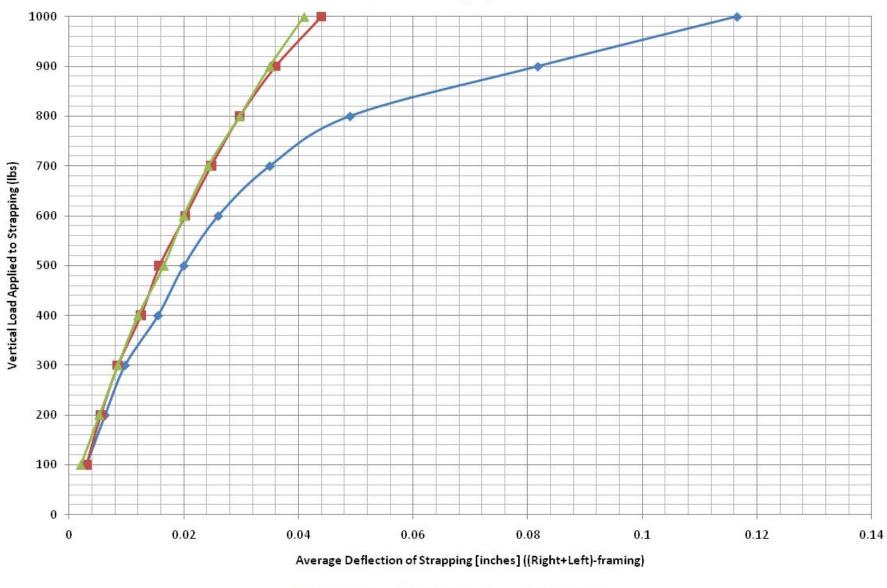
Deflection Testing - 1.25 CavityRock, strapping 24" oc, screws 16" oc



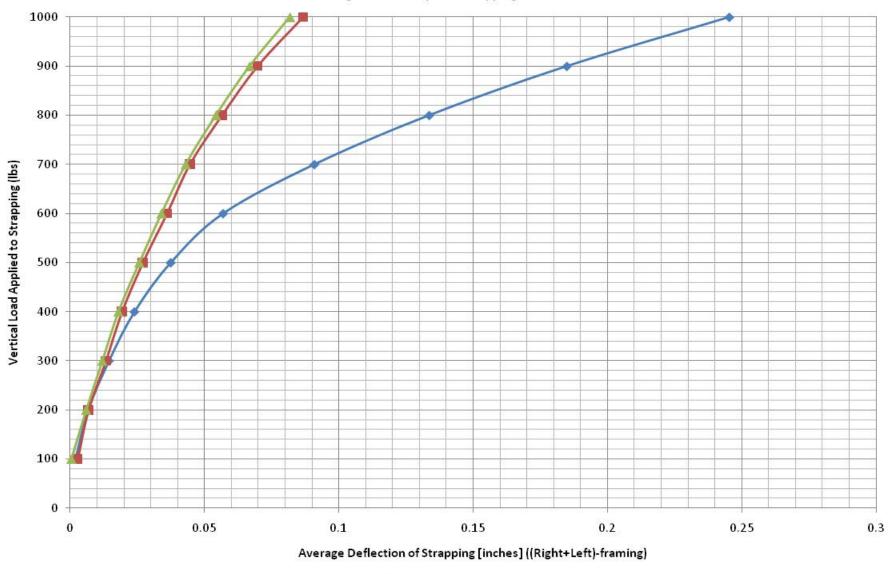
Deflection Testing - 1.25 RB80, strapping 24"oc, screws 16" oc



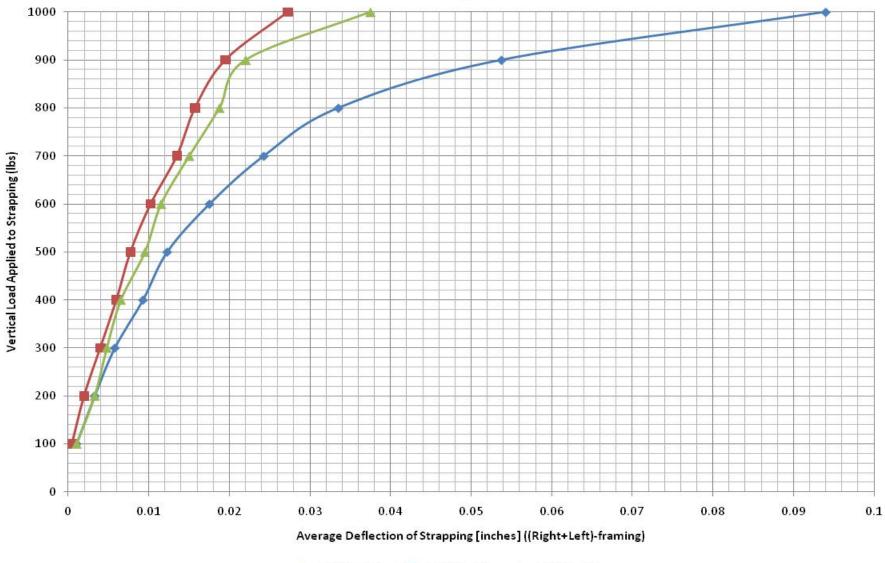
Deflection Testing - 1.25 DrainBoard, strapping 24" oc, screws 16" oc



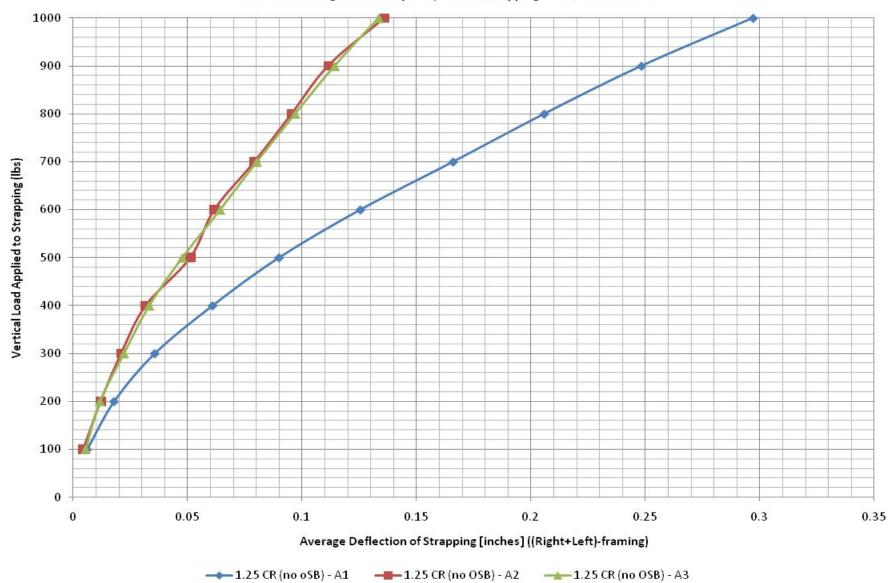
Deflection Testing - 3" RB<u>6</u>0, strapping 24"oc, screws 16" oc



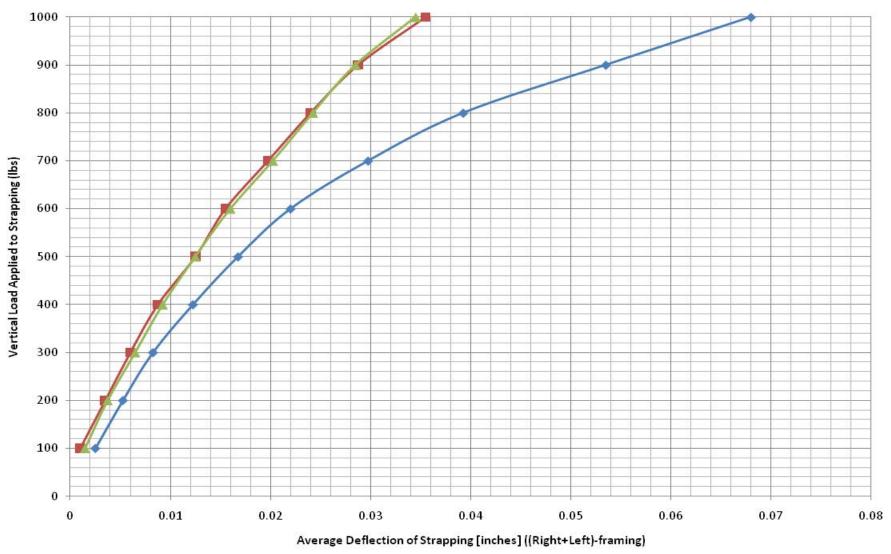
Deflection Testing - 3" DD CavityRock, strapping 24" oc, screws 16" oc



Deflection Testing - 3" RB<u>8</u>0, strapping 24"oc, screws 16" oc



Deflection Testing - 1.25 CavityRock, no OSB, strapping 24" oc, screws 16" oc



Deflection Testing - XPS exterior insulation, no OSB, strapping 24" oc, screws 16" oc

→ 1" XPS 1A → 1" XPS 2A → 1" XPS 3A