

Structural Calculations

for

Ankeny Woods Lower Floor Roof Canopy
11930 SE Ankeny St. Portland, Oregon 97216

Prepared for
KASA Architects, inc.

January 24, 2022

JOB NUMBER: KAS-10

Limitations

Engineer was retained in limited capacity for this project. Design is based upon information provided by the client, who is solely responsible for the accuracy of same. No responsibility and/or liability is assumed by, or is to be assigned to the engineer for items beyond that shown on these sheets.

9 sheets total including this cover sheet.



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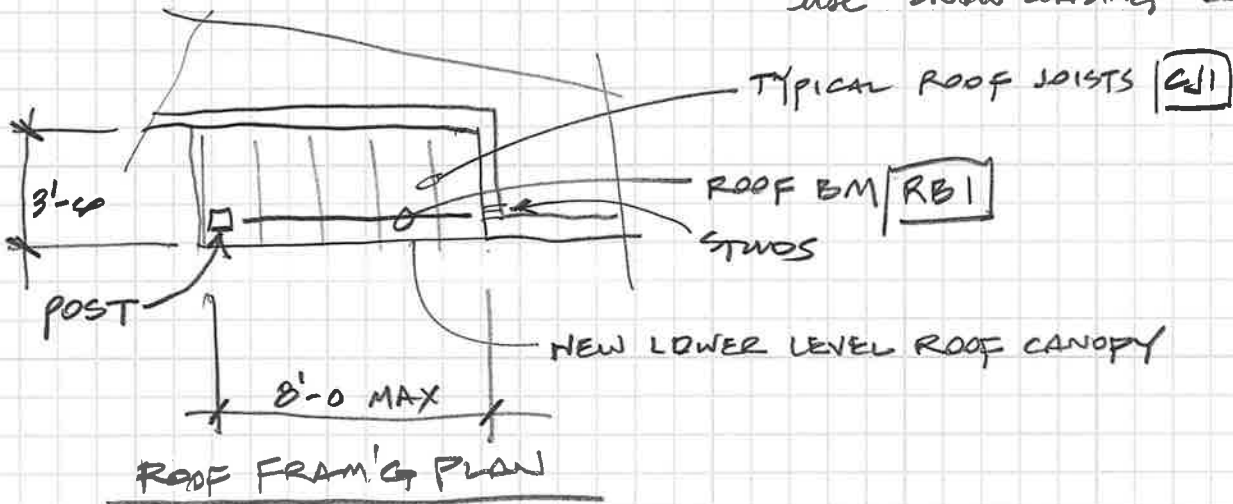


PROJECT: ANKENY WOODS APTS

RE: NEW FIRST FLR ROOF CANOPIES

CANOPY DL = 12 PSF

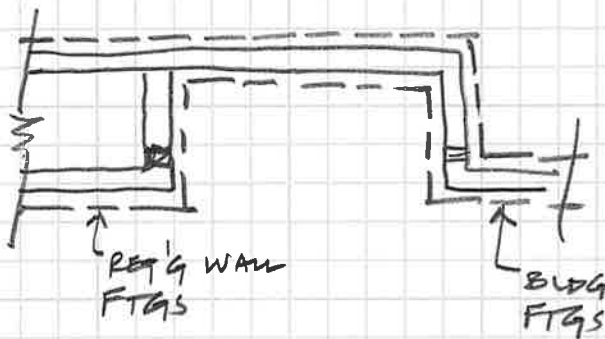
max SNOW LOADING = 60 PSF



NOTE: EXIST'G 2ND FLOOR DECK TO BE REMOVED & REPLACED WITH THIS NEW ROOF CANOPY.

THEREFORE NO CONCERNS ON EITHER GRAVITY OR LATERAL LOADS.

(SEE PAGES FOLLOW FOR FRAM'G DESIGN) →





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Typical Roof Joists CJ1

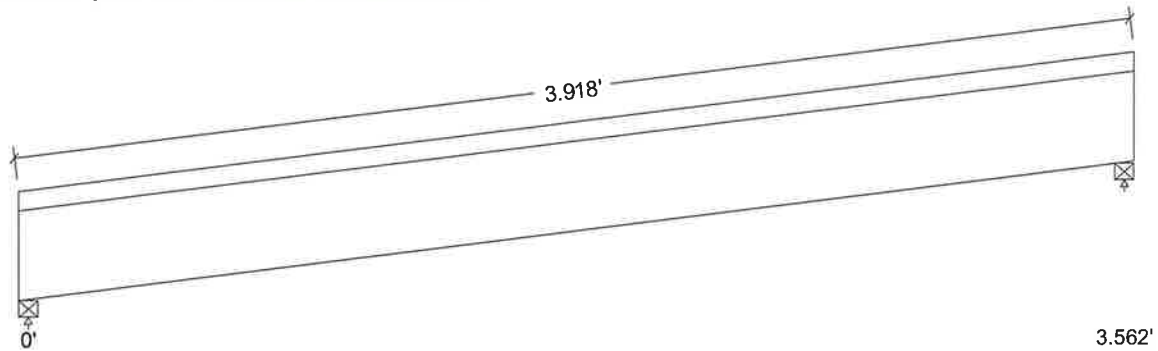
Design Check Calculation Sheet

WoodWorks Sizer 11.1

Loads:

Load	Type	Distribution	Pat- tern	Location [ft] Start End	Magnitude Start End	Unit
Load1	Dead	Full Area			12.00 (24.0")	psf
Load2	Snow	Full Area			60.00 (24.0")	psf
Self-weight	Dead	Full UDL			1.1	plf

Maximum Reactions (lbs) and Bearing Lengths (in) :



Unfactored:			
Dead	48		48
Snow	217		217
Factored:			
Total	265		265
Bearing:			
Length	0.75		0.75
Min req'd	0.75		0.75

;Canopy Roof Joists CJ1

Lumber-soft, Hem-Fir, No.2, 2x4 (1-1/2"x3-1/2")

Supports: All - Timber-soft Beam, D.Fir-L No.2

Roof joist spaced at 24.0" c/c; Total length: 3.92'; Clear span: 3.689'; volume = 0.1 cu.ft.; Pitch: 4/12

Service: wet; Lateral support: top= full, bottom= at supports;

Analysis vs. Allowable Stress and Deflection using NDS 2015 :

Criterion	Analysis Value	Design Value	Unit	Analysis/Design
Shear	$f_v = 59$	$F_v' = 134$	psi	$f_v/F_v' = 0.44$
Bending(+)	$f_b = 910$	$F_b' = 997$	psi	$f_b/F_b' = 0.91$
Live Defl'n	$0.08 = L/555$	$0.19 = L/240$	in	0.43
Total Defl'n	$0.12 = L/385$	$0.25 = L/180$	in	0.47

Design Notes:

1. WoodWorks analysis and design are in accordance with the ICC International Building Code (IBC 2015), the National Design Specification (NDS 2015), and NDS Design Supplement.
2. Please verify that the default deflection limits are appropriate for your application.
3. Sawn lumber bending members shall be laterally supported according to the provisions of NDS Clause 4.4.1.
4. SLOPED BEAMS: level bearing is required for all sloped beams.



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Beam1

RB1

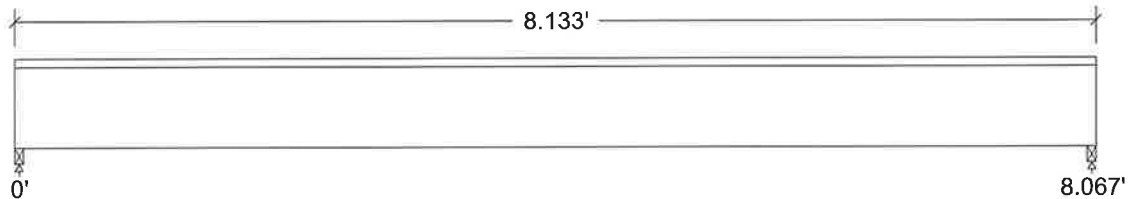
Design Check Calculation Sheet

WoodWorks Sizer 11.1

Loads:

Load	Type	Distribution	Pat-tern	Location [ft] Start End	Magnitude Start End	Unit
Load1	Dead	Full Area			12.00 (24.0")	psf
Load2	Snow	Full Area			60.00 (24.0")	psf
Self-weight	Dead	Full UDL			5.2	plf

Maximum Reactions (lbs) and Bearing Lengths (in) :



Unfactored:			
Dead	119		119
Snow	488		488
Factored:			
Total	607		607
Bearing:			
Length	0.80		0.80
Min req'd	0.80		0.80

;Canopy Beam RB1

Lumber-soft, Hem-Fir, No.2, 4x8 (3-1/2"x7-1/4")

Supports: All - Timber-soft Beam, D.Fir-L No.2

Roof joist spaced at 24.0" c/c; Total length: 8.13'; Clear span: 8.0'; volume = 1.4 cu.ft.

Service: wet; Lateral support: top= full, bottom= at supports;

Analysis vs. Allowable Stress and Deflection using NDS 2015 :

Criterion	Analysis Value	Design Value	Unit	Analysis/Design
Shear	$f_v = 30$	$F_v' = 134$	psi	$f_v/F_v' = 0.22$
Bending(+)	$f_b = 475$	$F_b' = 1017$	psi	$f_b/F_b' = 0.47$
Live Defl'n	$0.09 = < L/999$	$0.40 = L/240$	in	0.23
Total Defl'n	$0.14 = L/703$	$0.54 = L/180$	in	0.26

Design Notes:

1. WoodWorks analysis and design are in accordance with the ICC International Building Code (IBC 2015), the National Design Specification (NDS 2015), and NDS Design Supplement.
2. Please verify that the default deflection limits are appropriate for your application.
3. Sawn lumber bending members shall be laterally supported according to the provisions of NDS Clause 4.4.1.



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Canopy Post

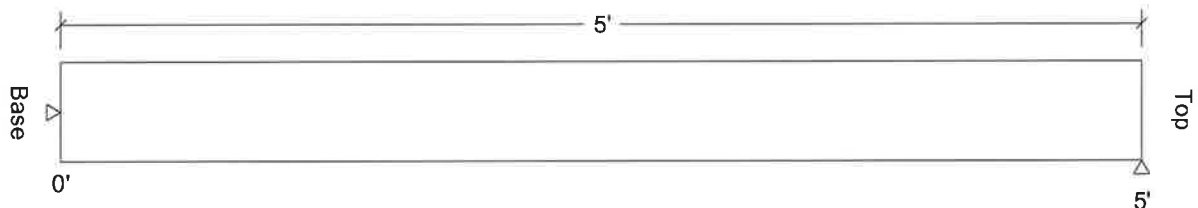
Design Check Calculation Sheet

WoodWorks Sizer 11.1

Loads:

Load	Type	Distribution	Location [ft] Start End	Magnitude Start End	Unit
Load1	Dead	Axial	(Ecc. = 0.92")	150	lbs
Load2	Snow	Axial	(Ecc. = 0.92")	500	lbs
Self-weight	Dead	Axial		31	lbs

Lateral Reactions (lbs):



Unfactored:			
Dead	2		-2
Snow	8		-8
Factored:			
R->L			-10
Load comb			#2
L->R	10		

Canopy Post

Timber-soft, Hem-Fir, No.2, 6x6 (5-1/2"x5-1/2")

Support: Non-wood

Total length: 5.0'; Clear span: 5.0'; volume = 1.1 cu.ft.; Post and timber

Pinned base; Load face = width(b); Service: wet; $K_e \times L_b: 1.0 \times 5.0 = 5.0$ [ft]; $K_e \times L_d: 1.0 \times 5.0 = 5.0$ [ft];

Analysis vs. Allowable Stress and Deflection using NDS 2015 :

Criterion	Analysis Value	Design Value	Unit	Analysis/Design
Shear	$f_v = 0$	$F_v' = 129$	psi	$f_v/F_v' = 0.00$
Bending(+)	$f_b = 22$	$F_b' = 529$	psi	$f_b/F_b' = 0.04$
Axial	$f_c = 23$	$F_c' = 457$	psi	$f_c/F_c' = 0.05$
Combined (axial + eccentric moment)				Eq.15.4-3 = 0.04
Axial Bearing	$f_c = 23$	$F_c^* = 481$	psi	$f_c/F_c^* = 0.05$
Live Defl'n	$0.00 = < L/999$	$0.50 = L/120$	in	0.00
Total Defl'n	$0.00 = < L/999$	$0.50 = L/120$	in	0.00

Design Notes:

- WoodWorks analysis and design are in accordance with the ICC International Building Code (IBC 2015), the National Design Specification (NDS 2015), and NDS Design Supplement.
- Please verify that the default deflection limits are appropriate for your application.
- FIRE RATING: may be conservative relative to approved code provisions for "short" columns.
- Axial load eccentricity applied in direction of load face only. It is the designers responsibility to check for effect of eccentricity in the other direction.



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Bearing Studs in Wall

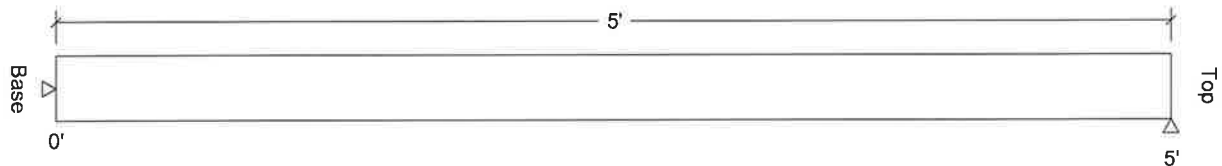
Design Check Calculation Sheet

WoodWorks Sizer 11.1

Loads:

Load	Type	Distribution	Location [ft] Start End	Magnitude Start End	Unit
Load1	Dead	Axial UDL	(Ecc. = 0.58")	75	plf
Load3	Wind	Full Area		25.00 (12.0")	psf
Load4	Snow	Axial UDL	(Ecc. = 0.58")	500	plf
Self-weight	Dead	Axial UDL		12	plf

Lateral Reactions (lbs):



Unfactored:			
Dead	1		-1
Snow	5		-5
Wind	63		63
Factored:			
R->L			-6
Load comb			#2
L->R	38		37

Canopy Support Studs in Wall

Lumber n-ply, D.Fir-L, No.2, 2x4, 2-ply (3"x3-1/2")

Support: Lumber n-ply Bottom plate, D.Fir-L No.2; Bearing length = stud thickness; continuous lower support

Spaced at 12.0" c/c; Total length: 5.0'; Clear span: 4.75'; volume = 0.4 cu.ft.

Pinned base; Load face = width(b); $K_e \times L_b: 1.0 \times 0.0 = 0.0$ [ft]; $K_e \times L_d: 1.0 \times 5.0 = 5.0$ [ft]; Repetitive factor: applied where permitted (refer to online help);

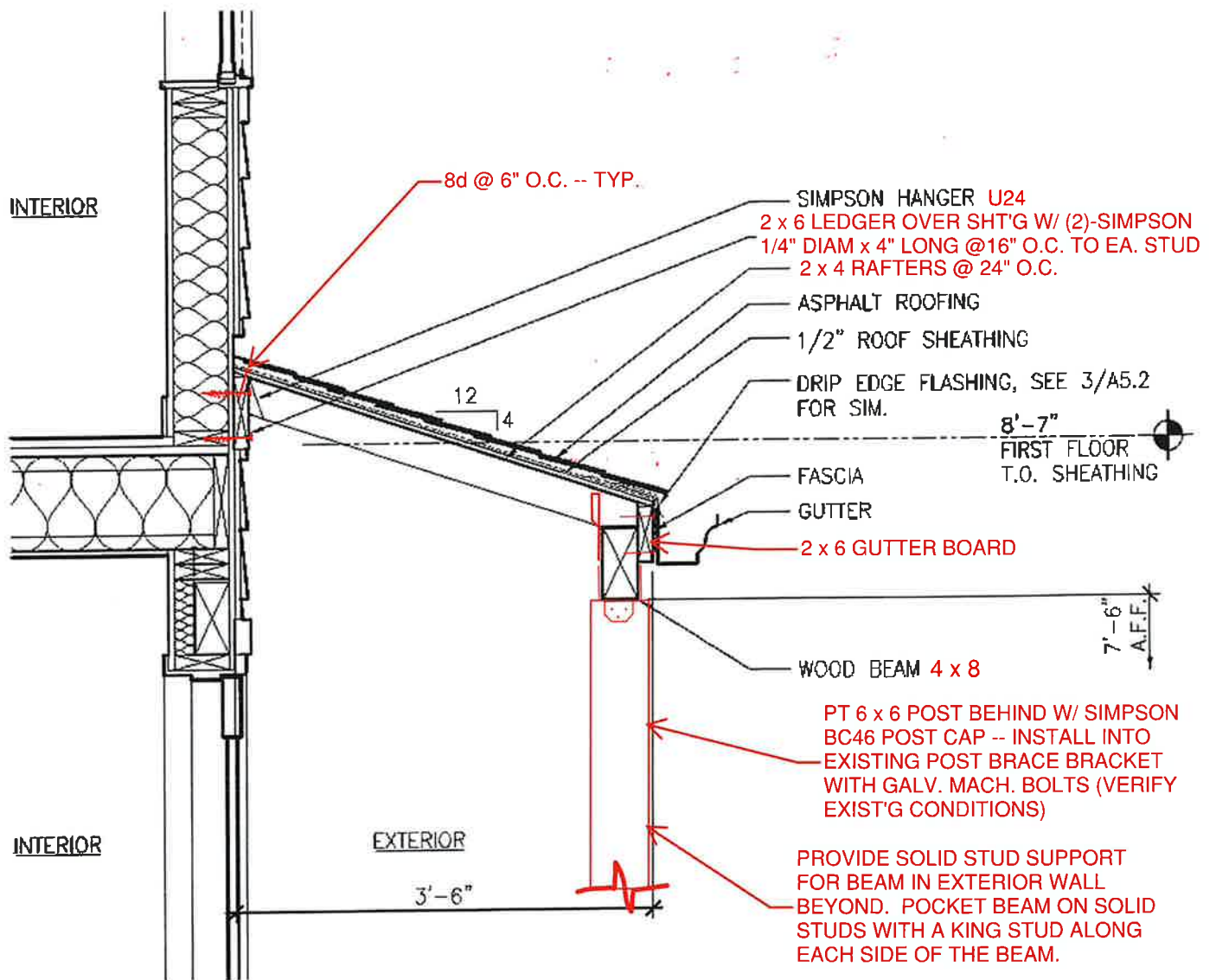
Analysis vs. Allowable Stress and Deflection using NDS 2015 :

Criterion	Analysis Value	Design Value	Unit	Analysis/Design
Shear	$f_v = 5$	$F_v' = 288$	psi	$f_v/F_v' = 0.02$
Bending(+)	$f_b = 95$	$F_b' = 2484$	psi	$f_b/F_b' = 0.04$
Axial	$f_c = 56$	$F_c' = 1173$	psi	$f_c/F_c' = 0.05$
Combined (axial + eccentric & side load bending)				Eq.15.4-1= 0.05
Axial Bearing	$f_c = 56$	$F_c^* = 1785$	psi	$f_c/F_c^* = 0.03$
Support Bearing	$f_{cp} = 56$	$F_{cp} = 703$	psi	$f_{cp}/F_{cp} = 0.08$
Live Defl'n	$0.01 = <L/999$	$0.50 = L/120$	in	0.02
Total Defl'n	$0.01 = <L/999$	$0.50 = L/120$	in	0.03

Design Notes:

- WoodWorks analysis and design are in accordance with the ICC International Building Code (IBC 2015), the National Design Specification (NDS 2015), and NDS Design Supplement.
- Please verify that the default deflection limits are appropriate for your application.
- BUILT-UP COLUMNS: nailed or bolted built-up columns shall conform to the provisions of NDS Clause 15.3.
- FIRE RATING: Joists, wall studs, and multi-ply members are not rated for fire endurance.

SK-1



A

Canopy at Patio Doors

3/4" = 1'-0"

1710 07 3113 13a

SK-1