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# AutoTight® Rod Holdown System

System Design for

### **Tree Farm**



### LYVER ENGINEERING AND DESIGN

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Prepared for **ProTeck** 

prepared by Tom Boydston Commins Project ID # 18-1789

Includes ICC ES 1344 Code Report,

http://www.icc-es.org/reports/pdf\_files/ICC-ES/ESR-1344.pdf#view=fit

and applicable catalog pages.

Engineering Calculations Revision: 1 AutoDesign Revision: 4 Eng

Calcs Date 09/17/2018

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10/11/2018 1 of 12



### (1) Key to Calculation Table

## THIS PAGE SAMPLE RUN ONLY

AutoTight® System Run Design Calc. Sheet for: Engineering Calcs Revision: 1

**Project Name** Plan Set: BID SET

Plan Set Date: mm/dd/vvvv

Run Name:	1				CAT ID#	##-####	
		Run Qty:	4	Te	ensile Stren	gth	Calc'd
	(7)	(	9)				
		(8)	(10)	(11)	(12)	(13)	(14)
Run Specifica	ations	Componer	t Description	Capacity	Demand	D/C	Elong.
Required Lo	ads:	Commins Auto	Tight	(kips)	(kips)	Ratio	(in.)
Level = 2		Componer	t Description	Capacity	Demand	D/C	Elong.
Differential Load:	4.00 (kips)	AT 125	Shrinkage at Level. Shrinkage Device travel & D/C Ratio (in.)	1.10	0.50	45.5%	-
Tension Load:	20.00 (kips)	AT 125	Shrinkage Device (1-1/4" I.D.) - Allowable Load	34.50	4.00	11.6%	-
Compression:	20.00 (kips)	-	Shrinkage Device - Deflection at Load	-	-	-	0.002
Story Height:	12.50 (ft.)	-	Shrinkage Device - Travel and Seating Increment ΔR	-	-	-	0.002
Plate Height:	11.33 (ft.)	S8L	Bearing Plate at Reaction Point	7.96	4.00	50.2%	0.020
Floor Depth:	14.00 (in.)	R9	1-1/8"-A307 Tension Rod	22.37	20.00	89.4%	0.125
		-	No Stretch Rod	#N/A	20.00	0.0%	n/a
		-	Wood Beam Start Bearing Plate	n/a	n/a	0.00	n/a
		-	Steel Beam Start in Tension	n/a	n/a	0.00	n/a
		1	imiting Component Tension Load Capacity, Load and D/C Ratio	22.37	20.00	89.4%	-
		Maximum	Allowed Level Elongation, D/C Ratio and Total Level Elongation	0,200	-	74.5%	0.149
Compression	Outer (1) 4x8	(1) 4x8 Inne	4x Wall Post per Side of Rod-Enter by Hand as Needed	32.08	20,00	62.3%	-
Wood	Posts (3) 2x6	(3) 2x6 Post	6x Wall Post per Side of Rod-Enter by Hand as Needed	30.93	20.00	64.7%	-
Level = F		Componen		Capacity	Demand	D/C	Elong.
Tension Load:	20.00 (kips)	R9	1-1/8"-A307 Anchor Rod	22.37	20.00	89.4%	n/a

- All these cells are filled with data from the AutoTight Run Designer spreadsheet's Project Info page and Load Justification Table page
- The Builder's Name of the project
- The revision level of the plan set.
- The Bid Date.
- The Commins Mfg. project number.
- The Builder's number for the project. (6)
- The name of this run.
- Commins AutoTight part number
- The quantity of this type of run.
- This column is the description of the component shown on each row
- This column of the table is the Load Capacities of the various components. This column of the table is the Load placed on the various components.
- This column of the table is the Demand / Capacity ratio for each component.
- This column is the contribution of each componenent to the total elongation for this level, and the total elongation for the level
- (15) The name of this level.
- (16) Differential Load applied by this level.
- Total tension in rod at this level.
- Compression load on the compression posts at this level.
- (19) Story Height carpet to carpet
- Top of Sill Plate to Top of Sill Plate height of this level. (20)
- This row compares the total shrinkage at this level with the capacity of the AT's to take up this shrinkage.
- (23) This row compares the load capacity of the AT device to the load applied to it. Per AC316 Sec. 1.4.5
   (24) This row shows the deflection of the AT device(s) under the applied load. Per AC316 Sec. 1.4.8
- This row shows the ΔR=Travel and Seating increment of the AT Device(s). Per AC316 Sec. 1.4.7
- (26) This row shows Bearing Plate Load Capacity and compares to its Load also its deflection's contribution to the total Elongation. (unless the calcs call for rod stretch only.) (It sees only the differential load.) Per AF&PA NDS Tbl 4A, 4B incl Cf factor.
- (27) This row shows Tension Rod Load Capacity and compares to its Load, also its deflection's contribution to the total Elongation. Per AISC 360-05
- This row shows Stretch Rod Load Capacity and compares to its Load, also its deflection's contribution to the total Elongation. Only if Stretch Rod is used.
- (29) This row shows the Wood Beam Start's Bearing Plate Load Capacity and compares to its Load, also its deflection's contribution to the total Elongation. (Only if a Wood Beam Start is used.) (It sees the tension load.) Per AF&PA-NDS Tbl 4A, 4B incl Cf factor.
- This row shows the Steel Beam Start's Load Capacity and compares to its Load, also its deflection's contribution to the total Elongation (Only if a Steel Beam Start is used.) (It sees the tension load.) The rod seats on the steel beam and the weld cross section is greater than the rod cross section so the Steel
- Beam Start elongation is included in rod elongation. Per ICC ES-1344 & 5889

  (31) This row shows worst case component's Load and compares to its Load Capacity.
- (32) This row shows the maximum allowed Elongation and the total Elongation calculated for this level.
- This row shows the inner and outer compression post required, their load capacities and loads if the wall is 4x.
- It is used only if Commins Mfg specifies the Compression Posts and is filled in manually. If line is not shown posting is per structural drawing.
- (34) This row shows the inner and outer compression post required, their load capacities and loads if the wall is 6x.
- It is used only if Commins Mfg specifies the Compression Posts and is filled in manually. If line is not shown posting is per structural drawing.
- (35) This row shows the load capacity of the Anchor Rod embedded in the concrete and compares to its load, if used. (Not the concrete strength)
- (36) Anchor bolt elongation is included in the length of the tension rods
- (37) Nuts, Coupler Nuts and Reducing Coupler Nuts are not listed individually because they are grade compatible with the Tension Rod.
- Nuts, Coupler Nuts and Reducing Coupler Nuts calculated contribution to elongation is 0.0005 inch or less.
- (39) Revision level of this document

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AutoTight® System Run Design Calc. Sheet for:

Engineering Calcs Revision: 1 Plan

Tree Farm

Plan Set: Plan Check 2 Plan Set Date: 03/23/2018

ermit #						CAT ID#	18-1789	
Run Name:	EW2ab				Te	nsile Stren	gth	Calc'o
Run Specif Required		Comp	ponent AutoTigi	Description at	Capacity (kips)	Demand (kips)	D/C Ratio	Elong (in.)
Level =	Level 3	Com	ponent	Description	Capacity	Demand	D/C	Elong
Differential Load:	19.86 (kips)	AT10	0A-1.5	Shrinkage at Level, Shrinkage Device travel & D/C Ratio (in.)	1.63"	0.50"	30.7%	-
Tension Load:	19.86 (kips)	AT10	0A-1.5	Shrinkage Device (1-1/4" I.D.) - Allowable Load	28.07	19.86	70.8%	-
Compression:	33.08 (kips)		-	Shrinkage Device - Deflection at Load	-	-	-	0.014
Story Height:	13.00 (ft.)		-	Shrinkage Device - Travel and Seating Increment ΔR	-	-	-	0.000
Plate Height:	11.95 (ft.)	L21-	1-1/4"	Bearing Plate at Reaction Point	21.03	19.86	94.4%	0.038
Floor Depth:	12.63 (in.)	R9/	4307	1 1/8"-A307 Tension Rod	22.37	19.86	88.8%	0.054
			Lim	iting Component Tension Load Capacity, Load and D/C Ratio	21.03	19.86	94.4%	-
		Maxi	mum All	owed Level Elongation, D/C Ratio and Total Level Elongation	0.200	-	53.0%	0.106
Compression Wood	Outer Posts (2) 2x6	(5) 2x6	Inner Posts	6x Wall Compression Post per Comp Post Calc Sheet	36.09	33.08	91.7%	-
Level =	Level 2	Comp	ponent	Description	Capacity	Demand	D/C	Elong
Differential Load:	13.76 (kips)	AT12	2A-1.5	Shrinkage at Level, Shrinkage Device travel & D/C Ratio (in.)	1.63"	0.25"	15.3%	-
Tension Load:	33.62 (kips)	AT12	2A-1.5	Shrinkage Device (1-1/2" I.D.) - Allowable Load	28.07	13.76	49.0%	-
Compression:	50.26 (kips)		-	Shrinkage Device - Deflection at Load	-	-	-	0.010
Story Height:	13.00 (ft.)		-	Shrinkage Device - Travel and Seating Increment ΔR	-	-	-	0.000
Digto Height:	11 OF /#	140	4 4/011	Paging Distant Densition Daint	10.00	12.70	70 70/	0.000

Compression:	50.26	(kips)		-	Shrinkage Device - Deflection at Load	-	-	-	0.010
Story Height:	13.00	(ft.)		-	Shrinkage Device - Travel and Seating Increment ΔR	-	-	-	0.000
Plate Height:	11.95	(ft.)	L18-	-1-1/2"	Bearing Plate at Reaction Point	18.92	13.76	72.7%	0.029
Floor Depth:	12.63	(in.)	R12	2A307	1 1/2"-A307 Tension Rod	39.76	33.62	84.6%	0.129
				Lim	iting Component Tension Load Capacity, Load and D/C Ratio	39.76	33.62	84.6%	-
	Limiting Component Tension Load Capacity, Load and D/C Maximum Allowed Level Elongation, D/C Ratio and Total Level Elong					0.200	-	84.0%	0.168
Compression	Outer			Inner					
Wood	Posts	(2) 2x6	(8) 2x6	Posts	6x Wall Compression Post per Comp Post Calc Sheet	51.56	50.26	97.5%	-

Level =	Footing	Component	Description	Capacity	Demand	D/C	Elong.
Tension Load:	33.62 (kips)	R12A307	1 1/2"-A307 Anchor Rod	39.76	33.62	84.6%	n/a

Design Code: OSSC\_2014 Main/State/Local

Loads per: S702 10/10/2018

Loads Type: ASD Steel Stess Increase: No

Takeup Device at Each Level: Yes Take Off Revision: 4 Eng

Elongation Limit Required: Yes

Elongation Limit per Connection: 0.200 (inch) between load reaction points.

Elongation Components: System Stretch Includes sum of: Rod, Bearing Plate, Shrinkage Device ΔA & Shrinkage Device ΔR.

Shrinkage: 0,250 inch per floor

Shearwall Plates Wood Species: DFL Douglas Fir-Larch Shearwall Plate Compression Capacity (Cross Grain): 625 psi (all grades)

Compression Post Wood Species: DFL Douglas Fir-Larch Compression Post Wood Capacity (Parallel to Grain): 1350 psi

Compression Post Design: per AutoTight

Compression Post Species: per Structural Plans S001

Compression Post Nail Qty. Allowable per 16d Sinker in DFL = 189, Qty nails = 106, Allowable load = 20.03 kips, Total load = 19.86 kips, D/C = 99.1%.

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Take Off Revision: 4 Eng

AutoTight® System Run Design Calc. Sheet for: Engineering Calcs Revision: 1

Tree Farm

Plan Set: Plan Check 2 Plan Set Date: 03/23/2018

Permit #					CAT ID#	18-1789	
Run Name:	EW6			Te	nsile Streng	gth	Calc'd
Run Specif	fications	Component	Description	Capacity	Demand	D/C	Elong.
Required	Loads:	Commins AutoTight		(kips)	(kips)	Ratio	(in.)
Level =	Level 3	Component	Description	Capacity	Demand	D/C	Elong.
Differential Load:	29.81 (kips)	AT16A-2	Shrinkage at Level, Shrinkage Device travel & D/C Ratio (in.)	2.07"	0.50"	24.2%	-
Tension Load:	29.81 (kips)	AT16A-2	Shrinkage Device (2" I.D.) - Allowable Load	39.45	29.81	75.6%	-
Compression:	47.32 (kips)	-	Shrinkage Device - Deflection at Load	-	-	-	0.008
Story Height:	13.00 (ft.)	-	Shrinkage Device - Travel and Seating Increment ΔR	-	-	-	0.001
Plate Height:	11.95 (ft.)	L33-1-1/2"	Bearing Plate at Reaction Point	33.18	29.81	89.9%	0.036
Floor Depth:	12.63 (in.)	R12A307	1 1/2"-A307 Tension Rod	39.76	29.81	75.0%	0,056
		Limit	ng Component Tension Load Capacity, Load and D/C Ratio	33.18	29.81	89.9%	-
		Maximum Allov	wed Level Elongation, D/C Ratio and Total Level Elongation	0.200	-	50.5%	0.101
Compression	Outer	Inner					
Wood	Posts (2) 2x6	6 (8) 2x6 Posts	6x Wall Compression Post per Comp Post Calc Sheet	51.56	47.32	91.8%	-

Level =	Level 2		Comp	onent	Description	Capacity	Demand	D/C	Elong.
Differential Load:	18.23	(kips)	AT1	6A-2	Shrinkage at Level, Shrinkage Device travel & D/C Ratio (in.)	2.07"	0.25"	12.1%	-
Tension Load:	48.04	(kips)	AT1	6A-2	Shrinkage Device (2" I.D.) - Allowable Load	39.45	18.23	46.2%	-
Compression:	70.14	(kips)			Shrinkage Device - Deflection at Load	-	-	-	0.005
Story Height:	13.00	(ft.)			Shrinkage Device - Travel and Seating Increment ΔR	-	-	-	0.001
Plate Height:	11.95	(ft.)	L20	)-2"	Bearing Plate at Reaction Point	18.54	18.23	98.3%	0.039
Floor Depth:	12.63	(in.)	R14/	A307	1 3/4"-A307 Tension Rod	54.12	48.04	88.8%	0.144
				Limiti	ng Component Tension Load Capacity, Load and D/C Ratio	18.54	18.23	98.3%	~
			Maxir	mum Allov	ved Level Elongation, D/C Ratio and Total Level Elongation	0.200	-	94.5%	0.189
Compression	Outer			Inner					
Wood	Posts	(2) 2x6	(12) 2x6	Posts	6x Wall Compression Post per Comp Post Calc Sheet	72.18	70.14	97.2%	~

Level =	Footing	Component	Description	Capacity	Demand	D/C	Elong
Tension Load:	48.04 (kips)	R10G105	1 1/4"-G105 Anchor Rod	57.52	48.04	83.5%	n/a

Design Code: OSSC\_2014 Main/State/Local

Loads per: S702 10/10/2018

Loads Type: ASD

Steel Stess Increase: No Takeup Device at Each Level: Yes

Elongation Limit Required: Yes
Elongation Limit per Connection: 0.200 (inch) between load reaction points.

Elongation Components: System Stretch Includes sum of: Rod, Bearing Plate, Shrinkage Device ΔR & Shrinkage Device ΔR.

Shrinkage: 0.250 inch per floor
Shearwall Plates Wood Species: DFL Douglas Fir-Larch Shearwall Plate Compression Capacity (Cross Grain): 625 psi (all grades)

Compression Post Wood Capacity (Parallel to Grain): 1350 psi Compression Post Wood Species: DFL Douglas Fir-Larch

Compression Post Design: per AutoTight

Compression Post Species: per Structural Plans S001

Compression Post Nail Qty: Allowable per 16d Sinker in DFL = 189, Qty nails = 158, Allowable load = 29.86 kips, Total load = 29.81 kips, D/C = 99.8%.

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Take Off Revision: 4 Eng

psi

Shearwall Plate Compression Capacity (Cross Grain): 625 psi (all grades)

Compression Post Wood Capacity (Parallel to Grain): 1350

AutoTight® System Run Design Calc. Sheet for: Engineering Calcs Revision: 1

Tree Farm

Plan Set: Plan Check 2 Plan Set Date: 03/23/2018

Permit #							CAT ID#	18-1789	
Run Name:	EW6.5					Te	nsile Streng	gth	Calc'd
Run Speci	fications		Com	ponent	Description	Capacity	Demand	D/C	Elong.
Required	Loads:		Commins	AutoTight		(kips)	(kips)	Ratio	(in.)
Level =	Level 3		Com	ponent	Description	Capacity	Demand	D/C	Elong
Differential Load	22.44	(kips)	AT1	DA-1.5	Shrinkage at Level. Shrinkage Device travel & D/C Ratio (in.)	1.63"	0.50"	30.7%	-
Tension Load	22.44	(kips)	AT1	DA-1.5	Shrinkage Device (1-1/4" I.D.) - Allowable Load	28.07	22.44	80.0%	-
Compression	25.75	(kips)		-	Shrinkage Device - Deflection at Load	-	-	-	0.016
Story Height	13.00	(ft.)		-	Shrinkage Device - Travel and Seating Increment ΔR	-	-	-	0.000
Plate Height	11.95	(ft.)	L25-	1-1/4"	Bearing Plate at Reaction Point	24.94	22.44	90.0%	0.036
Floor Depth	12.63	(in.)	R10	A307	1 1/4"-A307 Tension Rod	27.61	22.44	81.3%	0.055
				Limit	ing Component Tension Load Capacity, Load and D/C Ratio	24.94	22.44	90.0%	-
			Maxi	mum Allo	wed Level Elongation, D/C Ratio and Total Level Elongation	0.200	-	53.5%	0.107
Compression	Outer			Inner					
Wood	Posts	(2) 2x6	(3) 2x6	Posts	6x Wall Compression Post per Comp Post Calc Sheet	25.78	25.75	99.9%	-

Level =	Level 2		Comp	onent	Description	Capacity	Demand	D/C	Elong.
Differential Load:	12.55	(kips)	AT12	A-1.5	Shrinkage at Level, Shrinkage Device travel & D/C Ratio (in.)	1.63"	0.25"	15.3%	-
Tension Load:	34.99	(kips)	AT12	A-1.5	Shrinkage Device (1-1/2" I.D.) - Allowable Load	28.07	12.55	44.7%	-
Compression:	39.12	(kips)			Shrinkage Device - Deflection at Load	-	-	-	0.009
Story Height:	13.00	(ft.)			Shrinkage Device - Travel and Seating Increment ΔR	-	-	-	0.000
Plate Height:	11.95	(ft.)	L18-1	-1/2"	Bearing Plate at Reaction Point	18.92	12.55	66.3%	0.027
Floor Depth:	12.63	(in.)	R12/	<b>\307</b>	1 1/2"-A307 Tension Rod	39.76	34.99	88.0%	0.141
				Limiti	ng Component Tension Load Capacity, Load and D/C Ratio	39.76	34.99	88.0%	-
			Maxir	num Allov	ved Level Elongation, D/C Ratio and Total Level Elongation	0.200	-	88.5%	0.177
Compression	Outer			Inner					
Wood	Posts	(2) 2x6	(6) 2x6	Posts	6x Wall Compression Post per Comp Post Calc Sheet	41.25	39.12	94.8%	-

Level =	Footing	Component	Description	Capacity	Demand	D/C	Elong.
Tension Load:	34.99 (kips)	R9G105	1 1/8"-G105 Anchor Rod	46.59	34.99	75.1%	n/a

Design Code: OSSC\_2014 Main/State/Local

Loads per: S702 10/10/2018

Loads Type: ASD Steel Stess Increase: No

Takeup Device at Each Level: Yes

Elongation Limit Required: Yes

Elongation Limit per Connection: 0.200 (inch) between load reaction points. Elongation Components: System Stretch Includes sum of: Rod, Bearing Plate, Shrinkage Device ΔR & Shrinkage Device ΔR.

Shrinkage: 0,250 inch per floor

Shearwall Plates Wood Species: DFL Douglas Fir-Larch

Compression Post Wood Species: DFL Douglas Fir-Larch

Compression Post Design: per AutoTight Compression Post Species: per Structural Plans S001

Compression Post Nail Qty: Allowable per 16d Sinker in DFL = 189, Qty nails = 120, Allowable load = 22.68 kips, Total load = 22.44 kips, D/C = 98.9%.

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AutoTight® System Run Design Calc. Sheet for: Engineering Calcs Revision: 1 Tree Farm

Plan Set: Plan Check 2 Plan Set Date: 03/23/2018

Permit #							CAT ID#	18-1789	
Run Name:	NSB1					Te	nsile Streng	gth	Calc'd
Run Specit	ications		Com	ponent	Description	Capacity	Demand	D/C	Elong.
Required	Loads:		Commins	AutoTight		(kips)	(kips)	Ratio	(in.)
Level =	Level 3		Com	ponent	Description	Capacity	Demand	D/C	Elong.
Differential Load:	23.23	(kips)	AT10	A-1.5	Shrinkage at Level, Shrinkage Device travel & D/C Ratio (in.)	1.63"	0.50"	30.7%	-
Tension Load:	23.23	(kips)	AT10	A-1.5	Shrinkage Device (1-1/4" I.D.) - Allowable Load	28.07	23.23	82.8%	-
Compression:	26.48	(kips)		-	Shrinkage Device - Deflection at Load	-	-	-	0.016
Story Height:	13.00	(ft.)		-	Shrinkage Device - Travel and Seating Increment ΔR	-	-	-	0.000
Plate Height:	11.95	(ft.)	L25-	1-1/4"	Bearing Plate at Reaction Point	24.94	23.23	93.2%	0.037
Floor Depth:	12.63	(in.)	R10	A307	1 1/4"-A307 Tension Rod	27.61	23,23	84.1%	0.057
				Limiti	ng Component Tension Load Capacity, Load and D/C Ratio	24.94	23.23	93.2%	-
			Maxi	mum Alloy	ved Level Elongation, D/C Ratio and Total Level Elongation	0.200	-	55.0%	0,110
Compression	Outer			Inner					
Wood	Posts	(2) 2x6	(4) 2x6	Posts	6x Wall Compression Post per Comp Post Calc Sheet	30.94	26.48	85.6%	-

Level =	Level 2		Com	ponent	Description	Capacity	Demand	D/C	Elong.
Differential Load:	12.94	(kips)	AT1	2A-1.5	Shrinkage at Level, Shrinkage Device travel & D/C Ratio (in.)	1.63"	0.25"	15.3%	-
Tension Load:	36.17	(kips)	AT1	2A-1.5	Shrinkage Device (1-1/2" I.D.) - Allowable Load	28.07	12.94	46.1%	-
Compression:	40.23	(kips)		-	Shrinkage Device - Deflection at Load	-	-	-	0.009
Story Height:	13.00	(ft.)		-	Shrinkage Device - Travel and Seating Increment ΔR	-	-	-	0.000
Plate Height:	11.95	(ft.)	L18-	1-1/2"	Bearing Plate at Reaction Point	18.92	12.94	68.4%	0.027
Floor Depth:	12.63	(in.)	R12	A307	1 1/2"-A307 Tension Rod	39.76	36.17	91.0%	0.146
				Limit	ing Component Tension Load Capacity, Load and D/C Ratio	39.76	36.17	91.0%	-
			Maxi	mum Allo	wed Level Elongation, D/C Ratio and Total Level Elongation	0.200	-	91.5%	0.183
Compression	Outer			Inner					
Wood	Posts	(2) 2x6	(6) 2x6	Posts	6x Wall Compression Post per Comp Post Calc Sheet	41.25	40.23	97.5%	-

Level =	Footing	Component	Description	Capacity	Demand	D/C	Elong.
Tension Load:	36.17 (kips)	R9G105	1 1/8"-G105 Anchor Rod	46.59	36.17	77.6%	n/a
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Design Code: OSSC\_2014 Main/State/Local

Loads per: S702 10/10/2018

Loads Type: ASD Steel Stess Increase: No

Takeup Device at Each Level: Yes Take Off Revision: 4 Eng

Elongation Limit Required: Yes
Elongation Limit per Connection: 0.200 (inch) between load reaction points.

Elongation Components: System Stretch Includes sum of: Rod, Bearing Plate, Shrinkage Device ΔR & Shrinkage Device ΔR.

Shrinkage: 0,250 inch per floor

Shearwall Plates Wood Species: DFL Douglas Fir-Larch Shearwall Plate Compression Capacity (Cross Grain). 625 psi (all grades)

Compression Post Wood Species: DFL Douglas Fir-Larch Compression Post Wood Capacity (Parallel to Grain): 1350 psi

Compression Post Design: per AutoTight

Compression Post Species: per Structural Plans S001

Compression Post Nail Qty. Allowable per 16d Sinker in DFL = 189, Qty nails = 124, Allowable load = 23.44 kips, Total load = 23.23 kips, D/C = 99.1%.

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Take Off Revision: 4 Eng

AutoTight® System Run Design Calc. Sheet for: Engineering Calcs Revision: 1

**Tree Farm** 

Plan Set: Plan Check 2

Plan Set Date: 03/23/2018

Permit #					CAT ID#	18-1789	
Run Name:	NSC1		T	Te	nsile Streng	gth	Calc'o
Run Specif Required		Component Commins AutoTigi	Description nt	Capacity (kips)	Demand (kips)	D/C Ratio	Elong. (in.)
Level =	Level 3	Component	Description	Capacity	Demand	D/C	Elong
Differential Load:	22.38 (kips)	AT10A-1.5	Shrinkage at Level, Shrinkage Device travel & D/C Ratio (in.)	1.63"	0.50"	30.7%	-
Tension Load:	22.38 (kips)	AT10A-1.5	Shrinkage Device (1-1/4" I.D.) - Allowable Load	28.07	22.38	79.7%	-
Compression:	23.99 (kips)	-	Shrinkage Device - Deflection at Load	-	-	-	0.016
Story Height:	13.00 (ft.)	-	Shrinkage Device - Travel and Seating Increment ΔR	-	-	-	0.000
Plate Height:	11.95 (ft.)	L25-1-1/4"	Bearing Plate at Reaction Point	24.94	22.38	89.8%	0.038
Floor Depth:	12.63 (in.)	R10A307	1 1/4"-A307 Tension Rod	27.61	22.38	81.1%	0.054
		Lim	iting Component Tension Load Capacity, Load and D/C Ratio	24.94	22.38	89.8%	-
		Maximum All	owed Level Elongation, D/C Ratio and Total Level Elongation	0.200	-	53.0%	0.106
Compression Wood	Outer Posts (2) 2x6	(3) 2x6   Inner   Posts	6x Wall Compression Post per Comp Post Calc Sheet	25.78	23.99	93.1%	
Level =	Level 2	Component	Description	Capacity	Demand	D/C	Elong
Differential Load:	12.06 (kips)	AT12A-1.5	Shrinkage at Level, Shrinkage Device travel & D/C Ratio (in.)	1.63"	0.25"	15.3%	-
Tension Load:	34 44 (kips)	AT12A-1 5	Shrinkage Device (1-1/2" LD.) - Allowable Load	28.07	12.06	43.0%	_

Level =	Level 2		Com	ponent	Description	Capacity	Demand	D/C	Elong.
Differential Load:	12.06	(kips)	AT1	2A-1.5	Shrinkage at Level, Shrinkage Device travel & D/C Ratio (in.)	1.63"	0.25"	15.3%	-
Tension Load:	34.44	(kips)	AT1	2A-1.5	Shrinkage Device (1-1/2" I.D.) - Allowable Load	28.07	12.06	43.0%	-
Compression:	36.46	(kips)		-	Shrinkage Device - Deflection at Load	-	-	-	0.009
Story Height:	13.00	(ft.)		-	Shrinkage Device - Travel and Seating Increment ΔR	-	-	-	0.000
Plate Height:	11.95	(ft.)	L18-	1-1/2"	Bearing Plate at Reaction Point	18.92	12.06	63.8%	0.026
Floor Depth:	12.63	(in.)	R12	A307	1 1/2"-A307 Tension Rod	39.76	34.44	86.6%	0.139
				Limit	ing Component Tension Load Capacity, Load and D/C Ratio	39.76	34.44	86.6%	-
			Maxi	mum Allo	wed Level Elongation, D/C Ratio and Total Level Elongation	0.200	-	86.5%	0.173
Compression	Outer			Inner					
Wood	Posts	(2) 2x6	(6) 2x6	Posts	6x Wall Compression Post per Comp Post Calc Sheet	41.25	36.46	88.4%	-

Level = Footing	Component	Description	Capacity	Demand	D/C	Eleng.
Tension Load: 34.44 (kip	os) R9G105	1 1/8"-G105 Anchor Rod	46.59	34.44	73.9%	n/a

Design Code: OSSC\_2014 Main/State/Local

Loads per: S702 10/10/2018

Loads Type: ASD Steel Stess Increase: No Takeup Device at Each Level: Yes

Elongation Limit Required: Yes
Elongation Limit per Connection: 0.200 (inch) between load reaction points.

Elongation Components: System Stretch Includes sum of: Rod, Bearing Plate, Shrinkage Device ΔR & Shrinkage Device ΔR.

Shrinkage: 0,250 inch per floor Shearwall Plates Wood Species: DFL Douglas Fir-La

Douglas Fir-Larch Shearwall Plate Compression Capacity (Cross Grain): 625 psi (all grades)

Compression Post Wood Species: DFL Douglas Fir-Larch Compression Post Wood Capacity (Parallel to Grain): 1350 psi

Compression Post Design: per AutoTight

Compression Post Species: per Structural Plans S001

Compression Post Nail Qty: Allowable per 16d Sinker in DFL = 189, Qty nails = 120, Allowable load = 22.68 kips, Total load = 22.38 kips, D/C = 98.7%.

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AutoTight® System Run Design Calc. Sheet for: Engineering Calcs Revision: 1

Tree Farm

Plan Set: Plan Check 2 Plan Set Date: 03/23/2018

Permit #						CAT ID#	18-1789	
Run Name:	NSC2				Te	nsile Streng	gth	Calc'd
Run Specit	fications	Com	ponent	Description	Capacity	Demand	D/C	Elong.
Required	Loads:	Commins	AutoTight		(kips)	(kips)	Ratio	(in.)
Level =	Level 3	Com	ponent	Description	Capacity	Demand	D/C	Elong
Differential Load:	20.42 (kips)	AT10	DA-1.5	Shrinkage at Level, Shrinkage Device travel & D/C Ratio (in.)	1.63"	0.50"	30.7%	-
Tension Load:	20.42 (kips)	AT10	DA-1.5	Shrinkage Device (1-1/4" I.D.) - Allowable Load	28.07	20.42	72.8%	-
Compression:	22.99 (kips)		-	Shrinkage Device - Deflection at Load	-	-	-	0.014
Story Height:	13.00 (ft.)		-	Shrinkage Device - Travel and Seating Increment ΔR	-	-	-	0.000
Plate Height:	11.95 (ft.)	L21-	1-1/4"	Bearing Plate at Reaction Point	21.03	20.42	97.1%	0,039
Floor Depth:	12.63 (in.)	R9/	A307	1 1/8"-A307 Tension Rod	22.37	20.42	91.3%	0.056
			Limit	ing Component Tension Load Capacity, Load and D/C Ratio	21.03	20.42	97.1%	-
		Maxi	mum Allo	wed Level Elongation, D/C Ratio and Total Level Elongation	0.200	-	54.5%	0.109
Compression	Outer		Inner					
Wood	Posts (2) 2x6	(3) 2x6	Posts	6x Wall Compression Post per Comp Post Calc Sheet	25.78	22.99	89.2%	-

Level =	Level 2		Com	ponent	Description	Capacity	Demand	D/C	Elong.
Differential Load:	11.30	(kips)	AT1	2A-1.5	Shrinkage at Level, Shrinkage Device travel & D/C Ratio (in.)	1.63"	0.25"	15.3%	-
Tension Load:	31.72	(kips)	AT1	2A-1.5	Shrinkage Device (1-1/2" I.D.) - Allowable Load	28.07	11.30	40.3%	-
Compression:	34.94	(kips)		-	Shrinkage Device - Deflection at Load	-	-	-	0.008
Story Height:	13.00	(ft.)		-	Shrinkage Device - Travel and Seating Increment ΔR	-	-	-	0.000
Plate Height:	11.95	(ft.)	L18-	1-1/2"	Bearing Plate at Reaction Point	18.92	11.30	59.7%	0.024
Floor Depth:	12.63	(in.)	R12	A307	1 1/2"-A307 Tension Rod	39.76	31.72	79.8%	0.121
				Limit	ting Component Tension Load Capacity, Load and D/C Ratio	39.76	31.72	79.8%	~
			Max	mum Allo	owed Level Elongation, D/C Ratio and Total Level Elongation	0.200	-	76.5%	0.153
Compression	Outer			Inner					
Wood	Posts	(2) 2x6	(5) 2x6	Posts	6x Wall Compression Post per Comp Post Calc Sheet	36.09	34.94	96.8%	-

Level = Foo	oting	Component	Description	Capacity	Demand	D/C	Elong.
Tension Load: 3	1.72 (kips)	R12A307	1 1/2"-A307 Anchor Rod	39.76	31.72	79.8%	n/a

Design Code: OSSC\_2014 Main/State/Local

Loads per: S702 10/10/2018

Loads Type: ASD

Steel Stess Increase:

Takeup Device at Each Level:

Elongation Limit Required: Yes
Elongation Limit per Connection: 0.200 (inch) between load reaction points.

Shrinkage: 0,250 inch per floor
Shearwall Plates Wood Species: DFL Douglas Fir-Larch

Compression Post Wood Species: DFL Douglas Fir-Larch Compression Post Design: per AutoTight

Compression Post Species: per Structural Plans S001

No Yes

Elongation Components: System Stretch Includes sum of: Rod, Bearing Plate, Shrinkage Device ΔR & Shrinkage Device ΔR.

Shearwall Plate Compression Capacity (Cross Grain): 625

Compression Post Wood Capacity (Parallel to Grain): 1350 psi

psi (all grades)

Take Off Revision: 4 Eng

Compression Post Nail Qty: Allowable per 16d Sinker in DFL = 189, Qty nails = 110, Allowable load = 20.79 kips, Total load = 20.42 kips, D/C = 98.2%.

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AutoTight® System Run Design Calc. Sheet for:

**Engineering Calcs Revision: 1** 

**Tree Farm** 

Plan Set: Plan Check 2 Plan Set Date: 03/23/2018

Permit #						CAT ID#	18-1789	
Run Name:	NSD				Te	nsile Streng	gth	Calc'd
Run Specif	ications	Com	ponent	Description	Capacity	Demand	D/C	Elong
Required	Loads:	Commins	AutoTigh	rt .	(kips)	(kips)	Ratio	(in.)
Level =	Level 2	Com	ponent	Description	Capacity	Demand	D/C	Elong
Differential Load:	26.23 (kips)	AT1	0A-1.5	Shrinkage at Level, Shrinkage Device travel & D/C Ratio (in.)	1.63"	0.25"	15.3%	-
Tension Load:	26.23 (kips)	AT1	0A-1.5	Shrinkage Device (1-1/4" I.D.) - Allowable Load	28.07	26.23	93.5%	-
Compression:	30.43 (kips)		-	Shrinkage Device - Deflection at Load	-	-	-	0.01
Story Height:	13.00 (ft.)		-	Shrinkage Device - Travel and Seating Increment ΔR	-	-	-	0.00
Plate Height:	11.95 (ft.)	L28-	1-1/4"	Bearing Plate at Reaction Point	27.28	26.23	96.2%	0.03
Floor Depth:	12.63 (in.)	R10	A307	1 1/4"-A307 Tension Rod	27.61	26.23	95.0%	0.07
			Limi	ting Component Tension Load Capacity, Load and D/C Ratio	27.28	26.23	96.2%	-
		Max	mum Alk	owed Level Elongation, D/C Ratio and Total Level Elongation	0.200	-	65.0%	0.13
Compression	Outer		Inner					
Wood	Posts (2) 2x6	(4) 2x6	Posts	6x Wall Compression Post per Comp Post Calc Sheet	30.94	30.43	98.4%	-

Level = 1	-ooting	Component	Description	Capacity	Demand	D/C	Elong
Tension Load:	26.23 (kips)	R9G105	1 1/8"-G105 Anchor Rod	46.59	26.23	56.3%	n/a

Design Code: OSSC\_2014 Main/State/Local Loads per: S702 10/10/2018

Loads per: S702 10/10/2018

Loads Type: ASD

Steel Stess Increase: No

Takeup Device at Each Level: Yes
Elongation Limit Required: Yes
Elongation Limit per Connection: 0.200 (inch) between load reaction points.

Elongation Components: System Stretch Includes sum of: Rod, Bearing Plate, Shrinkage Device ΔA & Shrinkage Device ΔR. Shrinkage: 0.250 inch per floor

Shearwall Plates Wood Species: DFL Douglas Fir-Larch
Compression Post Wood Species: DFL Douglas Fir-Larch

Shearwall Plate Compression Capacity (Cross Grain): 625 Compression Post Wood Capacity (Parallel to Grain): 1350

psi (all grades) psi

Take Off Revision: 4 Eng

Compression Post Design: per AutoTight

Compression Post Species: per Structural Plans S001
Compression Post Nail Qty: Allowable per 16d Sinker in DFL = 189, Qty nails = 140, Allowable load = 26.46 kips, Total load = 26.23 kips, D/C = 99.1%.

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AutoTight® System Run Design Calc. Sheet for: Engineering Calcs Revision: 1

**Tree Farm** 

Plan Set: Plan Check 2

Plan Set Date: 03/23/2018

Permit #						CAT ID#	18-1789	
Run Name:	NSE				Te	nsile Streng	gth	Calc'd
Run Specif	fications	Comp	onent	Description	Capacity	Demand	D/C	Elong.
Required	Loads:	Commins	AutoTight		(kips)	(kips)	Ratio	(in.)
Level =	Level 3	Comp	onent	Description	Capacity	Demand	D/C	Elong
Differential Load:	27.20 (kips)	AT10	A-1.5	Shrinkage at Level, Shrinkage Device travel & D/C Ratio (in.)	1.63"	0.50"	30.7%	-
Tension Load:	27.20 (kips)	AT10	A-1.5	Shrinkage Device (1-1/4" I.D.) - Allowable Load	28.07	27.20	96.9%	-
Compression:	56.01 (kips)		-	Shrinkage Device - Deflection at Load	-	-	-	0.019
Story Height:	13.00 (ft.)		-	Shrinkage Device - Travel and Seating Increment ΔR	-	-	-	0.000
Plate Height:	11.95 (ft.)	L28-1	1-1/4"	Bearing Plate at Reaction Point	27.28	27.20	99.7%	0.040
Floor Depth:	12.63 (in.)	R10/	4307	1 1/4"-A307 Tension Rod	27.61	27.20	98.5%	0.062
			Limit	ing Component Tension Load Capacity, Load and D/C Ratio	27.28	27.20	99.7%	-
		Maxir	mum Allo	wed Level Elongation, D/C Ratio and Total Level Elongation	0.200	-	61.0%	0.122
Compression	Outer		Inner					
Wood	Posts (2) 2x6	(9) 2x6	Posts	6x Wall Compression Post per Comp Post Calc Sheet	56.72	56.01	98.7%	-

Level =	Level 2		Comp	ponent	Description	Capacity	Demand	D/C	Elong.
Differential Load:	17.37	(kips)	AT1	6A-2	Shrinkage at Level, Shrinkage Device travel & D/C Ratio (in.)	2.07"	0.25"	12.1%	-
Tension Load:	44.57	(kips)	AT1	6A-2	Shrinkage Device (2" I.D.) - Allowable Load	39.45	17.37	44.0%	**
Compression:	80.97	(kips)		-	Shrinkage Device - Deflection at Load	-	-	-	0.005
Story Height:	13.00	(ft.)		-	Shrinkage Device - Travel and Seating Increment ΔR	-	-	-	0.001
Plate Height:	11.95	(ft.)	L18	3-2"	Bearing Plate at Reaction Point	17.96	17.37	96.7%	0.039
Floor Depth:	12.63	(in.)	R14	A307	1 3/4"-A307 Tension Rod	54.12	44.57	82.4%	0.126
				Limit	ng Component Tension Load Capacity, Load and D/C Ratio	17.96	17.37	96.7%	-
			Maxi	mum Allo	wed Level Elongation, D/C Ratio and Total Level Elongation	0.200	-	85.0%	0.170
Compression	Outer			Inner					
Wood	Posts	(2) 2x6	(14) 2x6	Posts	6x Wall Compression Post per Comp Post Calc Sheet	82.50	80.97	98.1%	-

Level = Footing	Component	Description	Capacity	Demand	D/C	Elong.
Tension Load: 44.57 (kips)	R14A307	1 3/4"-A307 Anchor Rod	54.12	44.57	82.4%	n/a

Design Code: OSSC\_2014 Main/State/Local

Loads per: S702 10/10/2018

Loads Type: ASD Steel Stess Increase: No

Takeup Device at Each Level: Yes Take Off Revision: 4 Eng

Elongation Limit Required: Yes
Elongation Limit per Connection: 0.200 (inch) between load reaction points.

Elongation Components: System Stretch Includes sum of: Rod, Bearing Plate, Shrinkage Device ΔR & Shrinkage Device ΔR.

Shrinkage: 0.250 inch per floor
Shearwall Plates Wood Species: DFL Douglas Fir-Larch Shearwall Plate Compression Capacity (Cross Grain): 625 psi (all grades)

Compression Post Wood Species: DFL Douglas Fir-Larch Compression Post Wood Capacity (Parallel to Grain): 1350 psi

Compression Post Design: per AutoTight

Compression Post Species: per Structural Plans S001

Compression Post Nail Qty: Allowable per 16d Sinker in DFL = 189, Qty nails = 144, Allowable load = 27.22 kips, Total load = 27.20 kips, D/C = 99.9%.

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17.67 14.55

Take Off Revision: 4 Eng.

82.3%

AutoTight® System Run Design Calc. Sheet for: Engineering Calcs Revision: 1

Tree Farm

Plan Set: Plan Check 2 Plan Set Date: 03/23/2018

ermit #					CAT ID#	18-1789	
Run Name:	NSC.3			Te	nsile Stren	gth	Calc'd
Run Specifi	cations	Component	Description	Capacity	Demand	D/C	Elong.
Required L	_oads:	Commins AutoTig	nt	(kips)	(kips)	Ratio	(in.)
Level =	Level 2	Component	Description	Capacity	Demand	D/C	Elong.
Differential Load:	14.55 (kips)	AT8A-1.5	Shrinkage at Level, Shrinkage Device travel & D/C Ratio (in.)	1.75"	0.25"	14.3%	-
Tension Load:	14.55 (kips)	AT8A-1.5	Shrinkage Device (1" I.D.) - Allowable Load	20.73	14.55	70.2%	-
Compression:	21.10 (kips)	-	Shrinkage Device - Deflection at Load	-	-	-	0.003
Story Height:	13.00 (ft.)	-	Shrinkage Device - Travel and Seating Increment ΔR	-	-	-	0.000
Plate Height:	11.95 (ft.)	L18-1-1/4"	Bearing Plate at Reaction Point	19.29	14.55	75.4%	0.030
Floor Depth:	12.63 (in.)	R8A307	1"-A307 Tension Rod	17.67	14.55	82.3%	0.053
		Lim	iting Component Tension Load Capacity, Load and D/C Ratio	17.67	14.55	82.3%	-
		Maximum All	owed Level Elongation, D/C Ratio and Total Level Elongation	0.200	-	43.5%	0.087
Compression	Outer	Inner					
Wood	Posts (2) 2x6	(3) 2x6 Posts	6x Wall Compression Post per Comp Post Calc Sheet	25.78	21.10	81.8%	-
Level =	Footing	Component	Description	Capacity	Demand	D/C	Elong.

Design Code: OSSC\_2014 Main/State/Local

R8A307

Loads per: S702 10/10/2018

Loads Type: ASD

Steel Stess Increase: No Takeup Device at Each Level: Yes
Elongation Limit Pequired: Yes
Elongation Limit per Connection: 0,200 (inch) between load reaction points.

Tension Load: 14.55 (kips)

Elongation Components: System Stretch Includes sum of: Rod, Bearing Plate, Shrinkage Device  $\Delta A$  & Shrinkage Device  $\Delta R$ .

1"-A307 Anchor Rod

Shrinkage: 0,250 inch per floor
Shearwall Plates Wood Species: DFL Douglas Fir-Larch
Compression Post Wood Species: DFL Douglas Fir-Larch Shearwall Plate Compression Capacity (Cross Grain): 625 psi (all grades) Compression Post Wood Capacity (Parallel to Grain): 1350 psi

Compression Post Design: per AutoTight

Compression Post Species: per Structural Plans S001
Compression Post Nail Qty: Allowable per 16d Sinker in DFL = 189, Qty nails = 78, Allowable load = 14.74 kips, Total load = 14.55 kips, D/C = 98.7%.

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### AutoTight® Mid Wall Termination Header Design Calculations for: Tree Farm

Take Off Revision: 4 Eng Calcs Code:OSSC\_2014 Main/State/Local (2005 NDS)

Calcs Revision: 1

Plan Set: Plan Check 2

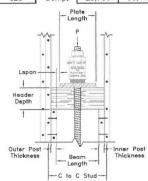
Plan Date: 03/23/2018

CAT Project ID: 18-1789

C to C Stud	Bay Width/2	Outer Post Thickness	Inner Post Thickness	Beam Length	Bearing Plate Length, L	Bearing Plate L / 2 (in)	Lspan	Term Header Species	Header Min Size	Header Width	Header Depth	Applied Load Compression	Allowable Capacity psi	section modulus	Allowable Capacity	Demand/ Capacity Ratio	Wall Thickness
(in)	(in)	(in)	(in)	(in)	(in)	(in)	(in)		(Nominal)	(in)	(in)	P (lbs)	DFL	Z	(lb)	D/C	
	E14/0 1			ı	104 4 4 4 4 1	Desertes	Dista Name										
16.00	7.25	3.00	7.50	7.00	7.00	= Bearing 3,50	Plate Name 0.00	DFL	4x6	5.50	3.50	19.860	625	11.23	NA>Shear	NA>Shear	6x Wall
-	g above		1,50	7.00	1 7.00	0.00	1 0.00	DIL	1770	1 0.00	0.00	10,000	020	11.20	Tre Citodi	TO COLOUR	07(110)
Shear:				7.00	7.00	] :	Shear Load F	raction =	0.00	5.50	3.50	0	625	Shear	16,042	0.0%	6x Wall
Compr	ession:	3.00	7.50			В	learing Area	per end =	57.75	5.50		19,860	625	Comp.	36,094	55.0%	6x Wall
Run:	EMB			1	1 33-1-1/2"	= Bearing	Plate Name										
16,00		3,00	12.00	7.00	10.00	5.00	-1.50	DFL	4x6	5,50	3,50	29,810	625	11.23	NA>Shear	NA>Shear	6x Wall
Bendin	g above	:					A	A									
Shear:				7.00	10.00	1	Shear Load F		0.00	5.50	3.50	0	625	Shear	16,042	0.0%	6x Wall
Compr	ession:	3.00	12.00			В	learing Area	per end =	82.50	5.50		29,810	625	Comp.	51,563	57.8%	6x Wall
Run:	EW6.5			1	L25-1-1/4"	= Bearing	Plate Name										
16.00	_	3.00	4.50	7.00	7.50	3.75	-0.25	DFL	4x6	5.50	3.50	22,440	625	11.23	NA>Shear	NA>Shear	6x Wall
Bendin	g above	:			·	,											
Shear:				7.00	7.50		Shear Load I		0.00	5.50	3,50	0	625	Shear	16,042	0.0%	6x Wall
Compr	ession:	3.00	4.50			В	learing Area	per ena =	41.25	5,50	1	22,440	625	Comp.	25,781	87.0%	6x Wall
Run:	NSB1				L25-1-1/4"	= Bearing	Plate Name										
16.00		3.00	6.00	7.00	7.50	3.75	-0.25	DFL	4x6	5.50	3.50	23,230	625	11.23	NA>Shear	NA>Shear	6x Wall
	g above	:				1											
Shear:		0.00	1 0.00	7.00	7.50		Shear Load F		0.00 49.50	5.50	3.50	23,230	625 625	Shear Comp.	16,042 30,938	0.0% 75.1%	6x Wall
Compr	ession:	3,00	6.00			D	learing Area	per ena -	49.50	3.50	J	23,230	025	Comp.	30,936	73.170	OX AAdii
Run:	NSC1				L25-1-1/4"	= Bearing	Plate Name										
16.00	7.25	3.00	4.50	7.00	7.50	3.75	-0.25	DFL	4x6	5.50	3.50	22,380	625	11.23	NA>Shear	NA>Shear	6x Wall
	g above	:			7.50	1 .	0		0.00	T 5.50	0.50	0	625	01	16,042	0.0%	6x Wall
Shear:	ession:	3.00	4.50	7.00	7.50	1	Shear Load F earing Area		0.00 41.25	5.50	3.50	22,380	625	Shear Comp.	25,781	86.8%	6x Wall
Compi	C331011.	3.00	4.50				cuming / tou	por one	71.20	0.00	ı	22,000	020	oomp.	20,101	00.070	
	NSC2						Plate Name										
16,00		3,00	4.50	7.00	7.00	3.50	0,00	DFL	4x6	5.50	3,50	20,420	625	11.23	NA>Shear	NA>Shear	6x Wall
Shear:	g above	:		7.00	7,00	1 .	Shear Load F	raction -	0,00	5,50	3,50	0	625	Shear	16,042	0.0%	6x Wall
	ession:	3.00	4.50	7,00	7.00	1	earing Area		41.25	5.50	3.30	20,420	625	Comp.	25,781	79.2%	6x Wall
озр.						_	3										
Run:							Plate Name								I a.		
16.00	7.25	3.00	6.00	7.00	9.00	4.50	-1.00	DFL	4x6	5.50	3,50	26,230	625	11.23	NA>Shear	NA>Shear	6x Wall
Shear:	g above			7.00	9.00	1 :	Shear Load F	raction =	0.00	5.50	3.50	0	625	Shear	16,042	0.0%	6x Wall
	ession:	3.00	6.00	7.00	0.00		earing Area		49.50	5.50	0.00	26,230	625	Comp.	30,938	84.8%	6x Wall
												-					
Run:				W 00			Plate Name	1 55		1 = =0	0.50	07.000	005	44.00	Thin Chan	NA Ch	6x Wall
16.00		3.00	13,50	7.00	9.00	4.50	-1.00	DFL	4x6	5.50	3,50	27,200	625	11.23	NA>Shear	NA>Snear	ex Maii
Shear:	g above			7.00	9.00	1 :	Shear Load F	raction =	0.00	5.50	3.50	0	625	Shear	16,042	0.0%	6x Wall
Compr	ession:	3.00	13.50			1	earing Area	CALCULATION CO.	90.75	5.50		27,200	625	Comp.	56,719	48.0%	6x Wall
	NSC.3	0.00	1.50	7.00			Plate Name	DEL	4:-0	T = = 0	2.50	11.550	025	11 00	10.715	77 70/	Cv Mell
16.00	7.25 g above	3.00	4.50	7.00	5.50	2.75	0.75	DFL	4x6	5.50	3,50	14,550	625	11.23	18,715	77.7%	6x Wall
Shear:	a anove	•		7.00	5.50		Shear Load F	raction =	0.00	5.50	3.50	0	625	Shear	16,042	0.0%	6x Wall
Compr	ession:	3.00	4.50				earing Area		41.25	5.50		14,550	625	Comp.	25,781	56.4%	6x Wall
										-							

#### Header Design Notes:

- Bearing Plate spreads load.
- 2. Point Load (P) location transfer of combined termination tension.
- 3. Beam supported at both ends 2 equal symmetrical loads max stress=W\*a/Z where a= Lspan & W=P/2 & Z=section modulus of beam
- 4. Shear calculated per NDS 2005 eqn 3.4-2 & sec 3.4.3 which says:
- "...uniformly distributed loads within a distance from supports equal to the depth of the bending member, d, shall be permitted to be ignored."
- fv=3\*V/2\*b\*d where fv=actual stress=species capacity, V=shear load=allowable, b=breadth, d=depth
- 5. When the plate overlaps the post or gets too close to the post the beam equation does not apply, see shear instead.



### Compression Post Schedule 6x Wall

### **Tree Farm**

18-1789

Z	Run Name	EW2ab	EW6	EW6.5	NSB1	NSC1	NSC2	NSD	NSE	NSC.3
Š	Wall Size	6x Wall								
	Post Location	Outer Inner								
	Post Size	2x6 2x6	2x6 2x6	2x6 2x6	2x6 : 2x6	2x6 2x6	2x6 2x6	1	2x6 2x6	
w	Post Qty	2 5	2 8	2 3	2 4	2 3	2 3		2 9	
O	Post Length inches	54.00	54.00	54.00	54.00	54.00	54.00		54.00	
1	Required Load kips	33.08	47.32	25.75	26.48	23.99	22.99		56.01	
L	Allowable Load kips	36.09	51.56	25.78	30.94	25.78	25.78		56.72	
	Limiting Failure Mode	Crushing	Crushing	Crushing	Crushing	Crushing	Crushing		Crushing	

	Post Size	2x6   2x6	2x6   2x6	2x6 : 2x6	2x6   2x6	2x6 2x6	2x6   2x6	2x6 : 2x6	2x6 : 2x6	2x6 : 2x6
12	Post Qty	2 8	2 12	2 6	2 6	2 6	2 5	2 4	2 14	2 3
O	Post Length inches	137.88	137.88	137.88	137.88	137.88	137.88	54.00	137.88	54.00
€	Required Load kips	50.26	70.14	39.12	40.23	36.46	34.94	30.43	80.97	21.10
L	Allowable Load kips	51.56	72.18	41.25	41.25	41.25	36.09	30.94	82.50	25.78
	Limiting Failure Mode	Crushing	Crushing	Crushing	Crushing	Crushing	Crushing	Crushing	Crushing	Crushing

#### Notes:

- 1. Posts may be arranged as desired by the builder as long as:
  - a. The total post quantity is the same as or greater than the quantity listed here.
  - b. And there is at least 1 post on each side of each rod.
  - c. Compression post lengths shown in schedule are for calculation purposes only. Framer is responsible for actual post lengths.
- 2. These Posts are in addition to post counts on Plans.
- 3. Sill Plates are Douglas Fir-Larch Grade #2 or better.
- 4. Compression Posts are Douglas Fir-Larch Grade #2 or better.

Office: 360-378-9484 Fax: 360-378-9485

AutoTight® Holdown Systems

by Commins Manufacturing



### Structural · Civil Engineers

**Submittal Transmittal** 

Fo: Guerrilla Developme	ent
-------------------------	-----

2500 NE Sandy Blvd, Suite C

Portland, OR 97232

Attn: Kevin Cavenaugh

cc: Ben Carr, BSA

From:

Brynn Adkins

Date: Job Name: August 6, 2018

Job No.:

Tree Farm 17001.40

File:

17001 trans submit take up 2.docx

Submitted item:  Auto Tight Tie Down  Fabricator / Manufacturer: Date received:  O8/06/2018  Reviewed as checked below:  Reviewed as noted Revise & resubmit Sheet numbers reviewed:  ATS10, ATS11 Sh1, ATS11 Sh2, ATS12, RL-1, Calcs  Returned via:  Express Delivery	Attached are1 copies of	of shop drawings as follows:		\$
Fabricator / Manufacturer:  Date received:  Commins Manufacturing, Inc.  08/06/2018  Reviewed as checked below:  Reviewed as noted  Contains items not reviewed  Revise & resubmit  Submit add'l/specified items  ATS10, ATS11 Sh1, ATS11 Sh2, ATS12, RL-1, Calcs	Submittal No.:	03	-	
Date received: 08/06/2018  Reviewed as checked below:  ☑ Reviewed as noted □ Contains items not reviewed □ Revise & resubmit □ Submit add'l/specified items  Sheet numbers reviewed: ATS10, ATS11 Sh1, ATS11 Sh2, ATS12, RL-1, Calcs	Submitted item:	Auto Tight Tie Down	-	
Reviewed as checked below:  I Reviewed as noted	Fabricator / Manufacturer:	Commins Manufacturing, Inc.	-	
☐ Reviewed as noted ☐ Contains items not reviewed ☐ Revise & resubmit ☐ Submit add'l/specified items ☐ ATS10, ATS11 Sh1, ATS11 Sh2, ATS12, RL-1, Calcs	Date received:	08/06/2018	-	
□ Revise & resubmit □ Submit add'l/specified items  Sheet numbers reviewed: ATS10, ATS11 Sh1, ATS11 Sh2, ATS12, RL-1, Calcs	Reviewed as checked below:			
Sheet numbers reviewed: ATS10, ATS11 Sh1, ATS11 Sh2, ATS12, RL-1, Calcs	⊠ Reviewed as noted	□ Contains items not reviewed		
	☐ Revise & resubmit	☐ Submit add'l/specified items		
Returned via:   E-mail 40 pages incl. trans  Messenger   Mail Express Delivery	Sheet numbers reviewed:	ATS10, ATS11 Sh1, ATS11 Sh	2, ATS12, RL-1, Calcs	
	Returned via:   E-mail 4	0 pages incl. trans	enger 🗅 Mail	☐ Express Delivery

### Remarks:

☑ No Exception Taken	☐ Make Corrections Noted
☐ Submit Additional/	☐ Revise and

Specified Items

Checking by WDY is only for general

conformance with the design concept of the project and general compliance with the information given in the contract documents. Any action shown is subject to the requirements of the plans and specifications. The general contractor is responsible for: Dimensions which shall be confirmed at the jobsite; fabrication processes and techniques of construction; coordination of his work with that of all other trades; and the satisfactory performance of his work.

WDY, Inc.

Date: 08-06-2018

By: Brynn Adkins



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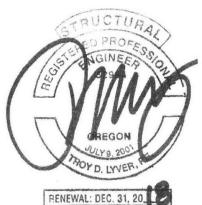
## AutoTight® Rod Holdown System

# System Design for **Tree Farm**



### LYVER ENGINEERING AND DESIGN

7950 SE 106th, Portland, Oregon 97266
Ph: 503.705.5283 Fax: 503.482.7449 TroyL@Lyver-EAD.com www.Lyver-EAD.com



Prepared for **ProTeck** 

prepared by Tom Boydston Commins Project ID # 18-1789

Includes ICC ES 1344 Code Report, http://www.icc-es.org/reports/pdf\_files/ICC-ES/ESR-1344.pdf#view=fit and applicable catalog pages.

Engineering Calculations Revision: 0 AutoDesign Revision: 2 Eng

Calcs Date 06/13/2018



CAT ID # ##-####

### (1) Key to Calculation Table

### THIS PAGE SAMPLE RUN ONLY

AutoTight® System Run Design Calc. Sheet for: Engineering Calcs Revision: 1

**Project Name** 

Plan Set: BID SET Plan Set Date: mm/dd/yyyy

Run Name:	1	Run Qty:	4		Te	nsile Streng	gth	Calc'd
	(7)	(8)	(9)	(10)	(11)	(12)	(13)	74.43
D 0 :6		1		1 7				(14)
Run Specifi		Compo		Description	Capacity	Demand	D/C	Elong.
Required l		Commins A			(kips)	(kips)	Ratio	(in.)
Level =	2	Compo	nent	Description	Capacity	Demand	D/C	Elong.
Differential Load:	4.00 (kips)	AT 1	25	Shrinkage at Level, Shrinkage Device travel & D/C Ratio (in.)	1.10	0.50	45.5%	-
Tension Load:	20.00 (kips)	AT 1	25	Shrinkage Device (1-1/4" I.D.) - Allowable Load	34.50	4.00	11.6%	
Compression:	20.00 (kips)	-		Shrinkage Device - Deflection at Load	-	-	-	0.002
Story Height:	12.50 (ft.)	-		Shrinkage Device - Travel and Seating Increment ΔR	-	-		0.002
Plate Height:	11.33 (ft.)	S8I	L	Bearing Plate at Reaction Point	7.96	4.00	50.2%	0.020
Floor Depth:	14.00 (in.)	RS	)	1-1/8"-A307 Tension Rod	22.37	20.00	89.4%	0.125
		-		No Stretch Rod	#N/A	20.00	0.0%	n/a
		-		Wood Beam Start Bearing Plate	n/a	n/a	0.00	n/a
		-		Steel Beam Start in Tension	n/a	n/a	0.00	n/a
			Limit	ing Component Tension Load Capacity, Load and D/C Ratio	22.37	20.00	89.4%	-
		Maxim	um Allo	wed Level Elongation, D/C Ratio and Total Level Elongation	0,200	-	74.5%	0.149
Compression	Outer (1) 4x8	3 (1) 4x8 I	nner	4x Wall Post per Side of Rod-Enter by Hand as Needed	32.08	20.00	62.3%	-
Wood	Posts (3) 2x6	6 (3) 2x6 F	Posts	6x Wall Post per Side of Rod-Enter by Hand as Needed	30.93	20.00	64.7%	-
Level =	Footing	Compo	nent	Description	Capacity	Demand	D/C	Elong.
Tension Load:	20.00 (kips)	RS	)	1-1/8"-A307 Anchor Rod	22.37	20.00	89.4%	n/a

- All these cells are filled with data from the AutoTight Run Designer spreadsheet's Project Info page and Load Justification Table page.
- The Builder's Name of the project.
- The revision level of the plan set.
- The Bid Date.
- The Commins Mfg. project number. The Builder's number for the project.
- The name of this run.

Project Number:

- Commins AutoTight part number. The quantity of this type of run.
- This column is the description of the component shown on each row
- This column of the table is the Load Capacities of the various components. This column of the table is the Load placed on the various components.
- This column of the table is the Demand / Capacity ratio for each component.
- (14) This column is the contribution of each componenent to the total elongation for this level, and the total elongation for the level.
- Elongation numbers are in blue text.
- The name of this level. (16) Differential Load applied by this level.
- Total tension in rod at this level.
- (18) Compression load on the compression posts at this level.
- (19) Story Height carpet to carpet
- Top of Sill Plate to Top of Sill Plate height of this level.
- (21) Depth of floor beams
- (22) This row compares the total shrinkage at this level with the capacity of the AT's to take up this shrinkage.
- This row compares the load capacity of the AT device to the load applied to it. Per AC316 Sec. 1.4.5
- [24] This row shows the deflection of the AT device(s) under the applied load. Per AC316 Sec. 1.4.8 [25] This row shows the  $\Delta R$ =Travel and Seating increment of the AT Device(s). Per AC316 Sec. 1.4.7
- This row shows Bearing Plate Load Capacity and compares to its Load also its deflection's contribution to the total Elongation
- (unless the calcs call for rod stretch only.) (It sees only the differential load.) Per AF&PA NDS Tbl 4A, 4B incl Cf factor.

  [27] This row shows Tension Rod Load Capacity and compares to its Load, also its deflection's contribution to the total Elongation, Per AISC 360-05
- (28) This row shows Stretch Rod Load Capacity and compares to its Load, also its deflection's contribution to the total Elongation. Only if Stretch Rod is used.
- (29) This row shows the Wood Beam Start's Bearing Plate Load Capacity and compares to its Load, also its deflection's contribution to the total Elongation (Only if a Wood Beam Start is used.) (It sees the tension load.) Per AF&PA-NDS Tbl 4A, 4B incl Cf factor.
- (30) This row shows the Steel Beam Start's Load Capacity and compares to its Load, also its deflection's contribution to the total Elongation.
- (Only if a Steel Beam Start is used.) (It sees the tension load.) The rod seats on the steel beam and the weld cross section is greater than the rod cross section so the Steel Beam Start elongation is included in rod elongation. Per ICC ES-1344 & 5889
- (31) This row shows worst case component's Load and compares to its Load Capacity.
- (32) This row shows the maximum allowed Elongation and the total Elongation calculated for this level
- This row shows the inner and outer compression post required, their load capacities and loads if the wall is 4x. It is used only if Commins Mfg specifies the Compression Posts and is filled in manually. If line is not shown posting is per structural drawing.
- (34) This row shows the inner and outer compression post required, their load capacities and loads if the wall is 6x. It is used only if Commins Mfg specifies the Compression Posts and is filled in manually. If line is not shown posting is per structural drawing.
- (35) This row shows the load capacity of the Anchor Rod embedded in the concrete and compares to its load, if used. (Not the concrete strength) (36) Anchor bolt elongation is included in the length of the tension rods.
- Nuts, Coupler Nuts and Reducing Coupler Nuts are not listed individually because they are grade compatible with the Tension Rod.
- (38) Nuts, Coupler Nuts and Reducing Coupler Nuts calculated contribution to elongation is 0.0005 inch or less.
- (39) Revision level of this document

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0.200

53.41

51.56

51.52

51.52

Take Off Revision: 2 Eng

86.0%

96.5%

99.9%

psi (all grades)

0.172

AutoTight® System Run Design Calc. Sheet for:

Engineering Calcs Revision: 0

Tree Farm

Plan Set Date: 03/23/2018

ermit #					CAT ID#	18-1789	
Run Name:	EW2ab			Te	nsile Streng	gth	Calc'o
Run Specif	fications	Component	Description	Capacity	Demand	D/C	Elong
Required	Loads:	Commins AutoTigh	nt	(kips)	(kips)	Ratio	(in.)
Level =	Level 3	Component	Description	Capacity	Demand	D/C	Elong
Differential Load:	20.30 (kips)	AT10A-1.5	Shrinkage at Level, Shrinkage Device travel & D/C Ratio (in.)	1.63"	0.50"	30.7%	-
Tension Load:	20.30 (kips)	AT10A-1.5	Shrinkage Device (1-1/4" I.D.) - Allowable Load	28.07	20.30	72.3%	-
Compression:	33.80 (kips)	-	Shrinkage Device - Deflection at Load	-	-	-	0.01
Story Height:	13.00 (ft.)	-	Shrinkage Device - Travel and Seating Increment ΔR	-	-	-	0.00
Plate Height:	13.00 (ft.)	L21-1-1/4"	Bearing Plate at Reaction Point	21.03	20.30	96.5%	0.03
		R9A307	1 1/8"-A307 Tension Rod	22.37	20.30	90.7%	0.05
		Lim	iting Component Tension Load Capacity, Load and D/C Ratio	21.03	20.30	96.5%	-
		Maximum All	owed Level Elongation, D/C Ratio and Total Level Elongation	0.200	-	55.0%	0.11
Compression	Outer (2) 2x4	(9) 2x4 Inner	4x Wall Compression Post per Comp Post Calc Sheet	36.09	33.80	93.7%	-
Wood	Posts (2) 2x6	(5) 2x6 Posts	6x Wall Compression Post per Comp Post Calc Sheet	36.09	33.80	93.7%	-
Level =	Level 2	Component	Description	Capacity	Demand	D/C	Elono
Differential Load:	14.21 (kips)	AT12A-1.5	Shrinkage at Level, Shrinkage Device travel & D/C Ratio (in.)	1.63"	0.25"	15.3%	-
Tension Load:	34.51 (kips)	AT12A-1.5	Shrinkage Device (1-1/2" I.D.) - Allowable Load	28.07	14.21	50.6%	-
Compression:	51.52 (kips)	-	Shrinkage Device - Deflection at Load	-	-	-	0.01
Story Height:	13.00 (ft.)	-	Shrinkage Device - Travel and Seating Increment ΔR	-	-	-	0.00
Plate Height:	11.95 (ft.)	L18-1-1/2"	Bearing Plate at Reaction Point	18.92	14.21	75.1%	0.03
Floor Depth:	12.63 (in.)	R12A307	1 1/2"-A307 Tension Rod	39.76	34.51	86.8%	0.13
		Lim	iting Component Tension Load Capacity, Load and D/C Ratio	39.76	34.51	86.8%	-

Level =	Footing	Component	Description	Capacity	Demand	D/C	Elong.
Tension Load:	34.51 (kips)	R12A307	1 1/2"-A307 Anchor Rod	39.76	34.51	86.8%	n/a

4x Wall Compression Post per Comp Post Calc Sheet

6x Wall Compression Post per Comp Post Calc Sheet

Maximum Allowed Level Elongation, D/C Ratio and Total Level Elongation

Design Code: OSSC\_2014 Main/State/Local

Outer (2) 2x4 (21) 2x4 Inner

Posts (2) 2x6 (8) 2x6

Loads per: Include Drawing Date

Loads Type: ASD Steel Stess Increase: No Takeup Device at Each Level: Yes

Elongation Limit Required:

Compression

Wood

Elongation Limit per Connection: 0.200 (inch) between load reaction points.

Elongation Components: System Stretch Includes sum of: Rod, Bearing Plate, Shrinkage Device ΔA & Shrinkage Device ΔR.

Shrinkage: 0.250 inch per floor

Shearwall Plates Wood Species: DFL Douglas Fir-Larch

Shearwall Plate Compression Capacity (Cross Grain): 625 Compression Post Wood Species: DFL Douglas Fir-Larch Compression Post Wood Capacity (Parallel to Grain): 1350

Compression Post Design: per AutoTight

Compression Post Species: per Structural Plans S001

Compression Post Nail Qty: Allowable per 16d Sinker in DFL = 189, Qty nails = 108, Allowable load = 20.41 kips, Total load = 20.30 kips, D/C = 99.5%.

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Take Off Revision: 2 Eng

psi (all grades)

AutoTight® System Run Design Calc. Sheet for: Engineering Calcs Revision: 0

Tree Farm

Plan Set: Plan Check 2

Plan Set Date: 03/23/2018

ermit #	1						CALID#	18-1789	
Run Name:	EW6					Te	ensile Streng	gth	Calc'd
Run Specit	fications		Comp	onent	Description	Capacity	Demand	D/C	Elong
Required	Loads:		Commins	AutoTigl	nt	(kips)	(kips)	Ratio	(in.)
Level =	Level 3		Comp	onent	Description	Capacity	Demand	D/C	Elong
Differential Load:	30.83	(kips)	AT1	6A-2	Shrinkage at Level, Shrinkage Device travel & D/C Ratio (in.)	2.07"	0.50"	24.2%	-
Tension Load:	30.83	(kips)	AT1	6A-2	Shrinkage Device (2" I.D.) - Allowable Load	39.45	30.83	78.1%	-
Compression:	48.54	(kips)		•	Shrinkage Device - Deflection at Load	-	-	-	0.008
Story Height:	13.00	(ft.)		-	Shrinkage Device - Travel and Seating Increment ΔR	-	-	-	0.00
Plate Height:	13.00	(ft.)	L33-	1-1/2"	Bearing Plate at Reaction Point	33.18	30.83	92.9%	0.03
			R12	A307	1 1/2"-A307 Tension Rod	39.76	30.83	77.5%	0.05
				Lim	iting Component Tension Load Capacity, Load and D/C Ratio	33.18	30.83	92.9%	-
			Maxi	mum All	owed Level Elongation, D/C Ratio and Total Level Elongation	0.200	-	52.5%	0.10
Compression	Outer	(2) 2x4	(13) 2x4	Inner	4x Wall Compression Post per Comp Post Calc Sheet	49.22	48.54	98.6%	-
Wood	Posts	(2) 2x6	(8) 2x6	Posts	6x Wall Compression Post per Comp Post Calc Sheet	51.56	48.54	94.1%	-
Level =	Level 2		Comp	onent	Description	Capacity	Demand	D/C	Elong
Differential Load:	18.71	(kips)	AT1	6A-2	Shrinkage at Level, Shrinkage Device travel & D/C Ratio (in.)	2.07"	0.25"	12.1%	-
Tension Load:	49.54	(kips)	AT1	6A-2	Shrinkage Device (2" I.D.) - Allowable Load	39.45	18.71	47.4%	-
Compression:	72.18	(kips)		-	Shrinkage Device - Deflection at Load	-	-	-	0.00
Story Height:	13.00	(ft.)	10	-	Shrinkage Device - Travel and Seating Increment ΔR	-	-	-	0.00
Plate Height:	11.95	(ft.)	L25	5-2"	Bearing Plate at Reaction Point	23.69	18.71	79.0%	0.03
Floor Depth:	12.63	(in.)	R14	A307	1 3/4"-A307 Tension Rod	54.12	49.54	91.5%	0.14
				Lim	iting Component Tension Load Capacity, Load and D/C Ratio	54.12	49.54	91.5%	-:
			Maxi	mum All	owed Level Elongation, D/C Ratio and Total Level Elongation	0.200	-	88.5%	0.17
Compression	Outer	(2) 2x4	(30) 2x4	Inner	4x Wall Compression Post per Comp Post Calc Sheet	74.30	72.18	97.1%	-
Wood	Posts	(2) 2x6	(12) 2x6	Posts	6x Wall Compression Post per Comp Post Calc Sheet	72.18	72.18	100.0%	-
Level =	Footing		Comp	onent	Description	Capacity	Demand	D/C	Elong
Tension Load:	49.54	(kips)	R14.	A307	1 3/4"-A307 Anchor Rod	54.12	49.54	91.5%	n/a

Design Code: OSSC\_2014 Main/State/Local

Loads per:

Include Drawing Date

Loads Type: Steel Stess Increase: ASD

No

Yes

Takeup Device at Each Level: Elongation Limit Required:

Elongation Limit per Connection:

0.200 0.250

**Elongation Components:** 

(inch) between load reaction points. System Stretch Includes sum of: Rod, Bearing Plate, Shrinkage Device ΔA & Shrinkage Device ΔR. inch per floor

Douglas Fir-Larch

Shrinkage: Shearwall Plates Wood Species:

Compression Post Wood Species:

Compression Post Design:

Compression Post Species: Compression Post Nail Qty: DFL DFL

Douglas Fir-Larch per AutoTight

per Structural Plans S001

Allowable per 16d Sinker in DFL = 189, Qty nails = 164, Allowable load = 31.00 kips, Total load = 30.83 kips, D/C = 99.5%.

Shearwall Plate Compression Capacity (Cross Grain):

Compression Post Wood Capacity (Parallel to Grain):

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Take Off Revision: 2 Eng

psi (all grades)

AutoTight® System Run Design Calc. Sheet for: Engineering Calcs Revision: 0

Tree Farm Plan Set: Plan Check 2

Plan Set Date: 03/23/2018

ermit #						CAT ID#	18-1789	
Run Name:	EW6.5				Te	nsile Streng	gth	Calc'
Run Specifi	cations	Compo	nent	Description	Capacity	Demand	D/C	Elong
Required L	_oads:	Commins A	AutoTigh	t	(kips)	(kips)	Ratio	(in.)
Level =	Level 3	Compo	nent	Description	Capacity	Demand	D/C	Elong
Differential Load:	23.16 (kips)	AT10A	-1.5	Shrinkage at Level, Shrinkage Device travel & D/C Ratio (in.)	1.63"	0.50"	30.7%	-
Tension Load:	23.16 (kips)	AT10A	-1.5	Shrinkage Device (1-1/4" I.D.) - Allowable Load	28.07	23.16	82.5%	-
Compression:	26.57 (kips)	<u>-</u>		Shrinkage Device - Deflection at Load	-	-	-	0.01
Story Height:	13.00 (ft.)	-		Shrinkage Device - Travel and Seating Increment ΔR	-	-	-	0.00
Plate Height:	13.00 (ft.)	L25-1-	1/4"	Bearing Plate at Reaction Point	24.94	23.16	92.9%	0.03
		R10A3	307	1 1/4"-A307 Tension Rod	27.61	23.16	83.9%	0.05
			Limi	ting Component Tension Load Capacity, Load and D/C Ratio	24.94	23.16	92.9%	-
		Maxim	um Allo	owed Level Elongation, D/C Ratio and Total Level Elongation	0.200	-	55.5%	0.11
Compression	Outer (2) 2x4	(7) 2x4 II	nner	4x Wall Compression Post per Comp Post Calc Sheet	29.53	26.57	90.0%	-
Wood	Posts (2) 2x6	(4) 2x6 F	osts	6x Wall Compression Post per Comp Post Calc Sheet	30.94	26.57	85.9%	~
Level =	Level 2	Compo	nent	Description	Capacity	Demand	D/C	Elon
Differential Load:	13.07 (kips)	AT12A	-1.5	Shrinkage at Level, Shrinkage Device travel & D/C Ratio (in.)	1.63"	0.25"	15.3%	-
Tension Load:	36.23 (kips)	AT12A	-1.5	Shrinkage Device (1-1/2" I.D.) - Allowable Load	28.07	13.07	46.6%	-
Compression:	40.50 (kips)	-		Shrinkage Device - Deflection at Load	-	-	-	0.00
Story Height:	13.00 (ft.)	-		Shrinkage Device - Travel and Seating Increment ΔR	-	-	-	0.00
Plate Height:	11.95 (ft.)	L18-1-	1/2"	Bearing Plate at Reaction Point	18.92	13.07	69.1%	0.02
Floor Depth:	12.63 (in.)	R12A	307	1 1/2"-A307 Tension Rod	39.76	36.23	91.1%	0.13
			Limi	ting Component Tension Load Capacity, Load and D/C Ratio	39.76	36.23	91.1%	-
		Maxim		owed Level Elongation, D/C Ratio and Total Level Elongation	0.200	-	88.0%	0.17
Compression	Outer (2) 2x4		nner	4x Wall Compression Post per Comp Post Calc Sheet	41.80	40.50	96.9%	-
Wood	Posts (2) 2x6		osts	6x Wall Compression Post per Comp Post Calc Sheet	41.25	40.50	98.2%	-
	Footing	Compo		Description	Capacity	Demand	D/C	Flon

R12A307 Design Code: OSSC\_2014 Main/State/Local

Loads per: Include Drawing Date Loads Type: ASD

Steel Stess Increase: No Takeup Device at Each Level: Yes Elongation Limit Required: Yes

Tension Load: 36.23 (kips)

Elongation Limit per Connection: 0.200 (inch) between load reaction points.

**Elongation Components:** System Stretch Includes sum of: Rod, Bearing Plate, Shrinkage Device ΔA & Shrinkage Device ΔR.

1 1/2"-A307 Anchor Rod

Shrinkage: 0.250 inch per floor

Shearwall Plates Wood Species: Douglas Fir-Larch Shearwall Plate Compression Capacity (Cross Grain): Compression Post Wood Species: DFL Douglas Fir-Larch

Compression Post Wood Capacity (Parallel to Grain):

Compression Post Design: per AutoTight

Compression Post Species: per Structural Plans S001

Allowable per 16d Sinker in DFL = 189, Qty nails = 124, Allowable load = 23.44 kips, Total load = 23.16 kips, D/C = 98.8%. Compression Post Nail Qty:

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Take Off Revision: 2 Eng

AutoTight® System Run Design Calc. Sheet for:

Engineering Calcs Revision: 0

**Tree Farm** 

Plan Set: Plan Check 2 Plan Set Date: 03/23/2018

ermit #							CAT ID#	18-1789	
Run Name:	NSB1					Te	nsile Streng	gth	Calc'd
Run Specif	ications		Comp	onent	Description	Capacity	Demand	D/C	Elong.
Required	Loads:		Commins AutoTight			(kips)	(kips)	Ratio	(in.)
Level =	Level = Level 3		Comp	onent	Description	Capacity	Demand	D/C	Elong.
Differential Load:	38.82	(kips)	AT1	6A-2	Shrinkage at Level, Shrinkage Device travel & D/C Ratio (in.)	2.07"	0.50"	24.2%	-
Tension Load:	38.82	(kips)	AT1	6A-2	Shrinkage Device (2" I.D.) - Allowable Load	39.45	38.82	98.4%	-
Compression:	38.82	(kips)		-	Shrinkage Device - Deflection at Load	-	-	-	0.010
Story Height:	13.00	(ft.)		-	Shrinkage Device - Travel and Seating Increment ΔR	-	-	-	0.001
Plate Height:	13.00	(ft.)	L40-	1-1/2"	Bearing Plate at Reaction Point	40.05	38.82	96.9%	0.039
			R12	A307	1 1/2"-A307 Tension Rod	39.76	38.82	97.6%	0.079
				Limi	ting Component Tension Load Capacity, Load and D/C Ratio	39.45	38.82	98.4%	-
			Maxi	mum Allo	wed Level Elongation, D/C Ratio and Total Level Elongation	0.200	-	64.0%	0.128
Compression	Outer	(2) 2x4	(10) 2x4	Inner	4x Wall Compression Post per Comp Post Calc Sheet	39.37	38.82	98.6%	
Wood	Posts	(2) 2x6	(6) 2x6	Posts	6x Wall Compression Post per Comp Post Calc Sheet	41.25	38.82	94.1%	-

Level =	Level 2		Comp	onent	Description	Capacity	Demand	D/C	Elong.
Differential Load:	0.70	(kips)	AT12	A-1.5	Shrinkage at Level, Shrinkage Device travel & D/C Ratio (in.)	1.63"	0.25"	15.3%	-
Tension Load:	39.52	(kips)	AT12	A-1.5	Shrinkage Device (1-1/2" I.D.) - Allowable Load	28.07	0.70	2.5%	
Compression:	43.29	(kips)		- Shrinkage Device - Deflection at Load		-	-	-	0.000
Story Height:	13.00	(ft.)		- Shrinkage Device - Travel and Seating Increment ΔR		-	-	-	0.000
Plate Height:	11.95	(ft.)	L18-	I-1/2"	Bearing Plate at Reaction Point	18.92	0.70	3.7%	0.001
Floor Depth:	12.63	(in.)	R12	4307	1 1/2"-A307 Tension Rod	39.76	39.52	99.4%	0.151
				Limiti	ing Component Tension Load Capacity, Load and D/C Ratio	39.76	39.52	99.4%	~
			Maxi	num Allo	wed Level Elongation, D/C Ratio and Total Level Elongation	0.200	-	76.5%	0.153
Compression	Outer	(2) 2x4	(17) 2x4	Inner	4x Wall Compression Post per Comp Post Calc Sheet	44.12	43.29	98.1%	-
Wood	Posts	(2) 2x6	(7) 2x6			46.40	43.29	93.3%	-

Level =	Footing	Component	Description	Capacity	Demand	D/C	Elong.
Tension Load:	39.52 (kips)	R12A307	1 1/2"-A307 Anchor Rod	39.76	39.52	99.4%	n/a

Design Code: OSSC\_2014 Main/State/Local

Include Drawing Date Loads per:

Loads Type: ASD No Yes Steel Stess Increase: Takeup Device at Each Level:

Elongation Limit Required: Yes Elongation Limit per Connection: 0.200 (inch) between load reaction points.

Elongation Components: System Stretch Includes sum of: Rod, Bearing Plate, Shrinkage Device  $\Delta A$  & Shrinkage Device  $\Delta R$ .

Shrinkage: 0.250 inch per floor

Shearwall Plates Wood Species: DFL Douglas Fir-Larch Shearwall Plate Compression Capacity (Cross Grain): 625 psi (all grades)

Compression Post Wood Species: Douglas Fir-Larch Compression Post Wood Capacity (Parallel to Grain): 1350

Compression Post Design: per AutoTight

Compression Post Species: per Structural Plans S001

Compression Post Nail Qty: Allowable per 16d Sinker in DFL = 189, Qty nails = 206, Allowable load = 38.93 kips, Total load = 38.82 kips, D/C = 99.7%.

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0.200

91.0%

Take Off Revision: 2 Eng

0.182

AutoTight® System Run Design Calc. Sheet for:

Engineering Calcs Revision: 0

Tree Farm

Plan Set: Plan Check 2

Plan Set Date: 03/23/2018

ermit #					CAT ID#	18-1789	
Run Name:	NSB2			Te	nsile Streng	gth	Calc'd
Run Specif Required		Component Commins AutoTigh	Description	Capacity (kips)	Demand (kips)	D/C Ratio	Elong (in.)
	Level 3	Component	Description	Capacity	Demand	D/C	Elong
Differential Load:		AT16A-2	Shrinkage at Level, Shrinkage Device travel & D/C Ratio (in.)	2.07"	0.50"	24.2%	-
Tension Load:	38.82 (kips)	AT16A-2	Shrinkage Device (2" I.D.) - Allowable Load	39.45	38.82	98.4%	-
Compression:	41.58 (kips)	-	Shrinkage Device - Deflection at Load	-	-	-	0.010
Story Height:	13.00 (ft.)	-	Shrinkage Device - Travel and Seating Increment ΔR	-	-	-	0.00
Plate Height:	13.00 (ft.)	L40-1-1/2"	Bearing Plate at Reaction Point	40.05	38.82	96.9%	0.03
		R12A307	1 1/2"-A307 Tension Rod	39.76	38.82	97.6%	0.07
		Limi	ting Component Tension Load Capacity, Load and D/C Ratio	39.45	38.82	98.4%	-
		Maximum Alle	owed Level Elongation, D/C Ratio and Total Level Elongation	0.200	-	62.0%	0.12
Compression	Outer (2) 2x4	(11) 2x4 Inner	4x Wall Compression Post per Comp Post Calc Sheet	42.65	41.58	97.5%	-
Wood	Posts (2) 2x6	(7) 2x6 Posts	6x Wall Compression Post per Comp Post Calc Sheet	46.40	41.58	89.6%	-
Level =	Level 2	Component	Description	Capacity	Demand	D/C	Elong
Differential Load:	13.49 (kips)	AT16A-2	Shrinkage at Level, Shrinkage Device travel & D/C Ratio (in.)	2.07"	0.25"	12.1%	-
Tension Load:	52.31 (kips)	AT16A-2	Shrinkage Device (2" I.D.) - Allowable Load	39.45	13.49	34.2%	-
Compression:	55.91 (kips)	-	Shrinkage Device - Deflection at Load	-	-	-	0.00
Story Height:	: 13.00 (ft.)	-	Shrinkage Device - Travel and Seating Increment ΔR	-	-	-	0.00
Plate Height:	: 11.95 (ft.)	L18-2"	Bearing Plate at Reaction Point	17.96	13.49	75.1%	0.03
Floor Depth:	12.63 (in.)	R14A307	1 3/4"-A307 Tension Rod	54.12	52.31	96.7%	0.14
		Limi	ting Component Tension Load Capacity, Load and D/C Ratio	54.12	52.31	96.7%	-

Compression	Outer (2) 2x4	(23) 2x4 Inner	4x Wall Compression Post per Comp Post Calc Sheet	58.05	55.91	96.3%	~
Wood	Posts (2) 2x6	(9) 2x6 Posts	6x Wall Compression Post per Comp Post Calc Sheet	56.72	55.91	98.6%	-
Level =	Footing	Component	Description	Capacity	Demand	D/C	Elong.

Maximum Allowed Level Elongation, D/C Ratio and Total Level Elongation

Design Code: OSSC\_2014 Main/State/Local

Include Drawing Date Loads per: ASD

Loads Type: Steel Stess Increase: No Takeup Device at Each Level: Yes

Elongation Limit Required: Yes

Elongation Limit per Connection: 0.200 (inch) between load reaction points.

**Elongation Components:** System Stretch Includes sum of: Rod, Bearing Plate, Shrinkage Device ΔA & Shrinkage Device ΔR.

Shrinkage: 0.250

inch per floor Shearwall Plates Wood Species:

Douglas Fir-Larch Shearwall Plate Compression Capacity (Cross Grain): psi (all grades) Compression Post Wood Species: Douglas Fir-Larch Compression Post Wood Capacity (Parallel to Grain):

Compression Post Design: per AutoTight

Compression Post Species: per Structural Plans S001

Compression Post Nail Qty: Allowable per 16d Sinker in DFL = 189, Qty nails = 206, Allowable load = 38.93 kips, Total load = 38.82 kips, D/C = 99.7%.

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AutoTight® System Run Design Calc. Sheet for: Engineering Calcs Revision: 0

Tree Farm

Plan Set: Plan Check 2

Plan Set Date: 03/23/2018

Permit #						CAT ID#	18-1789	
Run Name:	NSC1				Te	nsile Stren	gth	Calc'd
Run Spec	ifications	Compor	nent	Description	Capacity	Demand	D/C	Elong
Required	Loads:	Commins A	utoTight		(kips)	(kips)	Ratio	(in.)
Level:	= Level 3	Component		Description	Capacity	Demand	D/C	Elong
Differential Load	l: 25.13 (kips)	AT10A-	-1.5	Shrinkage at Level, Shrinkage Device travel & D/C Ratio (in.)	1.63"	0.50"	30.7%	-
Tension Load	1: 25.13 (kips)	AT10A	-1.5	Shrinkage Device (1-1/4" I.D.) - Allowable Load	28.07	25.13	89.5%	-
Compression	: 26.95 (kips)	-		Shrinkage Device - Deflection at Load	-	-	-	0.01
Story Height	t: 13.00 (ft.)	-		Shrinkage Device - Travel and Seating Increment ΔR	-	-	-	0.00
Plate Height	t: 13.00 (ft.)	L28-1-	1/4"	Bearing Plate at Reaction Point	27.28	25.13	92.1%	0.03
		R10A3	307	1 1/4"-A307 Tension Rod	27.61	25.13	91.0%	0.06
			Limiti	ing Component Tension Load Capacity, Load and D/C Ratio	27.28	25.13	92.1%	-
		Maxim	um Allov	wed Level Elongation, D/C Ratio and Total Level Elongation	0.200	-	58.5%	0.11
Compression	Outer (2) 2x4	(7) 2x4 Ir	nner	4x Wall Compression Post per Comp Post Calc Sheet	29.53	26.95	91.3%	-
Wood	Posts (2) 2x6	(4) 2x6 P	osts	6x Wall Compression Post per Comp Post Calc Sheet	30.94	26.95	87.1%	-

Level =	Level 2		Comp	onent	Description	Capacity	Demand	D/C	Elong.
Differential Load:	13.67	(kips)	AT12	2A-1.5	Shrinkage at Level, Shrinkage Device travel & D/C Ratio (in.)	1.63"	0.25"	15.3%	-
Tension Load:	38.80	(kips)			Shrinkage Device (1-1/2" I.D.) - Allowable Load	28.07	13.67	48.7%	-
Compression:	1 / /		-	Shrinkage Device - Deflection at Load	-	-	-	0.010	
Story Height:	y Height: 13.00 (ft.) -		-	Shrinkage Device - Travel and Seating Increment ΔR	-	-	-	0.000	
Plate Height:	t: 11.95 (ft.) L18-1-1/2"		1-1/2"	Bearing Plate at Reaction Point	18.92	13.67	72.3%	0.029	
Floor Depth:	12.63	(in.)	R12	A307	1 1/2"-A307 Tension Rod	39.76	38.80	97.6%	0.149
				Limiti	ing Component Tension Load Capacity, Load and D/C Ratio	39.76	38.80	97.6%	~
			Maxi	mum Allo	wed Level Elongation, D/C Ratio and Total Level Elongation	0.200	-	93.5%	0.187
Compression	Compression Outer (2) 2x4 (16) 2x4 Inner 4x Wall		4x Wall Compression Post per Comp Post Calc Sheet	41.80	41.07	98.3%	-		
Wood	Posts	osts (2) 2x6 (6) 2x6 Posts 6x Wall Compression Post per Comp Post Calc Sheet		41.25	41.07	99.6%	-		

Level =	Footing	Component	Description	Capacity	Demand	D/C	Elong.
Tension Load:	38.80 (kips)	R12A307	1 1/2"-A307 Anchor Rod	39.76	38.80	97.6%	n/a
	\\\						

Design Code: OSSC\_2014 Main/State/Local

Loads per:

Include Drawing Date

Loads Type: ASD

Steel Stess Increase:

Takeup Device at Each Level: Yes

Yes

Elongation Limit Required:

Elongation Limit per Connection:

Elongation Components: System Stretch

0.200 (inch) between load reaction points.

Shrinkage:

0.250 inch per floor DFL Douglas Fir-Larch

Shearwall Plates Wood Species: Compression Post Wood Species: DFL Douglas Fir-Larch

per AutoTight

Compression Post Species:
Compression Post Species:

Compression Post Nail Qty:

per Structural Plans S001

Includes sum of: Rod, Bearing Plate, Shrinkage Device ΔA & Shrinkage Device ΔR.

Shearwall Plate Compression Capacity (Cross Grain): Compression Post Wood Capacity (Parallel to Grain):

psi (all grades)

Take Off Revision: 2 Eng

1350

Allowable per 16d Sinker in DFL = 189, Qty nails = 134, Allowable load = 25.33 kips, Total load = 25.13 kips, D/C = 99.2%.

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Take Off Revision: 2 Eng

psi (all grades)

AutoTight® System Run Design Calc. Sheet for:

Engineering Calcs Revision: 0

Tree Farm

Plan Set: Plan Check 2

Plan Set Date: 03/23/2018

ermit #					CAT ID#	18-1789	
Run Name:	NSC2			Te	nsile Stren	gth	Calc'd
Run Specif Required		Compone Commins Au	· ·	Capacity (kips)	Demand (kips)	D/C Ratio	Elong (in.)
Level =	Level 3	Compone	t Description	Capacity	Demand	D/C	Elong
Differential Load:	21.80 (kips)	AT10A-1	Shrinkage at Level, Shrinkage Device travel & D/C Ratio (in.)	1.63"	0.50"	30.7%	-
Tension Load:	21.80 (kips)	AT10A-1	Shrinkage Device (1-1/4" I.D.) - Allowable Load	28.07	21.80	77.7%	-
Compression:	24.55 (kips)	-	Shrinkage Device - Deflection at Load	-	-	-	0.01
Story Height:	13.00 (ft.)	-	Shrinkage Device - Travel and Seating Increment ΔR	-	-	-	0.00
Plate Height:	13.00 (ft.)	L25-1-1/	Bearing Plate at Reaction Point	24.94	21.80	87.4%	0.03
		R9A30	1 1/8"-A307 Tension Rod	22.37	21.80	97.5%	0.06
			imiting Component Tension Load Capacity, Load and D/C Ratio	22.37	21.80	97.5%	-
		Maximu	Allowed Level Elongation, D/C Ratio and Total Level Elongation		-	56.0%	0.11
Compression	Outer (2) 2x4	(6) 2x4 Inn	4x Wall Compression Post per Comp Post Calc Sheet	26.25	24.55	93.5%	-
Wood	Posts (2) 2x6	(3) 2x6 Po	6x Wall Compression Post per Comp Post Calc Sheet	25.78	24.55	95.2%	-
Level =	Level 2	Compone	t Description	Capacity	Demand	D/C	Elong
Differential Load:	12.19 (kips)	AT12A-1	Shrinkage at Level, Shrinkage Device travel & D/C Ratio (in.)	1.63"	0.25"	15.3%	-
Tension Load:	33.99 (kips)	AT12A-1	Shrinkage Device (1-1/2" I.D.) - Allowable Load	28.07	12.19	43.4%	-
Compression:	37.42 (kips)	-	Shrinkage Device - Deflection at Load	-	-	-	0.00
Story Height:		-	Shrinkage Device - Travel and Seating Increment ΔR	-	-	-	0.00
Plate Height:	11.95 (ft.)	L18-1-1/	Bearing Plate at Reaction Point	18.92	12.19	64.4%	0.02
Floor Depth:		R12A30		39.76	33.99	85.5%	0.13
,			imiting Component Tension Load Capacity, Load and D/C Ratio	39.76	33.99	85.5%	-
	L	Maximu	Allowed Level Elongation, D/C Ratio and Total Level Elongation	0.200	-	82.5%	0.16
Compression	Outer (2) 2x4			39.47	37.42	94.8%	-

Level =	Footing	Component		Description	Capacity	Demand	D/C	Elong.
Tension Load:	33.99 (kips)	R12A307	1 1/2"-A307 Anchor Rod		39.76	33.99	85.5%	n/a

6x Wall Compression Post per Comp Post Calc Sheet

Design Code: OSSC\_2014 Main/State/Local

Loads per: Include Drawing Date

Posts (2) 2x6 (6) 2x6 Posts

Loads Type: ASD
Steel Stess Increase: No
Takeup Device at Each Level: Yes

Elongation Limit Required: Yes
Elongation Limit per Connection: 0.200 (inch) between load reaction points.

Elongation Components: System Stretch Includes sum of: Rod, Bearing Plate, Shrinkage Device  $\Delta A$  & Shrinkage Device  $\Delta R$ .

Shearwall Plates Wood Species: DFL Douglas Fir-Larch Shearwall Plate Compression Capacity (Cross Grain):

Compression Post Wood Species: DFL Douglas Fir-Larch Compression Post Wood Capacity (Parallel to Grain): 1350

Compression Post Design: per AutoTight

Compression Post Species: per Structural Plans S001

Compression Post Nail Qty: Allowable per 16d Sinker in DFL = 189, Qty nails = 116, Allowable load = 21.92 kips, Total load = 21.80 kips, D/C = 99.4%.

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AutoTight® System Run Design Calc. Sheet for: Engineering Calcs Revision: 0

Tree Farm Plan Set: Plan Check 2

Plan Set Date: 03/23/2018

ermit #					CAT ID#	18-1789	
Run Name:	NSD			Te	nsile Stren	gth	Calc'd
Run Specif	fications	Component	Description	Capacity	Demand	D/C	Elono
Required	Loads:	Commins AutoTight		(kips) (kips) Ratio		(in.)	
Level =	Level 2	Component	Description	Capacity	Demand	D/C	Elong
Differential Load:	26.90 (kips)	AT10A-1.5	Shrinkage at Level, Shrinkage Device travel & D/C Ratio (in.)	1.63"	0.25"	15.3%	-
Tension Load:	26.90 (kips)	AT10A-1.5	Shrinkage Device (1-1/4" I.D.) - Allowable Load	28.07	26.90	95.8%	-
Compression:	31.19 (kips)	-	Shrinkage Device - Deflection at Load	-	-	-	0.01
Story Height:	13.00 (ft.)	-	Shrinkage Device - Travel and Seating Increment ΔR	-	-	-	0.00
Plate Height:	11.95 (ft.)	L28-1-1/4"	Bearing Plate at Reaction Point	27.28	26.90	98.6%	0.03
Floor Depth:	12.63 (in.)	R10A307	1 1/4"-A307 Tension Rod	27.61	26.90	97.4%	0.07
		Limit	ing Component Tension Load Capacity, Load and D/C Ratio	27.28	26.90	98.6%	-
		Maximum Allo	wed Level Elongation, D/C Ratio and Total Level Elongation	0.200	-	65.5%	0.13
Compression	Outer (2) 2x4	(8) 2x4 Inner	4x Wall Compression Post per Comp Post Calc Sheet	32.81	31.19	95.1%	-
Wood	Posts (2) 2x6	(5) 2x6 Posts	6x Wall Compression Post per Comp Post Calc Sheet	36.09	31.19	86.4%	-

Level =	Footing	Component	Description	Capacity	Demand	D/C	Elong.
Tension Load:	26.90 (kips)	R10A307	1 1/4"-A307 Anchor Rod	27.61	26.90	97.4%	n/a

Design Code: OSSC\_2014 Main/State/Local Include Drawing Date

Loads per: Loads Type:

ASD

Steel Stess Increase: Takeup Device at Each Level:

No

Yes

Elongation Limit Required: Elongation Limit per Connection:

(inch) between load reaction points.

0.200 Elongation Components:

Includes sum of: Rod, Bearing Plate, Shrinkage Device  $\Delta A$  & Shrinkage Device  $\Delta R$ .

System Stretch Shrinkage: 0.250 inch per floor

DFL Douglas Fir-Larch DFL Douglas Fir-Larch

Shearwall Plate Compression Capacity (Cross Grain):

625 psi (all grades)

Take Off Revision: 2 Eng

Compression Post Wood Capacity (Parallel to Grain): 1350 psi

Compression Post Wood Species: Compression Post Design: per AutoTight

Compression Post Species:

Shearwall Plates Wood Species:

per Structural Plans S001

Compression Post Nail Qty: Allowable per 16d Sinker in DFL = 189, Qty nails = 144, Allowable load = 27.22 kips, Total load = 26.90 kips, D/C = 98.8%.

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54.12 46.96 86.8%

Take Off Revision: 2 Eng

AutoTight® System Run Design Calc. Sheet for:

Engineering Calcs Revision: 0

Tree Farm Plan Set: Plan Check 2 Plan Set Date: 03/23/2018

ermit #					CAT ID#	18-1789	
Run Name:	NSE			Te	nsile Streng	gth	Calc'
Run Specif Required		Component Commins AutoTigl	Description ht	Capacity (kips)	Demand (kips)	D/C Ratio	Elong (in.)
Level =	Level 3	Component	Description	Capacity	Demand	D/C	Elong
Differential Load:	28.63 (kips)	AT16A-2	Shrinkage at Level, Shrinkage Device travel & D/C Ratio (in.)	2.07"	0.50"	24.2%	-
Tension Load:	28.63 (kips)	AT16A-2	Shrinkage Device (2" I.D.) - Allowable Load	39.45	28.63	72.6%	-
Compression:	57.55 (kips)	-	Shrinkage Device - Deflection at Load	-	-	-	0.00
Story Height:	13.00 (ft.)	-	Shrinkage Device - Travel and Seating Increment ΔR	-	-	-	0.00
Plate Height:	13.00 (ft.)	L30-1-1/2"	Bearing Plate at Reaction Point	29.74	28.63	96.3%	0.03
		R12A307	1 1/2"-A307 Tension Rod	39.76	28.63	72.0%	0.05
		Lim	iting Component Tension Load Capacity, Load and D/C Ratio	29.74	28.63	96.3%	-
		Maximum All	owed Level Elongation, D/C Ratio and Total Level Elongation	0.200	-	50.5%	0.10
Compression	Outer (2) 2x4	(16) 2x4 Inner	4x Wall Compression Post per Comp Post Calc Sheet	59.06	57.55	97.4%	-
Wood	Posts (2) 2x6	(10) 2x6 Posts	6x Wall Compression Post per Comp Post Calc Sheet	61.87	57.55	93.0%	-
vvoou	1 10313 (2) 210	(10) 200 1-0313	ox vvali compression i est per comp i est cale chect	01.07	01.00	93.076	
	1.evel 2	Component	Description	Capacity	Demand	D/C	Elon
Level =	Level 2	Component	Description	Capacity	Demand	D/C	
Level = Differential Load:	1.evel 2 18.33 (kips)	Component AT16A-2	Description Shrinkage at Level, Shrinkage Device travel & D/C Ratio (in.)	Capacity 2.07"	Demand 0.25"	D/C 12.1%	
Level = Differential Load: Tension Load:	1.evel 2 18.33 (kips) 46.96 (kips)	Component AT16A-2	Description Shrinkage at Level, Shrinkage Device travel & D/C Ratio (in.) Shrinkage Device (2" I.D.) - Allowable Load	Capacity 2.07" 39.45	Demand 0.25"	D/C 12.1%	Elon - - 0.00
Level = Differential Load: Tension Load: Compression:	1.evel 2 18.33 (kips) 46.96 (kips) 83.50 (kips)	Component AT16A-2	Description  Shrinkage at Level, Shrinkage Device travel & D/C Ratio (in.)  Shrinkage Device (2" I.D.) - Allowable Load  Shrinkage Device - Deflection at Load	2.07" 39.45	Demand 0.25" 18.33	D/C 12.1% 46.5%	Elon - - 0.00
Level = Differential Load: Tension Load: Compression: Story Height:	1.evel 2 18.33 (kips) 46.96 (kips) 83.50 (kips) 13.00 (ft.)	Component AT16A-2 AT16A-2	Description  Shrinkage at Level, Shrinkage Device travel & D/C Ratio (in.)  Shrinkage Device (2" I.D.) - Allowable Load  Shrinkage Device - Deflection at Load  Shrinkage Device - Travel and Seating Increment ΔR	Capacity 2.07" 39.45	Demand 0.25" 18.33	D/C 12.1% 46.5% -	- 0.00 0.00 0.04
Level = Differential Load: Tension Load: Compression: Story Height: Plate Height:	1.evel 2 18.33 (kips) 46.96 (kips) 83.50 (kips) 13.00 (ft.) 11.95 (ft.)	Component AT16A-2 AT16A-2	Description  Shrinkage at Level, Shrinkage Device travel & D/C Ratio (in.)  Shrinkage Device (2" I.D.) - Allowable Load  Shrinkage Device - Deflection at Load  Shrinkage Device - Travel and Seating Increment ΔR  Bearing Plate at Reaction Point	Capacity 2.07" 39.45 - - 18.54 54.12	Demand 0.25" 18.33 - - 18.33	D/C 12.1% 46.5% - - 98.9%	Elon -
Level = Differential Load: Tension Load: Compression: Story Height: Plate Height:	1.evel 2 18.33 (kips) 46.96 (kips) 83.50 (kips) 13.00 (ft.) 11.95 (ft.)	Component AT16A-2 AT16A-2 L20-2" R14A307	Description  Shrinkage at Level, Shrinkage Device travel & D/C Ratio (in.)  Shrinkage Device (2" I.D.) - Allowable Load  Shrinkage Device - Deflection at Load  Shrinkage Device - Travel and Seating Increment ΔR  Bearing Plate at Reaction Point  1 3/4"-A307 Tension Rod	Capacity 2.07" 39.45 - - 18.54 54.12	Demand 0.25" 18.33 - - 18.33 46.96	D/C 12.1% 46.5% - - 98.9% 86.8%	0.00 0.00 0.04
Level = Differential Load: Tension Load: Compression: Story Height: Plate Height:	1.evel 2 18.33 (kips) 46.96 (kips) 83.50 (kips) 13.00 (ft.) 11.95 (ft.)	Component AT16A-2 AT16A-2	Description  Shrinkage at Level, Shrinkage Device travel & D/C Ratio (in.) Shrinkage Device (2" I.D.) - Allowable Load Shrinkage Device - Deflection at Load Shrinkage Device - Travel and Seating Increment ΔR Bearing Plate at Reaction Point 1 3/4"-A307 Tension Rod iting Component Tension Load Capacity, Load and D/C Ratio	Capacity 2.07" 39.45 - - 18.54 54.12 18.54	Demand 0.25" 18.33 - - 18.33 46.96 18.33	D/C 12.1% 46.5% - - 98.9% 86.8% 98.9%	0.00 0.00 0.04 0.13

R14A307 Design Code: OSSC\_2014 Main/State/Local

Include Drawing Date Loads per:

Loads Type: ASD Steel Stess Increase: No Takeup Device at Each Level: Yes

Tension Load: 46.96 (kips)

Elongation Limit Required:

Elongation Limit per Connection: 0.200 (inch) between load reaction points. **Elongation Components:** System Stretch Includes sum of: Rod, Bearing Plate, Shrinkage Device ΔA & Shrinkage Device ΔR.

1 3/4"-A307 Anchor Rod

Shrinkage: 0.250 inch per floor

Shearwall Plates Wood Species: Douglas Fir-Larch Shearwall Plate Compression Capacity (Cross Grain): psi (all grades)

Compression Post Wood Species: Douglas Fir-Larch Compression Post Wood Capacity (Parallel to Grain):

Compression Post Design: per AutoTight

per Structural Plans S001 Compression Post Species:

Compression Post Nail Qty: Allowable per 16d Sinker in DFL = 189, Qty nails = 152, Allowable load = 28.73 kips, Total load = 28.63 kips, D/C = 99.7%.

www.comminsmfg.com



AutoTight® System Run Design Calc. Sheet for:

Engineering Calcs Revision: 0

Tree Farm

Plan Set: Plan Check 2

Plan Set Date: 03/23/2018

ermit #						CAT ID#	18-1789	
Run Name:	NSC.3				Te	nsile Streng	gth	Calc'd
Run Specif	ications	Compo	nent	Description	Capacity	Demand	D/C	Elong.
Required	Loads:	Commins	AutoTigh	t	(kips)	(kips)	Ratio	(in.)
Level =	Level 2	Compo	nent	Description	Capacity	Demand	D/C	Elong.
Differential Load:	15.06 (kips)	AT8A	-1.5	Shrinkage at Level, Shrinkage Device travel & D/C Ratio (in.)	1.75"	0.25"	14.3%	-
Tension Load:	15.06 (kips)	AT8A	-1.5	Shrinkage Device (1" I.D.) - Allowable Load	20.73	15.06	72.7%	-
Compression:	21.80 (kips)	-		Shrinkage Device - Deflection at Load	-	-	-	0.003
Story Height:	13.00 (ft.)	-		Shrinkage Device - Travel and Seating Increment ΔR	-	-	-	0.000
Plate Height:	11.95 (ft.)	L18-1	-1/4"	Bearing Plate at Reaction Point	19.29	15.06	78.1%	0.031
Floor Depth:	12.63 (in.)	R8A	307	1"-A307 Tension Rod	17.67	15.06	85.2%	0.055
			Limi	ting Component Tension Load Capacity, Load and D/C Ratio	17.67	15.06	85.2%	-
		Maxin	num Allo	wed Level Elongation, D/C Ratio and Total Level Elongation	0.200	-	45.0%	0.090
Compression	Outer (2) 2x4	(5) 2x4	nner	4x Wall Compression Post per Comp Post Calc Sheet	22.97	21.80	94.9%	-
Wood	Posts (2) 2x6	(3) 2x6	Posts	6x Wall Compression Post per Comp Post Calc Sheet	25.78	21.80	84.6%	-
	Footing	Comp		Description	Capacity		D/C	E

Level =	Footing	Component	Description	Capacity	Demand	D/C	Elong.
Tension Load:	15.06 (kips)	R8A307	1"-A307 Anchor Rod	17.67	15.06	85.2%	n/a

Design Code: OSSC\_2014 Main/State/Local

Loads per:

Include Drawing Date

Loads Type: ASD

Steel Stess Increase:

No

Takeup Device at Each Level:

Yes

Elongation Limit Required:

Yes

0.200 (inch) between load reaction points.

Elongation Limit per Connection: **Elongation Components:** 

System Stretch Includes sum of: Rod, Bearing Plate, Shrinkage Device ΔA & Shrinkage Device ΔR.

Shrinkage:

0.250 inch per floor

Douglas Fir-Larch DFL

Shearwall Plate Compression Capacity (Cross Grain):

Shearwall Plates Wood Species: Compression Post Wood Species: DFL

Douglas Fir-Larch

Compression Post Wood Capacity (Parallel to Grain): 1350 psi

625 psi (all grades)

Take Off Revision: 2 Eng

Compression Post Design: per AutoTight

Compression Post Species:

per Structural Plans S001 Allowable per 16d Sinker in DFL = 189, Qty nails = 80, Allowable load = 15.12 kips, Total load = 15.06 kips, D/C = 99.6%. Compression Post Nail Qty:

### AutoTight<sup>®</sup> Holdown System

www.comminsmfg.com



### AutoTight® Mid Wall Termination Header Design Calculations for:

**Tree Farm** 

Take Off Revision: 2 Eng Calcs F Code:OSSC\_2014 Main/State/Local (2005 NDS)

Calcs Revision: 0

Plan Set: Plan Check 2 Plan Date: 03/23/2018

CAT Project ID: 18-1789

C to C Bay	Outer	Inner	Beam	Bearing	Bearing	L <sub>span</sub>	Term	Header	Header	Header	Applied	Allowable	section	Allowable	Demand/	Wall
Stud Width/2		Post Thickness	Length	Plate Length, L	Plate L / 2 (in)		Header Species	Min Size	Width	Depth	Load Compression	Capacity psi	modulus	Capacity	Capacity Ratio	Thickness
(in) (in)	(in)	(in)	(in)	(in)	(in)	(in)	Opedica	(Nominal)	(in)	(in)	P (lbs)	DFL	Z	(lb)	D/C	
Run: EW2ab 16.00 7.25	3.00	7.50	7.00	7.00	= Bearing 3.50	Plate Name 0.00	DFL	4x6	5.50	3,50	20,300	625	11.23	NA>Shear	NA>Choor	Gy Moll
16.00 7.25	3.00	13.50	7.00	7.00	3.50	0.00	DFL	4x4	3.50	3.50	20,300	625	7.15	NA>Shear		6x Wall 4x Wall
Bending above																
Shear:			7.00	7.00	1	Shear Load I		0.00	5.50	3.50	0	625	Shear	16,042	0.0%	6x Wall
Shear: Compression:	3.00	7.50	7.00	7.00		Shear Load I earing Area		0.00 57.75	3.50 5.50	3.50	20,300	625 625	Shear	10,208	0.0%	4x Wall
Compression:	3.00	13.50				earing Area		57.75	3.50		20,300	625	Comp.	36,094 36,094	56.2% 56.2%	6x Wall 4x Wall
									0.00	,	20,000	020	о ор.	00,001	00.270	ix vvaii
Run: EW6						Plate Name								,		
16.00 7.25 16.00 7.25	3.00	12.00 19.50	7.00	10.00	5.00	-1.50 -1.50	DFL	4x6	5.50 3.50	3,50	30,830	625	11.23	NA>Shear		6x Wall
Bending above		19,50	7.00	10.00	5.00	-1.50	DFL	4x4	3.50	3.50	30,830	625	7.15	NA>Snear	NA>Shear	4x Wall
Shear:			7.00	10.00		Shear Load I	raction =	0.00	5.50	3.50	0	625	Shear	16,042	0.0%	6x Wall
Shear:			7.00	10.00		Shear Load F	The second secon	0.00	3.50	3.50	0	625	Shear	10,208	0.0%	4x Wall
Compression:	3.00	12.00				earing Area		82.50	5.50		30,830	625	Comp.	51,563	59.8%	6x Wall
Compression:	3.00	19.50			В	earing Area	per ena =	78.75	3.50		30,830	625	Comp.	49,219	62.6%	4x Wall
Run: EW6.5				L25-1-1/4"	= Bearing	Plate Name										
16.00 7.25	3.00	6.00	7.00	7.50	3.75	-0.25	DFL	4x6	5.50	3,50	23,160	625	11.23	NA>Shear	NA>Shear	6x Wall
16.00 7.25	3.00	10.50	7.00	7.50	3.75	-0.25	DFL	4x4	3.50	3.50	23,160	625	7.15	NA>Shear	NA>Shear	4x Wall
Bending above Shear:	E.		7.00	7.50	1 .	Shear Load I	Fraction - I	0.00	5.50	3.50	0	625	Shear	16,042	0.0%	6x Wall
Shear:			7.00	7.50		Shear Load I		0.00	3.50	3.50	0	625	Snear	10,208	0.0%	4x Wall
Compression:	3.00	6.00			1	earing Area		49.50	5.50	0.00	23,160	625	Comp.	30,938	74.9%	6x Wall
Compression:	3.00	10.50			В	earing Area	per end =	47.25	3.50		23,160	625	Comp.	29,531	78.4%	4x Wall
D NOD4			1	1 40 4 400		DI - N										
Run: NSB1 16.00 7.25	3.00	9.00	7.00	12.00	= Bearing 6.00	-2.50	DFL	4x6	5.50	3.50	38,820	625	11.23	NAShear	NA>Shear	6x Wall
16.00 7.25	3.00	15,00	7.00	12.00	6.00	-2.50	DFL	4x4	3.50	3.50	38,820	625	7.15		NA>Shear	4x Wall
Bending above																
Shear:			7.00	12.00		Shear Load I		0.00	5.50	3.50	0	625	Shear	16,042	0.0%	6x Wall
Shear:	2.00	9.00	7.00	12.00		Shear Load I		0.00	3.50	3.50	0	625	Shear	10,208	0.0%	4x Wall
Compression:	3.00	15.00				earing Area		66.00	5.50 3.50		38,820 38,820	625 625	Comp.	41,250 39,375	94.1% 98.6%	6x Wall 4x Wall
Gompi Godisii	0.00		1		_	ourning / mou	po. 0	00.00	0.00		00,020	020	Comp.	00,010	00.070	IX * COII
Run: NSB2						Plate Name			,							
16.00 7.25	3.00	10.50	7.00	12.00	6.00	-2.50	DFL	4x6	5.50	3.50	38,820	625	11.23		NA>Shear	6x Wall
16.00 7.25 16.00 7.25	3.00	10.50 16.50	7.00				DFL DFL	4x6 4x4	5.50	3.50 3.50	38,820 38,820	625 625	11.23 7.15		NA>Shear NA>Shear	6x Wall 4x Wall
16.00 7.25	3.00			12.00	6.00	-2.50	DFL									
16.00 7.25 16.00 7.25 Bending above	3.00	16.50	7.00	12.00 12.00	6.00 6.00	-2.50 -2.50	DFL Fraction =	4x4	3.50	3,50	38,820	625	7.15	NA>Shear	NA>Shear	4x Wall
16.00 7.25 16.00 7.25 Bending above Shear: Shear: Compression:	3.00	16.50	7.00	12.00 12.00	6.00 6.00	-2.50 -2.50 Shear Load I Shear Load I tearing Area	DFL Fraction = Fraction = per end =	0.00 0.00 74.25	3.50 5.50 3.50 5.50	3.50	38,820 0 0 38,820	625 625 625 625	7.15 Shear Shear Comp.	16,042 10,208 46,406	0.0% 0.0% 83.7%	6x Wall 4x Wall 6x Wall
16.00 7.25 16.00 7.25 Bending above Shear: Shear:	3.00	16.50	7.00	12.00 12.00	6.00 6.00	-2.50 -2.50 Shear Load I	DFL Fraction = Fraction = per end =	0.00 0.00	3.50 5.50 3.50	3.50	38,820 0 0	625 625 625	7.15 Shear Shear	NA>Shear 16,042 10,208	0.0% 0.0%	4x Wall 6x Wall 4x Wall
16.00 7.25 16.00 7.25 Bending above Shear: Shear: Compression:	3.00	16.50	7.00	12.00 12.00 12.00 12.00	6.00 6.00	-2.50 -2.50 Shear Load I Shear Load I tearing Area tearing Area	DFL Fraction = Fraction = per end =	0.00 0.00 74.25	3.50 5.50 3.50 5.50	3.50	38,820 0 0 38,820	625 625 625 625	7.15 Shear Shear Comp.	16,042 10,208 46,406	0.0% 0.0% 83.7%	6x Wall 4x Wall 6x Wall
16.00 7.25 16.00 7.25 Bending above Shear: Shear: Compression:	3.00	16.50	7.00	12.00 12.00 12.00 12.00	6.00 6.00	-2.50 -2.50 Shear Load I Shear Load I tearing Area	DFL Fraction = Fraction = per end =	0.00 0.00 74.25	3.50 5.50 3.50 5.50	3.50	38,820 0 0 38,820	625 625 625 625	7.15 Shear Shear Comp.	16,042 10,208 46,406 42,656	0.0% 0.0% 83.7%	6x Wall 4x Wall 6x Wall 6x Wall 4x Wall
16.00 7.25 16.00 7.25 Bending above Shear: Shear: Compression: Compression:	3.00	16.50 10.50 16.50	7.00 7.00 7.00	12.00 12.00 12.00 12.00 12.00	6.00 6.00 8 B B	-2.50 -2.50 Shear Load I Shear Load I earing Area rearing Area	DFL  Fraction = Fraction = per end = per end =	0.00 0.00 74.25 68.25	3.50 5.50 3.50 5.50 3.50	3.50 3.50 3.50	38,820 0 0 38,820 38,820	625 625 625 625 625	7.15 Shear Shear Comp. Comp.	16,042 10,208 46,406 42,656 NA>Shear	0.0% 0.0% 83.7% 91.0%	6x Wall 4x Wall 6x Wall 6x Wall 4x Wall
16.00 7.25 16.00 7.25 Bending above Shear: Shear: Compression: Compression: Run: NSC1 16.00 7.25 16.00 7.25 Bending above	3.00 3.00 3.00 3.00 3.00	10.50 10.50 16.50	7.00 7.00 7.00 7.00 7.00	12.00 12.00 12.00 12.00 12.00	6.00 6.00 8 8 8 8 8 8 4.50 4.50	-2.50 -2.50 Shear Load I Shear Load I searing Area searing Area Plate Name -1.00 -1.00	DFL Fraction = Fraction = per end = per end = DFL DFL	4x4 0.00 0.00 74.25 68.25 4x6 4x4	3.50 5.50 3.50 5.50 3.50 5.50 3.50	3,50 3,50 3,50 3,50 3,50 3,50	38,820 0 0 38,820 38,820 25,130 25,130	625 625 625 625 625 625 625	7.15 Shear Shear Comp. Comp.	16,042 10,208 46,406 42,656 NA>Shear	0.0% 0.0% 83.7% 91.0% NA>Shear NA>Shear	6x Wall 4x Wall 6x Wall 4x Wall 4x Wall 6x Wall 4x Wall
16.00 7.25 16.00 7.25 Bending above Shear: Compression: Compression: Run: NSC1 16.00 7.25 Bending above Shear:	3.00 3.00 3.00 3.00 3.00	10.50 10.50 16.50	7.00 7.00 7.00 7.00 7.00 7.00	12.00 12.00 12.00 12.00 12.00 12.00 12.00 12.00 9.00 9.00	6.00 6.00 8 8 8 8 8 8 4.50 4.50	-2.50 -2.50 Shear Load I Shear Load I Shearing Area dearing Area Plate Name -1.00 -1.00 Shear Load I	DFL Fraction = Fraction = per end = per end = DFL DFL DFL Fraction =	4x4 0.00 0.00 74.25 68.25 4x6 4x4 0.00	3.50 5.50 3.50 5.50 3.50 5.50 3.50	3.50 3.50 3.50 3.50 3.50	38,820 0 0 38,820 38,820 25,130 25,130	625 625 625 625 625 625 625 625	7.15 Shear Shear Comp. Comp. 11.23 7.15 Shear	16,042 10,208 46,406 42,656 NA>Shear NA>Shear	0.0% 0.0% 83.7% 91.0% NA>Shear NA>Shear	6x Wall 4x Wall 6x Wall 6x Wall 4x Wall 4x Wall 6x Wall 4x Wall 6x Wall
16.00 7.25 16.00 7.25 Bending above Shear: Compression: Compression: Run: NSC1 16.00 7.25 16.00 7.25 Bending above Shear: Shear:	3.00 3.00 3.00 3.00	10.50 10.50 16.50	7.00 7.00 7.00 7.00 7.00	12.00 12.00 12.00 12.00 12.00	6.00 6.00 8 8 8 8 8 4.50 4.50	-2.50 -2.50 Shear Load I Shear Load I Shearing Area dearing Area -1.00 -1.00 Shear Load I Shear Load I	DFL Fraction = Fraction = per end = per end = DFL DFL DFL Fraction = Fraction =	4x4 0.00 0.00 74.25 68.25 4x6 4x4 0.00 0.00	3.50 5.50 3.50 5.50 3.50 5.50 3.50 5.50 3.50	3,50 3,50 3,50 3,50 3,50 3,50	38,820 0 0 38,820 38,820 25,130 25,130 0 0	625 625 625 625 625 625 625 625	7.15 Shear Shear Comp. Comp. 11.23 7.15 Shear Shear Shear	16,042 10,208 46,406 42,656 NA>Shear NA>Shear 16,042 10,208	0.0% 0.0% 83.7% 91.0% NA>Shear NA>Shear 0.0%	6x Wall 4x Wall 6x Wall 4x Wall 4x Wall 4x Wall 6x Wall 4x Wall 6x Wall 4x Wall
16.00 7.25 16.00 7.25 Bending above Shear: Compression: Compression: Run: NSC1 16.00 7.25 Bending above Shear:	3.00 3.00 3.00 3.00 3.00	10.50 10.50 16.50	7.00 7.00 7.00 7.00 7.00 7.00	12.00 12.00 12.00 12.00 12.00 12.00 12.00 12.00 9.00 9.00	6.00 6.00 8 8 8 8 8 4.50 4.50	-2.50 -2.50 Shear Load I Shear Load I Shearing Area dearing Area Plate Name -1.00 -1.00 Shear Load I	DFL Fraction = Fraction = per end = per end = DFL DFL DFL Fraction = Fraction = per end =	4x4 0.00 0.00 74.25 68.25 4x6 4x4 0.00	3.50 5.50 3.50 5.50 3.50 5.50 3.50	3.50 3.50 3.50 3.50 3.50	38,820 0 0 38,820 38,820 25,130 25,130	625 625 625 625 625 625 625 625	7.15 Shear Shear Comp. Comp. 11.23 7.15 Shear	16,042 10,208 46,406 42,656 NA>Shear NA>Shear	0.0% 0.0% 83.7% 91.0% NA>Shear NA>Shear	6x Wall 4x Wall 6x Wall 6x Wall 4x Wall 4x Wall 6x Wall 4x Wall 6x Wall
16.00 7.25 16.00 7.25 Bending above Shear: Compression: Compression: Run: NSC1 16.00 7.25 16.00 7.25 Bending above Shear: Shear: Compression: Compression:	3.00 3.00 3.00 3.00 3.00	10.50 16.50 16.50 6.00 10.50	7.00 7.00 7.00 7.00 7.00 7.00	12.00 12.00 12.00 12.00 12.00 12.00 12.00 9.00 9.00 9.00	6.00 6.00 8 B B B B 4.50 4.50	-2.50 -2.50 Shear Load I Shear Load I Shearing Area Learing Area Load I Shear Load	DFL Fraction = Fraction = per end = per end = DFL DFL DFL Fraction = Fraction = per end =	4x4 0.00 0.00 74.25 68.25 4x6 4x4 0.00 0.00 49.50	5.50 3.50 5.50 3.50 5.50 3.50 5.50 3.50 5.50 3.50	3.50 3.50 3.50 3.50 3.50	38,820 0 0 38,820 38,820 25,130 25,130 0 0 25,130	625 625 625 625 625 625 625 625 625 625	7.15 Shear Shear Comp. Comp. 11.23 7.15 Shear Shear Comp.	NA>Shear  16,042 10,208 46,406 42,656  NA>Shear NA>Shear 16,042 10,208 30,938	NA>Shear  0.0% 0.0% 83.7% 91.0%  NA>Shear NA>Shear 0.0% 0.0% 81.2%	6x Wall 4x Wall 6x Wall 6x Wall
16.00 7.25 16.00 7.25 Bending above Shear: Compression: Compression: Run: NSC1 16.00 7.25 16.00 7.25 Bending above Shear: Shear: Compression: Compression: Run: NSC2	3.00 3.00 3.00 3.00 3.00 3.00	10.50 10.50 16.50 10.50	7.00 7.00 7.00 7.00 7.00 7.00 7.00	12.00 12.00 12.00 12.00 12.00 12.00 12.00 9.00 9.00 9.00	6.00 6.00 8 B B = Bearing 4.50 4.50	-2.50 -2.50 Shear Load I Shear Load I Shear Load I searing Area rearing Area -1.00 -1.00 Shear Load I Shear Load I shear Load I shear Load I shearing Area rearing Area	DFL  Fraction = Fraction = per end =  DFL  DFL  Traction = Fraction = per end = per end =	4x4 0.00 0.00 74.25 68.25 4x6 4x4 0.00 0.00 49.50 47.25	3.50 5.50 3.50 5.50 3.50 5.50 3.50 5.50 3.50 5.50 3.50	3.50 3.50 3.50 3.50 3.50 3.50 3.50	38,820 0 0 38,820 38,820 25,130 25,130 0 0 25,130	625 625 625 625 625 625 625 625 625 625	7.15 Shear Shear Comp. Comp.  11.23 7.15 Shear Shear Comp. Comp.	NA>Shear  16,042 10,208 46,406 42,656  NA>Shear NA>Shear 16,042 10,208 30,938 29,531	NA>Shear 0.0% 83.7% 91.0%  NA>Shear NA>Shear 0.0% 81.2% 85.1%	6x Wall 4x Wall 6x Wall 4x Wall 4x Wall 6x Wall 4x Wall 6x Wall 4x Wall 6x Wall 4x Wall 6x Wall 4x Wall
16.00 7.25 16.00 7.25 Bending above Shear: Compression: Compression: Run: NSC1 16.00 7.25 16.00 7.25 Bending above Shear: Compression: Compression: Compression: Compression: Compression: Compression: Run: NSC2 16.00 7.25	3.00 3.00 3.00 3.00 3.00 3.00 3.00	10.50 16.50 16.50 10.50 10.50	7.00 7.00 7.00 7.00 7.00 7.00 7.00	12.00 12.00 12.00 12.00 12.00 12.00 12.00 9.00 9.00 9.00 9.00 12.00 12.00 12.00 12.00 12.00 12.00	6.00 6.00 8 B B B B B B B B B B B B B B B B B B B	-2.50 -2.50 Shear Load I Shear Load I searing Area searing Area -1.00 -1.00 Shear Load I Shear Load I shear Load I shear Load I searing Area searing Area searing Area Plate Name -0.25	DFL Fraction = Fraction = per end = per end = DFL DFL Fraction = Fraction = per end = per end =	4x4 0.00 0.00 74.25 68.25 4x6 4x4 0.00 0.00 49.50 47.25	5.50 3.50 5.50 3.50 5.50 3.50 5.50 3.50 5.50 3.50 5.50	3.50 3.50 3.50 3.50 3.50 3.50 3.50	38,820 0 0 38,820 38,820 25,130 25,130 0 0 25,130 25,130 21,800	625 625 625 625 625 625 625 625 625 625	7.15  Shear Shear Comp. Comp.  11.23  7.15  Shear Shear Comp. Comp.  11.23	NA>Shear  16,042 10,208 46,406 42,656  NA>Shear NA>Shear 16,042 10,208 30,938 29,531  NA>Shear	NA>Shear 0.0% 0.0% 83.7% 91.0%  NA>Shear NA>Shear 0.0% 81.2% 85.1%	6x Wall 4x Wall 6x Wall 6x Wall
16.00 7.25 16.00 7.25 Bending above Shear: Compression: Compression: Run: NSC1 16.00 7.25 16.00 7.25 Bending above Shear: Shear: Compression: Compression: Run: NSC2	3.00 3.00 3.00 3.00 3.00 3.00 3.00 3.00	10.50 10.50 16.50 10.50	7.00 7.00 7.00 7.00 7.00 7.00 7.00	12.00 12.00 12.00 12.00 12.00 12.00 12.00 9.00 9.00 9.00	6.00 6.00 8 B B = Bearing 4.50 4.50	-2.50 -2.50 Shear Load I Shear Load I Shear Load I searing Area rearing Area -1.00 -1.00 Shear Load I Shear Load I shear Load I shear Load I shearing Area rearing Area	DFL  Fraction = Fraction = per end =  DFL  DFL  Traction = Fraction = per end = per end =	4x4 0.00 0.00 74.25 68.25 4x6 4x4 0.00 0.00 49.50 47.25	3.50 5.50 3.50 5.50 3.50 5.50 3.50 5.50 3.50 5.50 3.50	3.50 3.50 3.50 3.50 3.50 3.50 3.50	38,820 0 0 38,820 38,820 25,130 25,130 0 0 25,130	625 625 625 625 625 625 625 625 625 625	7.15 Shear Shear Comp. Comp.  11.23 7.15 Shear Shear Comp. Comp.	NA>Shear  16,042 10,208 46,406 42,656  NA>Shear NA>Shear 16,042 10,208 30,938 29,531  NA>Shear	NA>Shear 0.0% 83.7% 91.0%  NA>Shear NA>Shear 0.0% 81.2% 85.1%	6x Wall 4x Wall 6x Wall 4x Wall 4x Wall 6x Wall 4x Wall 6x Wall 4x Wall 6x Wall 4x Wall 6x Wall 4x Wall
16.00 7.25 16.00 7.25 Bending above Shear: Compression: Compression: Run: NSC1 16.00 7.25 16.00 7.25 Bending above Shear: Compression: Compression: Compression: Compression: Compression: Compression: Bun: NSC2 16.00 7.25 16.00 7.25 16.00 7.25 Bending above Shear:	3.00 3.00 3.00 3.00 3.00 3.00 3.00 3.00	10.50 16.50 16.50 10.50 10.50	7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00	12.00 12.00 12.00 12.00 12.00 12.00 12.00 9.00 9.00 9.00 9.00 125-1-1/4" 7.50 7.50	6.00 6.00 8 B B = Bearing 4.50 4.50 4.50 8 B = Bearing 3.75 3.75	-2.50 -2.50 Shear Load I Shear	DFL  Fraction =  Fraction =  per end =  DFL  DFL  Fraction =  Fraction =  Per end =  per end =  DFL  DFL  DFL  Fraction =	4x4 0.00 0.00 74.25 68.25 4x6 4x4 0.00 49.50 47.25 4x6 4x4 0.00	5.50 3.50 5.50 3.50 5.50 3.50 5.50 3.50 5.50 3.50 5.50 3.50	3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50	38,820 0 0 38,820 38,820 25,130 25,130 0 0 25,130 21,800 21,800	625 625 625 625 625 625 625 625 625 625	7.15 Shear Shear Comp. Comp.  11.23 7.15 Shear Shear Comp. Comp. 11.23 7.15	NA>Shear  16,042 10,208 46,406 42,656  NA>Shear NA>Shear  NA>Shear  NA>Shear  NA>Shear  NA>Shear	NA>Shear  0.0% 0.0% 83.7% 91.0%  NA>Shear NA>Shear 0.0% 85.1%  NA>Shear NA>Shear 0.0%	6x Wall 6x Wall 6x Wall 4x Wall 6x Wall 4x Wall 6x Wall 4x Wall 6x Wall 4x Wall 6x Wall 6x Wall 6x Wall 6x Wall 6x Wall
16.00 7.25 16.00 7.25 Bending above Shear: Compression: Compression: Run: NSC1 16.00 7.25 16.00 7.25 Bending above Shear: Compression: Compression: Compression: Compression: Compression: Run: NSC2 16.00 7.25 16.00 7.25 Bending above Shear: Shear: Compression: Run: NSC2 16.00 7.25 Bending above Shear: Shear:	3.00 3.00 3.00 3.00 3.00 3.00 3.00 3.00	10.50 16.50 16.50 10.50 10.50	7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00	12.00 12.00 12.00 12.00 12.00 12.00 9.00 9.00 9.00 9.00 125-1-1/4" 7.50 7.50	6.00 6.00 8 B B = Bearing 4.50 4.50 8 B B = Bearing 3.75	-2.50 -2.50 Shear Load I Shear	DFL Fraction = Fraction = per end = per end = DFL DFL Fraction = per end = per end = per end = per end = Fraction = Fraction = Fraction = Fraction = Fraction =	4x4  0.00 0.00 74.25 68.25  4x6 4x4  0.00 0.00 49.50 47.25  4x6 4x4  0.00 0.00 0.00	5.50 3.50 5.50 3.50 5.50 3.50 5.50 3.50 5.50 3.50 5.50 3.50 5.50 3.50	3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50	38,820 0 0 38,820 38,820 25,130 25,130 0 0 25,130 21,800 21,800 0	625 625 625 625 625 625 625 625 625 625	7.15 Shear Shear Comp. Comp.  11.23 7.15 Shear Shear Comp. Comp.  11.23 7.15 Shear S	NA>Shear  16,042 10,208 46,406 42,656  NA>Shear NA>Shear NA>Shear NA>Shear NA>Shear NA>Shear NA>Shear NA>Shear	NA>Shear 0.0% 83.7% 91.0% NA>Shear NA>Shear 0.0% 81.2% 85.1% NA>Shear 0.0% 0.0% 0.0% 0.0% 0.0%	6x Wall 4x Wall
16.00 7.25 16.00 7.25 Bending above Shear: Compression: Compression: Run: NSC1 16.00 7.25 16.00 7.25 Bending above Shear: Compression: Compression: Compression: Compression: Run: NSC2 16.00 7.25 16.00 7.25 Bending above Shear: Shear: Compression: Compression: Compression: Compression:	3.00 3.00 3.00 3.00 3.00 3.00 3.00 3.00	10.50 16.50 16.50 10.50 10.50 10.50	7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00	12.00 12.00 12.00 12.00 12.00 12.00 12.00 9.00 9.00 9.00 9.00 125-1-1/4" 7.50 7.50	6.00 6.00 8 B B B B B B B B B B B B B B B B B B B	-2.50 -2.50 Shear Load I Shear Load I searing Area learing Area -1.00 -1.00 Shear Load I shear L	DFL  Fraction =  Fraction =  per end =  DFL  DFL  Fraction =  Fraction =  Per end =  DFL  DFL  DFL  DFL  DFL  DFL  DFL  DF	4x4 0.00 0.00 74.25 68.25 4x6 4x4 0.00 0.00 49.50 47.25 4x6 4x4	5.50 3.50 5.50 3.50 5.50 3.50 5.50 3.50 5.50 3.50 5.50 3.50 5.50 3.50	3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50	38,820 0 0 38,820 38,820 25,130 25,130 0 0 25,130 21,800 21,800 0 0 0 0 0 0	625 625 625 625 625 625 625 625 625 625	7.15  Shear Shear Comp. Comp.  11.23  7.15  Shear Shear Comp. Comp.  11.23  7.15  Shear Shear Comp. Comp.  11.23  7.15	NA>Shear  16,042 10,208 46,406 42,656  NA>Shear	NA>Shear  0.0% 0.0% 83.7% 91.0%  NA>Shear NA>Shear NA>Shear 0.0% 81.2% 85.1%  NA>Shear NA>Shear NA>Shear NA>Shear	6x Wall 4x Wall 6x Wall 6x Wall 6x Wall 6x Wall 6x Wall 6x Wall
16.00 7.25 16.00 7.25 Bending above Shear: Compression: Compression: Run: NSC1 16.00 7.25 16.00 7.25 Bending above Shear: Compression: Compression: Compression: Compression: Compression: Run: NSC2 16.00 7.25 16.00 7.25 Bending above Shear: Shear: Shear: Shear: Shear: Shear: Shear: Shear: Shear:	3.00 3.00 3.00 3.00 3.00 3.00 3.00 3.00	10.50 16.50 16.50 10.50 10.50	7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00	12.00 12.00 12.00 12.00 12.00 12.00 12.00 9.00 9.00 9.00 9.00 125-1-1/4" 7.50 7.50	6.00 6.00 8 B B B B B B B B B B B B B B B B B B B	-2.50 -2.50 Shear Load I Shear	DFL  Fraction =  Fraction =  per end =  DFL  DFL  Fraction =  Fraction =  Per end =  DFL  DFL  DFL  DFL  DFL  DFL  DFL  DF	4x4  0.00 0.00 74.25 68.25  4x6 4x4  0.00 0.00 49.50 47.25  4x6 4x4  0.00 0.00 0.00	5.50 3.50 5.50 3.50 5.50 3.50 5.50 3.50 5.50 3.50 5.50 3.50 5.50 3.50	3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50	38,820 0 0 38,820 38,820 25,130 25,130 0 0 25,130 21,800 21,800 0	625 625 625 625 625 625 625 625 625 625	7.15 Shear Shear Comp. Comp.  11.23 7.15 Shear Shear Comp. Comp.  11.23 7.15 Shear S	NA>Shear  16,042 10,208 46,406 42,656  NA>Shear NA>Shear NA>Shear NA>Shear NA>Shear NA>Shear NA>Shear NA>Shear	NA>Shear 0.0% 83.7% 91.0% NA>Shear NA>Shear 0.0% 81.2% 85.1% NA>Shear 0.0% 0.0% 0.0% 0.0% 0.0%	6x Wall 4x Wall
16.00 7.25 16.00 7.25 Bending above Shear: Compression: Compression: Run: NSC1 16.00 7.25 16.00 7.25 Bending above Shear: Compression: Compression: Compression: Run: NSC2 16.00 7.25 16.00 7.25 Bending above Shear: Compression: Compression: Run: NSC2 16.00 7.25 Bending above Shear: Compression: Compression: Compression: Run: NSD	3.00 3.00 3.00 3.00 3.00 3.00 3.00 3.00	10.50 16.50 16.50 10.50 10.50 10.50 4.50 9.00	7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00	12.00 12.00 12.00 12.00 12.00 12.00 12.00 9.00 9.00 9.00 9.00 1.25-1-1/4" 7.50 7.50 7.50	6.00 6.00  B B B  = Bearing 4.50 4.50  4.50  B B B  = Bearing 3.75 3.75	-2.50 -2.50 Shear Load I Shear	DFL  Fraction =  Fraction =  per end =  DFL  DFL  Fraction =  Fraction =  per end =  DFL  DFL  DFL  Fraction =  per end =  DFL  per end =  per end =	4x4 0.00 0.00 74.25 68.25 4x6 4x4 0.00 0.00 49.50 47.25 4x6 4x4	5.50 3.50 5.50 3.50 5.50 3.50 5.50 3.50 5.50 3.50 5.50 3.50 5.50 3.50 5.50 3.50	3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50	38,820 0 0 38,820 38,820 25,130 25,130 0 0 25,130 21,800 21,800 0 0 0 0 0 0	625 625 625 625 625 625 625 625 625 625	7.15  Shear Shear Comp. Comp.  11.23  7.15  Shear Shear Comp. Comp.  11.23  7.15  Shear Shear Comp. Comp.  11.23  7.15	NA>Shear  16,042 10,208 46,406 42,656  NA>Shear NA>Shear NA>Shear 16,042 10,208 30,938 29,531  NA>Shear NA>Shear 25,781 26,250	NA>Shear 0.0% 83.7% 91.0% NA>Shear NA>Shear 0.0% 81.2% 85.1%  NA>Shear NA>Shear NA>Shear NA>Shear NA>Shear NA>Shear	6x Wall 4x Wall
16.00 7.25 16.00 7.25 Bending above Shear: Compression: Compression: Run: NSC1 16.00 7.25 16.00 7.25 Bending above Shear: Compression: Compression: Compression: Compression: Compression: Compression: Run: NSC2 16.00 7.25 Bending above Shear: Shear: Compression: Compression: Compression: Compression: Run: NSC2 16.00 7.25 Reding above Shear: Compression: Run: NSD 16.00 7.25	3.00 3.00 3.00 3.00 3.00 3.00 3.00 3.00	10.50 16.50 16.50 10.50 10.50 10.50 4.50 9.00	7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00	12.00 12.00 12.00 12.00 12.00 12.00 12.00 12.00 9.00 9.00 9.00 9.00 9.00 7.50 7.50 7.50	6.00 6.00 8 B B B B B B B B B B B B B B B B B B B	-2.50 -2.50 Shear Load I Shear Load I searing Area learing Area -1.00 -1.00 Shear Load I searing Area learing Area learing Area searing Area learing Area -1.00	DFL  Fraction = per end = per end = per end =  DFL  DFL  Fraction = per end = per end = per end = per end =  DFL  DFL  DFL  DFL  DFL  DFL  DFL  DF	4x4  0.00 0.00 74.25 68.25  4x6 4x4  0.00 0.00 49.50 47.25  4x6 4x4  0.00 0.00 41.25 42.00	5.50 3.50 5.50 3.50 5.50 3.50 5.50 3.50 5.50 3.50 5.50 3.50 5.50 3.50 5.50 3.50	3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50	38,820 0 0 38,820 38,820 25,130 25,130 0 0 25,130 25,130 21,800 21,800 0 0 21,800 21,800 21,800	625 625 625 625 625 625 625 625 625 625	7.15 Shear Comp. Comp. 11.23 7.15 Shear Shear Comp. Comp. 11.23 7.15 Shear Shear Comp. Comp. 11.23 7.15	NA>Shear  16,042 10,208 46,406 42,656  NA>Shear	NA>Shear  0.0% 0.0% 83.7% 91.0%  NA>Shear NA>Shear NA>Shear 0.0% 81.2% 85.1%  NA>Shear NA>Shear NA>Shear NA>Shear NA>Shear NA>Shear	6x Wall 4x Wall 6x Wall 6x Wall 6x Wall 6x Wall 6x Wall
16.00 7.25 16.00 7.25 Bending above Shear: Compression: Compression: Compression: Run: NSC1 16.00 7.25 Bending above Shear: Compression: Compression: Compression: Compression: Compression: Run: NSC2 16.00 7.25 Bending above Shear: Shear: Compression: Compression: Run: NSC2 16.00 7.25 Bending above Shear: Compression: Compression: Compression: Compression: Compression: Compression: Run: NSD 16.00 7.25 16.00 7.25	3.00 3.00 3.00 3.00 3.00 3.00 3.00 3.00	10.50 16.50 16.50 10.50 10.50 10.50 4.50 9.00	7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00	12.00 12.00 12.00 12.00 12.00 12.00 12.00 9.00 9.00 9.00 9.00 1.25-1-1/4" 7.50 7.50 7.50	6.00 6.00  B B B  = Bearing 4.50 4.50  4.50  B B B  = Bearing 3.75 3.75	-2.50 -2.50 Shear Load I Shear	DFL  Fraction =  Fraction =  per end =  DFL  DFL  Fraction =  Fraction =  per end =  DFL  DFL  DFL  Fraction =  per end =  DFL  per end =  per end =	4x4 0.00 74.25 68.25 4x6 4x4 0.00 0.00 49.50 47.25 4x6 4x4 0.00 0.00 47.25 4x6 4x4	5.50 3.50 5.50 3.50 5.50 3.50 5.50 3.50 5.50 3.50 5.50 3.50 5.50 3.50 5.50 3.50	3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50	38,820 0 0 38,820 38,820 25,130 25,130 0 0 25,130 21,800 21,800 0 0 21,800 21,800	625 625 625 625 625 625 625 625 625 625	7.15 Shear Comp. Comp.  11.23 7.15 Shear Comp. Comp.  11.23 7.15 Shear Comp. Comp.  11.23 7.15 Shear Comp. Comp.	NA>Shear  16,042 10,208 46,406 42,656  NA>Shear	NA>Shear 0.0% 83.7% 91.0% NA>Shear NA>Shear 0.0% 81.2% 85.1%  NA>Shear NA>Shear NA>Shear NA>Shear NA>Shear NA>Shear	6x Wall 4x Wall
16.00 7.25 16.00 7.25 Bending above Shear: Compression: Compression: Compression: Run: NSC1 16.00 7.25 Bending above Shear: Compression: Compression: Compression: Compression: Compression: Run: NSC2 16.00 7.25 Bending above Shear: Shear: Compression: Compression: Run: NSC2 16.00 7.25 Bending above Shear: Shear: Compression: Comp	3.00 3.00 3.00 3.00 3.00 3.00 3.00 3.00	10.50 16.50 16.50 10.50 10.50 10.50 4.50 9.00	7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00	12.00 12.00 12.00 12.00 12.00 12.00 12.00 9.00 9.00 9.00 9.00 7.50 7.50 7.50 7.50 7.50	6.00 6.00 8 8 8 8 8 = Bearing 4.50 4.50 3.75 3.75 8 8 8 = Bearing 4.50 4.50 4.50	-2.50 -2.50 -2.50 Shear Load I Shear Load I searing Area learing Area	DFL  Fraction = per end = per end =  DFL  DFL  Fraction = per end = per end = per end = per end =  DFL  DFL  DFL  DFL  DFL  DFL  DFL  DF	4x4  0.00 0.00 74.25 68.25  4x6 4x4  0.00 0.00 49.50 47.25  4x6 4x4  0.00 0.00 41.25 42.00	5.50 3.50 5.50 3.50 5.50 3.50 5.50 3.50 5.50 3.50 5.50 3.50 5.50 3.50 5.50 3.50	3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50	38,820 0 0 38,820 38,820 25,130 25,130 0 0 25,130 21,800 21,800 21,800 21,800 21,800 21,800	625 625 625 625 625 625 625 625 625 625	7.15 Shear Shear Comp. Comp.  11.23 7.15 Shear Shear Comp. Comp.  11.23 7.15 Shear Comp. Comp.  11.23 7.15	NA>Shear  16,042 10,208 46,406 42,656  NA>Shear NA>Shear  NA>Shear  16,042 10,208 30,938 29,531  NA>Shear  16,042 10,208 16,042 10,208 NA>Shear  NA>Shear	NA>Shear  0.0% 83.7% 91.0%  NA>Shear NA>Shear  0.0% 85.1%  NA>Shear  0.0% 86.1%  NA>Shear  0.0% 0.0% 87.2%  NA>Shear  0.0% NA>Shear  0.0% NA>Shear	6x Wall 4x Wall
16.00 7.25 16.00 7.25 Bending above Shear: Compression: Compression: Compression: Run: NSC1 16.00 7.25 Bending above Shear: Compression: Compression: Compression: Compression: Compression: Run: NSC2 16.00 7.25 Bending above Shear: Shear: Compression: Compression: Run: NSC2 16.00 7.25 Bending above Shear: Compression: Compression: Compression: Compression: Compression: Compression: Run: NSD 16.00 7.25 16.00 7.25	3.00 3.00 3.00 3.00 3.00 3.00 3.00 3.00	10.50 16.50 16.50 10.50 10.50 10.50 4.50 9.00	7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00	12.00 12.00 12.00 12.00 12.00 12.00 12.00 12.00 9.00 9.00 9.00 9.00 9.00 7.50 7.50 7.50	6.00 6.00 8 8 8 8 = Bearing 4.50 4.50 8 8 = Bearing 3.75 3.75 8 8 8 = Bearing 4.50 4.50	-2.50 -2.50 Shear Load I Shear Load I searing Area learing Area -1.00 -1.00 Shear Load I searing Area learing Area learing Area searing Area learing Area -1.00	DFL  Fraction =  Per end =  DFL  DFL  Fraction =  Fraction =  Fraction =  Per end =  DFL  DFL  Fraction =  Per end =  DFL  DFL  Fraction =  Fraction =  Per end =  DFL  DFL  Fraction =  Per end =  Per end =  Fraction =  DFL  DFL  Fraction =	4x4  0.00 0.00 74.25 68.25  4x6 4x4  0.00 0.00 49.50 47.25  4x6 4x4  0.00 0.00 41.25 42.00	5.50 3.50 5.50 3.50 5.50 3.50 5.50 3.50 5.50 3.50 5.50 3.50 5.50 3.50 5.50 3.50	3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50	38,820 0 0 38,820 38,820 25,130 25,130 0 0 25,130 25,130 21,800 21,800 0 0 21,800 21,800 21,800	625 625 625 625 625 625 625 625 625 625	7.15 Shear Comp. Comp. 11.23 7.15 Shear Shear Comp. Comp. 11.23 7.15 Shear Shear Comp. Comp. 11.23 7.15	NA>Shear  16,042 10,208 46,406 42,656  NA>Shear	NA>Shear  0.0% 0.0% 83.7% 91.0%  NA>Shear NA>Shear NA>Shear 0.0% 81.2% 85.1%  NA>Shear NA>Shear NA>Shear NA>Shear NA>Shear NA>Shear	6x Wall 4x Wall 6x Wall 6x Wall 6x Wall 6x Wall 6x Wall
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### AutoTight® Mid Wall Termination Header Design Calculations for: Tree Farm

Take Off Revision: 2 Eng Calcs
Code: OSSC\_2014 Main/State/Local (2005 NDS)

Calcs Revision: 0

Plan Set: Plan Check 2

Plan Date: 03/23/2018

CAT Project ID: 18-1789

C to C Ba Stud Widt	th/2	Outer Post nickness	Inner Post Thickness		Bearing Plate Length, L	Bearing Plate L / 2 (in)	L <sub>span</sub>	Term Header Species	Header Min Size	Header Width	Header Depth	Load Compression	Allowable Capacity psi	section modulus	Allowable Capacity	Capacity Ratio	Wall Thickness
(in) (in	1)	(in)	(in)	(in)	(in)	(in)	(in)		(Nominal)	(in)	(in)	P (lbs)	DFL	Z	(lb)	D/C	
Run: NSE					L30-1-1/2"	= Bearing I	Plate Name										
16.00 7.2	25	3.00	15.00	7.00	9.00	4.50	-1.00	DFL	4x6	5.50	3,50	28,630	625	11.23	NA>Shear	NA>Shear	6x Wall
16.00 7.2	25	3.00	24.00	7.00	9.00	4.50	-1.00	DFL	4x6	3.50	5.50	28,630	625	17.65	NA>Shear	NA>Shear	4x Wall
Bending abo	ove:																
Shear:				7.00	9.00	5	Shear Load F	raction =	0.00	5.50	3.50	0	625	Shear	16,042	0.0%	6x Wall
Shear:				7.00	9.00	8	hear Load F	raction =	0.00	3.50	5.50	0	625	Shear	16,042	0.0%	4x Wall
Compression	on:	3.00	15.00			Be	earing Area	per end =	99.00	5.50		28,630	625	Comp.	61,875	46.3%	6x Wall
Compression	on:	3.00	24.00			Be	earing Area	per end =	94.50	3.50		28,630	625	Comp.	59,063	48.5%	4x Wall
Run: NSC	2.3				L18-1-1/4"	= Bearing I	Plate Name										
16.00 7.2	25	3.00	4.50	7.00	5.50	2.75	0.75	DFL	4x6	5.50	3,50	15,060	625	11.23	18,715	80.5%	6x Wall
16.00 7.2	25	3.00	7.50	7.00	5.50	2.75	0.75	DFL	4x6	3.50	5.50	15,060	625	17.65	29,410	51.2%	4x Wall
Bending about	ove:																
Shear:				7.00	5.50	5	Shear Load F	raction =	0.00	5.50	3.50	0	625	Shear	16,042	0.0%	6x Wall
Shear:				7.00	5.50	5	Shear Load F	raction =	0.00	3.50	5.50	0	625	Shear	16,042	0.0%	4x Wall
Compression	on:	3.00	4.50			Be	earing Area	per end =	41.25	5.50		15,060	625	Comp.	25,781	58.4%	6x Wall

36.75

#### Header Design Notes:

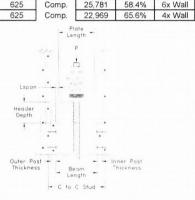
Compression:

1. Bearing Plate spreads load.

3.00

- 2. Point Load (P) location transfer of combined termination tension.
- 3. Beam supported at both ends 2 equal symmetrical loads max stress=W\*a/Z where a= Lspan & W=P/2 & Z=section modulus of beam
- 4. Shear calculated per NDS 2005 eqn 3.4-2 & sec 3.4.3 which says:
- "... uniformly distributed loads within a distance from supports equal to the depth of the bending member, d, shall be permitted to be ignored."
- fv=3\*V/2\*b\*d where fv=actual stress=species capacity, V=shear load=allowable, b=breadth, d=depth
- 5. When the plate overlaps the post or gets too close to the post the beam equation does not apply, see shear instead.

Bearing Area per end =



### Compression Post Schedule 4x Wall

# Tree Farm

Z	Run Name	EW	2ab	EV	V6	EW	6.5	NS	B1	NS	B2	NS	C1	NS	C2	NS	SD	NS	SE	NS	C.3
×	Wall Size	4x V	Vall	4x \	Vall	4x V	Vall														
ا تــ	Post Location	Outer	Inner																		
	Post Size	2x4			2x4	2x4															
က	Post Qty	2	9	2	13	2	7	2	10	2	11	2	7	2	6			2	16		
0	Post Length inches	54.	00	54.	00	54.	00	54.	00	54.	00	54.	00	54.	00			54.			
6	Required Load kips	33.	80	48.	54	26.	57	38.	82	41.	58	26.	95	24.	55			57.	55		
L	Allowable Load kips	36.	09	49.	22	29.	53	39.	37	42.	65	29.	53	26.	25			59.			
	Limiting Failure Mode	Crus	hing			Crus	hing														

	Post Size	2x4	2x4	2x4	2x4	2x4	2x4	2x4	2x4	2x4	2x4	2x4	2x4	2x4	2x4	2x4	2x4	2x4	2x4	2x4	2x4
2	Post Qty		21	2	30	2	16	2	17	2	23	2	16	2	15	2	8	2	34	2	5
e	Post Length inches	137	.88	137	.88	137	.88	137	.88	137	.88	137	.88	137	.88	54	.00	137	.88	54.	00
>	Required Load kips	51.	52	72.	18	40.	50	43.	29	55.	91	41.	07	37.	42	31.	.19	83.	50	21.	80
تــــــــــــــــــــــــــــــــــــــ	Allowable Load kips	53.	41	74.	30	41.	80	44.	12	58.	05	41.	80	39.	47	32.	.81	83.	59	22.	97
	Limiting Failure Mode	Bucl	kling	Buck	ding	Buck	kling	Buck	kling	Buck	kling	Buck	ding	Buck	ding	Crus	hing	Buck	kling	Crus	hing

#### Notes:

- 1. Posts may be arranged as desired by the builder as long as:
  - a. The total post quantity is the same as or greater than the quantity listed here.
  - b. And there is at least 1 post on each side of each rod.
  - c. Compression post lengths shown in schedule are for calculation purposes only. Framer is responsible for actual post lengths.
- 2. These Posts are in addition to post counts on Plans.
- 3. Sill Plates are Douglas Fir-Larch Grade #2 or better.
- 4. Compression Posts are Douglas Fir-Larch Grade #2 or better.

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### AutoTight® Holdown Systems

by Commins Manufacturing

### Compression Post Schedule 6x Wall

# Tree Farm

Z	Run Name	EW	2ab	EV	V6	EW	6.5	NS	B1	NS	B2	NS	C1	NS	C2	NS	SD	NS	SE	NS	C.3
Š	Wall Size	6x V	Vall	6x V	Vall	6x V	Vall	6x \	Vall	6x V	Vall	6x \	Vall	6x \	Vall	6x V	Vall	6x V	Vall	6x V	Vall
٦	Post Location	Outer	Inner																		
	Post Size	2x6			2x6	2x6															
ധ	Post Qty	2	5	2	8	2	4	2	6	2	7	2	4	2	3			2	10		
<u>a</u>	Post Length inches	54.	00	54.	00	54.	00	54.	.00	54.	.00	54.	.00	54.	00			54.	00		
2	Required Load kips	33.	.80	48.	54	26.	57	38.	.82	41.	.58	26.	.95	24.	55			57.	55		
اتـا	Allowable Load kips	36.	.09	51.	56	30.	94	41.	.25	46.	.40	30.	.94	25.	78			61.	87		
	Limiting Failure Mode	Crus	hing			Crus	hing														

	Post Size	2x6 2x6	2x6																	
12	Post Qty[	2 8	2	12	2	6	2	7	2	9	2	6	2	6	2	5	2	15	2	3
e	Post Length inches	137.88	137	.88	137	.88	137	.88	137	.88	137	.88	137	.88	54.	00	137	.88	54.	.00
2	Required Load kips	51.52	72.	18	40.	50	43	.29	55.	91	41.	.07	37.	42	31.	19	83.	50	21.	.80
Ľ	Allowable Load kips	51.56	72.	18	41.	25	46	.40	56.	72	41.	.25	41.	25	36.	09	87.	65	25.	.78
	Limiting Failure Mode	Crushing	Crus	hing																

#### Notes:

- 1. Posts may be arranged as desired by the builder as long as:
  - a. The total post quantity is the same as or greater than the quantity listed here.
  - b. And there is at least 1 post on each side of each rod.
  - c. Compression post lengths shown in schedule are for calculation purposes only. Framer is responsible for actual post lengths.
- 2. These Posts are in addition to post counts on Plans.
- 3. Sill Plates are Douglas Fir-Larch Grade #2 or better.
- 4. Compression Posts are Douglas Fir-Larch Grade #2 or better.

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AutoTight® Holdown Systems

by Commins Manufacturing

# AutoTight® By Commins Manufacturing

# Materials and References

Catalog Pages for:
AT Shrinkage Compensation Device
Rod
Bearing Plates
Coupler Nuts
Reducer Couplers
Nuts and Washers

ICC - Evaluation Service Report ESR-1344

COLA Report RR-25480

Commins Manufacturing Comminsmfg.com 360-378-9484

### **Commins Manufacturing Inc.**

360-378-9484



### AutoTight^® Rod

AutoTight uses a continuous threaded rod. Typical lengths are 2', 3', 6', 10', and 12'. Field cut if needed. Rod may be ordered custom cut with sufficient lead time.

Material Identification: R (Rod) + Dia. (1/8's of an inch) + Alloy

**Examples:** R5-A307 = 5/8"-11 NC threaded rod, ASTM A307 Steel (Standard Strength) R9-B7 =1-1/8"-7 NC threaded rod. ASTM A193-B7 Steel (High Strength)

Finish: Standard Black or zinc plated. Optional Hot Dip Galvanized (HDG)

Note: HDG rod must be chased to fit standard nuts & couplers. Or use special nuts and couplers.

**Diameter and Thread:** Rod is available from 1/2" (R4) to 2" (R16) diameter. Thread is Unified National Coarse (NC or UNC). Other sizes, material and lengths are available.

**Strength:** Rod Strength is per AISC 360 and ICC AC 391-3.2.1.1. Rod strength and elongation are identical for all suppliers (per AISC 360). **Some suppliers overstate strength and understate elongation. Please check!** 

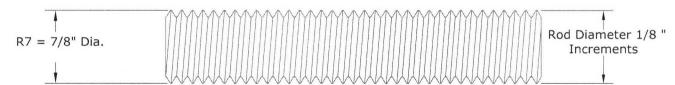
**Elongation:** Elongation for each (10') rod is shown at the maximum allowable tension load per ICC AC 391-3.2.1.1, Eq. 1. Adjust elongation based: on design load and distance between reaction points.

Code Acceptance: Tensile Values per IBC 2012, IBC 2009, IBC 2006 And AISC 360 13th edition.

### **Rod Basics**

**Rod** is specified by grade, diameter and length.

**Rod diameter** is specified by the diameter in  $\frac{1}{2}$  increments. A  $\frac{7}{8}$  diameter rod is specified as R7.



### **Calculating Elongation**

Both rod <u>strength</u> **and** <u>elongation</u> are critical to shear wall performance. Lower rod elongation results in lower shear wall drift and better performance. Rod is a major contributor to total system elongation. The fastest manual method of determining rod strength and elongation is to use a rod table and adjust to actual conditions.

When using a rod table: 1. select the rod for strength; 2. calculate rod elongation at the required load and rod length. 3. compare the elongation to requirements. 4. increase rod diameter to reduce elongation.

**Example:** Required Strength 11 kips. Floor Height (carpet-to-carpet) 11' - 4" (136").

**Solution:** #1 A307 Rod. Select an R7-A307 Rod from the AutoTight Rod table. This is a  $\frac{7}{8}$ "Ø A307 rod with a Strength Capacity = 13,530 pounds, Elongation = 0.121" (for a 10' (120") length). Calculated adjusted elongation: = 11,000/13,530 \* 136"/120" \* 0.121" = **0.1115**"

**Solution:** #2 **B7 Rod.** Select an R5-B7 Rod from the AutoTight Rod table. This rod is 5/8"Ø- B7 rod with a Strength Capacity = 14,380 pounds, Elongation = 0.263" for a 10' (120") length. Calculate adjusted elongation = 11,000/14,380 \* 136"/120" \* 0.263" = **0.2280**"



### AutoTight Rod (ASD Allowable Load per AISC 360)

		Rod Size & Alloy	A3	07	Rod Size & Alloy	F1554 G	rade 55
ngth	Diameter & Thread	Model	Allowable Tension (lb)	Elong in per 10'	Model	Allowable Tension (lb)	Elong in per 10'
E I	1/2"-13 UNC	R4-A307	4,418	0.129	R4-G55	5,522	0.161
9	5/8"-11 UNC	R5-A307	6,903	0.126	R5-G55	8,629	0.158
St	3/4"-10 UNC	R6-A307	9,940	0.123	R6-G55	12,425	0.154
0	7/8"-9 UNC	R7-A307	13,530	0.121	R7-G55	16,912	0.152
a	1"-8 UNC	R8-A307	17,672	0.121	R8-G55	22,089	0.151
פ	1-1/8"-7 UNC	R9-A307	22,365	0.121	R9-G55	27,957	0.152
a	1-1/4"-7 UNC	R10-A307	27,612	0.118	R10-G55	34,515	0.147
Sta	1-3/8"-6 UNC	R11-A307	33,410	0.120	R11-G55	41,763	0.150
	1-1/2"-6 UNC	R12-A307	39,761	0.117	R12-G55	49,701	0.146
	1-3/4"-5 UNC	R14-A307	54,119	0.118	R14-G55	67,649	0.147
	2"-4.5 UNC	R16-A307	70,686	0.117	R16-G55	88,357	0.146

		& Alloy	C10	045	& Alloy	A193-B7, F1	1554 Gr 105
	Diameter & Thread	Model	Allowable Tension (lb)	Elong in per 10'	Model	Allowable Tension (lb)	Elong in per 10'
th	1/2"-13 UNC	R4-C1045	8,836	0.258	R4-B7	9,204	0.268
ng	5/8"-11 UNC	R5-C1045	13,806	0.253	R5-B7	14,381	0.263
ē	3/4"-10 UNC	R6-C1045	19,880	0.246	R6-B7	20,709	0.256
Sti	7/8"-9 UNC	R7-C1045	27,059	0.242	R7-B7	28,187	0.253
	1"-8 UNC	R8-C1045	35,343	0.241	R8-B7	36,816	0.251
gh	1-1/8"-7 UNC	R9-C1045	44,731	0.242	R9-B7	46,595	0.253
Ī	1-1/4"-7 UNC	R10-C1045	55,223	0.236	R10-B7	57,524	0.246
	1-3/8"-6 UNC	R11-C1045	66,820	0.239	R11-B7	69,604	0.249
	1-1/2"-6 UNC	R12-C1045	79,522	0.234	R12-B7	82,835	0.244
	1-3/4"-5 UNC	R14-C1045	108,238	0.236	R14-B7	112,748	0.246
	2"-4.5 UNC	R16-C1045	141,372	0.234	R16-B7	147,262	0.244

Super Strength

		Rod Size & Alloy
•	Diameter & Thread	Model
	1-1/8"-7 UNC	R9-A654BD
	1-1/4"-7 UNC	R10-A654BD

	Rod Size & Alloy	A354 BD				
	Model	Allowable Tension (lb)	Elong in per 10'			
1	R9-A654BD	55,910	0.303			
	R10-A654BD	69,030	0.295			



High strength rod is typically identified with a high strength mark. The actual identification varies by specific supplier. Consult factory for more information.

#### Notes:

1. Material Properties: (Other grades available, consult factory)

ASTM A307 Fu = 60, Fy = 43 ksi. ASTM F1554 Gr. 55, Fu=75, Fy =55 ksi. ASTM A108-C1045 Fu = 120, Fy = 92 ASTM A193-B7, Fu=125, Fy=105 ksi. ASTM F1554 Gr. 105, Fu=125, Fy=105 ksi. ASTM A354-BD Fu = 150, Fy = 130 ksi.

2. Strength P = 0.75 x Fu x nominal area / 2 Per AISC 360 13th ed Table 7.2, pg. 7-2, P16.1-108 Eqn J3-1

3. Stress increase not allowed with AISC 13th Ed capacities. (IBC 2006 & later)

4. Rod stretch calculated per AC391 3.2.1.1 as follows:

 $\Delta$ Rod = PL/AnE where: P=Load, L=length, An=0.7854 (D-0.9743/n)^2,

D = nominal rod dia, n = threads per inch, E = elastic modulus = 29,000,000.

Table elongation is 10' rod at allowable load. Depending on jurisdiction stretch limit may be 1/8", 0.179", 0.200", or not specified. Elongation of other length rods may be calculated from this table by length ratio.

5. Large Ø rod (1-3/8" to 2" Ø) used for stretch reduction. Consult factory for advice before using.

6. Tabulated allowable loads are ASD for IBC 2006, 2009 & 2012, CBC 2007 & 2010, OSSC 2007 & 2010, LABC 2008 & 2011.

7. LRFD Strengths are 1.5 x ASD Allowable Loads.

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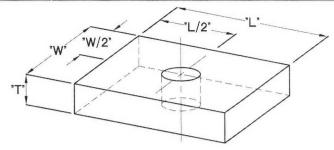
360-378-9484



### **Bearing Plates**

Bearing plates distribute compression loads into the structure at reaction points. AutoTight plates exceed the flexural requirements of AISC 360 and the wood-bearing requirements of the 2005 NDS. (ICC ES AC391 Sect 1.4.6, July 1, 2010)

Per 2005 NDS, plates deflect 0.040 inch at the compressive design value with a linear load deformation. (ICC ES AC 391 section 3.2.1.2).



### **Determining Compression Deflection**

AutoTight bearing plates provide a maximum deformation of 0.040" at rated the capacity. To select:

- 1. Determine the reaction load.
- 2. Select the smallest plate that can carry the reaction load.

  Check for: Bearing Capacity, Width (wall fit 4X or 6X Wall) and rod fit.
- 3. The wood deformation at the actual load is linear.

  With the load-deformation at the design load = 0.040" \* design load / rated load.

### Example:

Reaction is 11,000 pounds on Douglas Fir. Rod is  $1-\frac{1}{8}$ " Ø. Select an S11-1- $\frac{1}{4}$ " bearing plate with a rated capacity of 11,948 pounds.

Actual deformation (per AC 391, section 3.2.1.2 ) is 0.040 \* 11,000 / 11,948 = 0.037" For system deformation add the 0.037 to the rod and shrinkage compensator deformation.

### **Minimizing Total Deformation**

To lower deformation increase the size of the bearing plate.

### Example:

Reaction load is 11,000 pounds on Douglas Fir.

If an L20-1- $\frac{1}{4}$ " plate is selected, the plate deformation will be as follows:

Actual deformation will be 0.040 \* 11,000 / 21,016 = 0.021"

Changing the bearing plate is one method to adjust the total deflection (elongation) to achieve a tight system.

This example shows how to manually adjust components to achieve a desired deflection. The AutoTight Software allows for a fast, easy change of rod, bearing plates or shrinkage compensators to achieve the the required system deflection.

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### 360-378-9484



### **Bearing Plates**

Bearing Plates load the structure at reaction points. Bearing loads are limited by wood crushing at the NDS allowable wood bearing capacity.

Material:

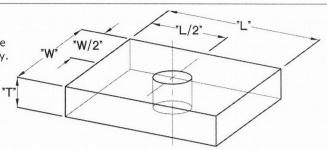
Complies with ASTM A36

Identification:

Plates or boxes marked with Part #.

Efficiency tip: Minimize the number of sizes used on any single job,

i.e. Keep it Simple.



SS	_	Bearing P	lates						
Wall	Typical Use	8	Best	Best	Max	Allowable Load (Cross Grain Crushing)			
Wall Thickness		Model No.	Sizes	TxWxL	Rod Ø	DFL @ 625	SYP @ 565	HF @ 425	SPF @ 405
		S5 -5/8"		1/4" x 3" x 3"	5/8	5,964	5,391	4,055	3,864
	₩	S5 -3/4"	***	1/4" x 3" x 3"	3/4	5,964	5,391	4,055	3,864
	AT (	For 1/2" throu	gh 1" R	od					
	and /	S7 -1"	***	3/8" x 3-1/2" x 3-1/2"		7,863	7,108	5,347	5,095
2	a n	S10 -1"	***	1/2" x 3-1/4" x 5"		10,322	9,331	7,019	6,689
6X walls	75	S11 -1"	***	1/2" x 3-1/2" x 5-1/2"	1"	11,948	10,801	8,125	7,742
	AT	S14 -1"		3/4" x 3-1/4" x 7"		13,665	12,353	9,292	8,855
•ర		S16 -1"		1" x 3-1/4" x 8"		15,696	14,189	10,673	10,171
4x	r 100 & 125	For 3/4"- 1-1/4" Rod							
Fit		S7 -1-1/4"	***	3/8" x 3-1/2" x 3-1/2"		7,540	6,816	5,127	4,886
		S10 -1-1/4"	***	1/2" x 3-1/4" x 5"	1-1/4"	10,009	9,048	6,806	6,486
		S11 -1-1/4"	***	1/2" x 3-1/2" x 5-1/2"		11,948	10,801	8,125	7,742
		S14 -1-1/4"		3/4" x 3-1/4" x 7"		13,373	12,089	9,094	8,666
	AT	S16 -1-1/4"		1" x 3-1/4" x 8"		15,404	13,926	10,475	9,982
	100	L18 -1-1/4"	***	1/2" x 5.5" x 5.5"		19,292	17,440	13,119	12,501
	ΙĒ	L20 -1-1/4"	***	5/8" x 5-1/2" x 6"	1-1/4"	21,016	18,998	14,291	13,618
S	AT.	L25 -1-1/4"		3/4" x 5-1/2" x 7-1/2"		24,936	22,542	16,956	16,158
SW8	ν 2	L30 -1-1/4"		1" x 5-1/2" x 9"		30,092	27,203	20,462	19,500
<u> </u>	AT125	L33 -1-1/4"		1-1/8" x 5-1/2" x 10"		33,529	30,311	22,800	21,727
>	4	L37 -1-1/4"		1-1/4" x 5-1/2" x11"		36,967	33,418	25,137	23,955
rge		For 1-3/8", 1-	1/2", 1-3	3/4" and 2" Rod					
<u>a</u>		L18 -2"	***	1/2" x 5.5" x 5.5"		17,965	16,240	12,216	11,641
and larger wallswalls	Only	L20 -2"	***	5/8" x 5-1/2" x 6"		19,695	17,805	13,393	12,763
9 х9	0	L25 -2"		3/4" x 5-1/2" x 7-1/2"	2"	23,693	21,419	16,111	15,353
Fit 6	200	L30 -2"		1" x 5-1/2" x 9"	2	28,849	26,080	19,618	18,694
ш	₽	L33 -2"		1-1/8" x 5-1/2" x 10"		32,287	29,187	21,955	20,922
		L37 -2"		1-1/4" x 5-1/2" x11"		35,724	32,295	24,293	23,149

Notes: Plate ID includes maximum rod diameter. Holes are 1/16" oversize.

Bearing Plate bending based on ASTM A36 Steel, Fy = 36 ksi. per AISC 13th ed.

Bearing Capacity per NDS 2005: DFL = 625, SP = 565, HF = 405, SPF = 425 psi.

Bearing area factor, Cb, included in listed capacities.

Allowable bearing capacity is not limited by plate bending. Deflection is 0.040" at Allowable Load.

Allowable Capacity = (Fc perp) \* Bearing Area \* Bearing Factor (per AC 391 3.2.1.2 May 2012)

S5, S7, S10 and L18 plates may be used on the first floor mudsill for end of wall connection.

Finish: S5, S7, L11 and L18 plates are HDG. All other are black iron except as noted.

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360-378-9484



Shrinkage compensators require evaluations for: fit, strength, expansion and deflection. Two code defined deflections ( $\triangle A$ ) and ( $\triangle R$ ) are required.

**Load-deflection** ( $\Delta A$ ) design load/actual load \* Rated  $\Delta A$ . **Delta R** ( $\Delta R$ ) is always added in full to system deflection. Delta R is the product internal slack.

### **Example:**

Reaction Load = 11,000 pounds

Shrinkage Compensator AT 100 (Select based on the rod size)

Rated Capacity: 25,300 pounds.

Deflection Maximum:  $\Delta A = 0.032$ ",  $\Delta R = 0.002$ "

Expansion 1.2" (ICC ESR 1344)

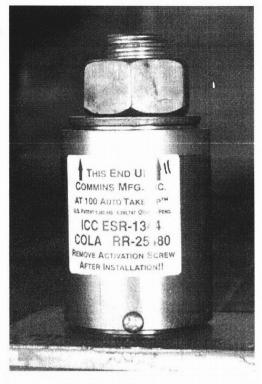
Calculate Deflection: Load Deflection = 0.032 \* 11,000/25,300 = 0.014"

Delta R ( $\Delta$ R) (From Table) = 0.002

Total Deformation = 0.016"

Add sum to the system elongation per AC 316 and AC 391 section 3.1.1.

Want to know more? Watch a 2 minute video that explains  $\Delta \mathbf{R}$  on our website.



US Patents 6,390,747 6,585,469. Other patents foreign and domestic, pending

### AutoTight:

Rod Sizes to 2" Dia! Larger rod = Lower Deflection

Inside Spring

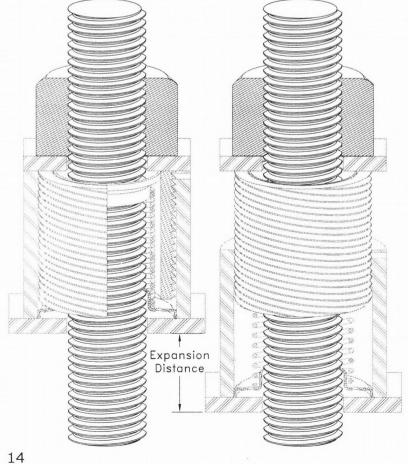
= Protected Mechanism

Special thread

= 60% Lower Deflecton

**Tightest Systems** 

= Shear Wall Performance



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The AutoTight shrinkage compensator automatically expands as the building shrinks and settles.

This expansion helps keep shear walls tight and performing to the code.

Code Listed: ICC ESR-1344, COLA RR-25480, Tested to AC 316 & AC 391, IBC 2012 Rated

Material: Aluminum - 6061 Alloy, Finish: Light Oil

**Steel** - 12L14,

Finish: Zinc chromate, moly disulfide lubricant.

Installation: Place a steel bearing plate over the rod and onto the wood

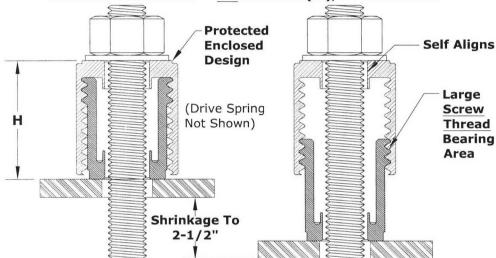
Place the AT over the rod and onto the bearing plate,

Place Washer over the rod and onto the AT, Install and tighten Nut,

Remove the activation screw.

Listen for release

Threaded Mechanism = NO Backlash ( $\Delta r$ ), No Looseness!



High Capacity, NO Backlash,

"Floating" Take-Up Device = Jam resistant
Tested at 3°out-of-plumb. (3° = 6-1/4" in 10 feet.)
Stackable: Doubles Expansion to 5"

Tested to 3 times rated load.

Fully functional at  $2-\frac{1}{2}$  times rated load



US Patents 6,390,747 6,585,469. Other patents foreign and domestic, pending

### No Backlash with AutoTight =

### **Much Better Shear Wall Performance**

Some shrinkage compensators use ratchets. These ratchets can introduce looseness (backlash) up to  $\frac{3}{16}$ ".

This looseness can reduce the shear wall capacity by 40%.

See Videos at www.comminsmfg.com

	Model Number			Dimensions (Inches)		Rated Allowable Take-Up Load	Average Ultimate	Seating Increment	Deflection at Allowable			
- 1		Diameter		Dia.	Н	(Inches)	Pounds	Pounds	∆ <sub>R</sub> *	Load ∆ <sub>A</sub> "		
New	AT4A-1.5	1/2"	E	1-1/2"	3"	1-1/2"	6,450	6,450 24,857		0.011		
New	AT4A-2.5	3/4"	<sup>72</sup> <u>⊇</u> 1-1/2 4-1/16" 2-1/2"	0,430	24,037	0.000"	0.011					
New	AT6A-1.5		3/4"	Aluminum	2-1/8"	3-3/16"	1-1/2"	10,550	40,737	0.000	0.011	
New	AT6A-2.5			5/4	3/4	3/4	₹	2-1/0	4-3/16"	2-1/2"	10,550	40,707
-	AT 75	3/4"	3/4"		2"	3"	1.10"	16,450	50,533		0.024	
[	AT 75-2.5			3/4	_	2"	4"	2-1/2"	15,183	54,728		0.020
	AT 100	1"	Steel	2-1/4"	3-1/8"	1.10"	25,300	78,067	0.002"	0.032		
	AT 125	1-1/4"	S	2-3/4"	3-1/8"	1.12"	34,500	104,683		0.016		
New	AT 200-2.0	2"		4"	3-3/4"	2.25"	50,000	150,000		0.024		

Note:  $\Delta_R$ = Average Travel and Seating Increment is the "Lost Motion" with device direction change from advancing to load resistance. This is sometimes called "Backlash".

<sup>\*</sup>The AutoTight Aluminum Shrinkage Compensator has 0.0002" backlash ( $\Delta_r$ ).

# Partie Land Control of the Partie Land Line

### **Coupler Nuts**

Coupler nuts connect threaded rod to form a continuous rod system.

Straight couplers have the same thread on both ends.
Coupler Nut Reducers have different diameter threads on each end.

Thread pitch is Unified National Coarse (NC or UNC). Coupler nuts are available to fit rod from 1/2"-13 through 2"-4.5 NC.

Tal		1:4	ica	4:	-	-	
10	en		I Ca	ш	O	п	:

**Straight Coupler:** Example CN-9

CN = Coupler Nut,

9 = rod Size in  $\frac{9}{8}$  inch =  $1-\frac{1}{8}$ " dia.

Grade: Standard Coupler Nuts are ASTM A563 Grade A Grade 2

High Strength Couplers are ASTM A563 Grade C

Over  $1-\frac{3}{8}$ " are Grade 5

Sighted couplers have one or more holes drilled to aid installation.

### Installation:

Thread coupler onto rod until the rod can be seen in the sight hole. Thread the next rod until it can also be seen through the sight hole. A nail inserted into the sight hole can be used for a temporary stop.

Note: Full strength is achieved with thread engagement equal to a standard nut. This is typically one rod diameter

### **Options:**

Oversize threads in coupler nuts for use with galvanized rod are available. To specify add a suffix after the product. Example CN-6 FHDG. This provides an oversize end to fit HDG rod. Contact factory for details.

#### Code Acceptance:

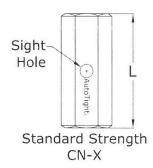
Nuts and coupler nuts shall be grade compatible and conform to ASTM A563 and IFI-128. One or two sight holes are provided to assist installation. Standard strength couplers shall be used with ASTM A307 and equivalent rod; High strength couplers shall be used with ASTM C1045, ASTM A193-B7 and other high strength rod. High strength couplers may be used with standard strength rod. See ICC ES AC 391 section 1.4.5 for additional information.

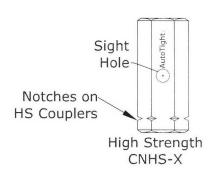
Coupler elongation is minimal and is not considered in elongation calculations.

Standard Couplers				
Model Number	Rod Ø			
Woder Number	Both Ends			
CN-4	1/2"			
CN-5	5/8''			
CN-6	3/4"			
CN-7	7/8"			
CN-8	1"			
CN-9	1-1/8"			
CN-10	1-1/4"			

<b>High Strengt</b>	h Coupler		
Model Number	Rod Ø Both Ends		
CNHS-5	5/8"		
CNHS-6	3/4"		
CNHS-7	7/8"		
CNHS-8	1"		
CNHS-9	1-1/8"		
CNHS-10	1-1/4"		
CNHS-11	1-3/8"		
CNHS-12	1-1/2"		
CNHS-14	1-3/4"		
CNHS-16	2"		







<sup>\*</sup> Check with factory for availability of these sizes.

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360-378-9484



### **Coupler Nut Reducer**

Use coupler nut reducers to change rod size. Normally rod is reduced in size. However sometimes the rod is increased from an embedment to a "run".

#### **Identification:**

### **Coupler Nut Reducer**

Example: CNR610
CNR = Coupling Nut Reducer,

610 = 3/4" - 10 NC to 1-1/4" - 7 NC Thread.

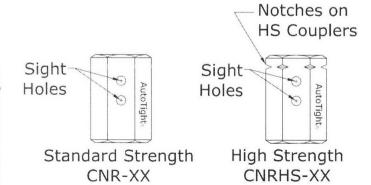
#### Grade:

Standard Coupler Nuts are ASTM A563 Grade A. High strength Couplers are ASTM A563 Grade C. Over  $1-\frac{1}{4}$ " at the big end Grade 5 is supplied Sight holes are standard.

### Installation

Thread coupler onto larger rod, bottom. Thread smaller rod into coupler and bottom on the larger thread. The thread bottoming in the coupler will indicate full engagement, a sight hole is not necessary.

### Coupler Nut Reducer



	Model Number	Ro	d Ø	
	Model Mulliber	Small	Large	
	CNR-45		1/2"	
	CNR-46	1/2"	3/4"	
	CNR-47		7/8"	
	CN-48		1"	
4	CNR-56		3/4"	
ngtl	CNR-57	5/8"	7/8"	
Strength	CNR-58	3/8	1"	
S	CNR-59		1-1/8"	
5	CNR-67		7/8"	
Standard	CNR-68	3/4"	1"	
star	CNR-69	3/4	1-1/8"	
٠,	CNR-610		1-1/4"	
	CNR-78		1"	
	CNR-79	7/8"	1-1/8"	
	CNR-710		1-1/4"	
	CNR-89	1"	1-1/8"	
	CNR-810	1	1-1/4"	
	CNR-910	1-1/8"	1-1/4"	

	Model Number	Ro	d Ø
	Model Number	Small	Large
	CNRHS-56		3/4"
	CNRHS-57	5/8"	7/8"
	CNRHS-58	3/8	1"
	CNRHS-59		1-1/8"
	CNRHS-67		7/8"
	CNRHS-68	3/4"	1"
	CNRHS-69	3/4	1-1/8"
	CNRHS-610		1-1/4"
	CNRHS-78		1"
	CNRHS-79	7/8"	1-1/8"
	CNRHS-710		1-1/4"
	CNRHS-89		1-1/8"
gth	CNRHS-810	1"	1-1/4"
Strength	CNRHS-812 *		1-1/2"
S	CNRHS-814 *		1-3/4"
	CNRHS-910		1-1/4"
High	CNRHS-912 *	1-1/8"	1-1/2"
	CNRHS-914 *	1-1/6	1-3/4"
	CNRHS-916 *		2"
	CNRHS-1011 *		1-3/8"
	CNRHS-1012 *	1-1/4"	1-1/2"
	CNRHS-1014 *	1 1/4	1-3/4"
	CNRHS-1016 *		2"
	CNRHS-1112 *		1-1/2"
	CNRHS-1114 *	1-3/8"	1-3/4
	CNRHS-1116 *		2"
	CNRHS-1214 *	1-1/2"	1-3/4
	CNRHS-1216 *	1-1/2	2"
	CNRHS-1416 *	1-3/4"	2"

<sup>\*</sup> Check with factory for availability of these sizes.

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360-378-9484



### **Nuts**

All nuts are Unified National Coarse thread pitch (UNC or NC)

Standard Nuts are SAE Grade 2 or ASTM 563-Grade A

High Strength Nuts are SAE grade 5, ASTM 563-Grade C or A194-2H.



### **Nuts for HDG**

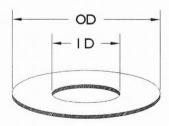
Oversize nuts to fit HDG Hot Dipped Galvanized Rod available. Consult factory for sizes available. Rethreading after HD Galvanizing is preferred.

SI	tandard Nuts
Model Number	Diameter & Thread
N-4	1/2"-13 NC
N-5	5/8"-11 NC
N-6	3/4"-10 NC
N-7	7/8"-9 NC
N-8	1"-8 NC
N-9	1-1/8"-7 NC
N-10	1-1/4"-7 NC
N-11	1-3/8"-6 NC
N-12	1-1/2"-6 NC
N-14	1-3/4"-5 NC
N-16	2"-4.5 NC

High S	trength Nuts
Model Number	Diameter & Thread
NHS-4	1/2"-13 NC
NHS-5	5/8"-11 NC
NHS-6	3/4"-10 NC
NHS-7	7/8"-9 NC
NHS-8	1"-8 NC
NHS-9	1-1/8"-7 NC
NHS-10	1-1/4"-7 NC
NHS-11	1-3/8"-6 NC
NHS-12	1-1/2"-6 NO
NHS-14	1-3/4"-5 NC
NHS-16	2"-4.5 NC

### **Washers**

Washers supplied are SAE Washers. Common Washers may be substituted. W-11 thru W-16 are special  $3-\frac{1}{2}$ " square washers.



	Washers	
Model Number	Nominal Diameter	Outside Diameter
W-4	1/2"	1-1/16"
W-5	5/8"	1-5/16"
W-6	3/4"	1-1/2"
W-7	7/8"	1-3/4"
W-8	1"	2"
W-9	1-1/8"	2-1/4"
W-10	1-1/4"	2-1/2"
W-11	1-3/8"	3-1/2"
W-12	1-1/2"	3-1/2"
W-14	1-3/4"	3-1/2"
W-16	2"	3-1/2"

<sup>\*</sup> Check with factory for availability of these sizes.



**Most Widely Accepted and Trusted** 

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**ESR-1344** 

Reissued 12/2017 This report is subject to renewal 12/2018.

DIVISION: 06 00 00—WOOD, PLASTICS AND COMPOSITES SECTION: 06 05 23—WOOD, PLASTIC, AND COMPOSITE FASTENINGS

### **REPORT HOLDER:**

### COMMINS MANUFACTURING, INC.

960 B GUARD STREET FRIDAY HARBOR, WASHINGTON 98250

### **EVALUATION SUBJECT:**

### AT AUTOMATIC TAKE-UP™ SHRINKAGE COMPENSATOR



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### **ICC-ES Evaluation Report**

ESR-1344

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DIVISION: 06 00 00—WOOD, PLASTICS AND COMPOSITES

Section: 06 05 23—Wood, Plastic, and Composite Fastenings

#### REPORT HOLDER:

COMMINS MANUFACTURING, INC. 960 B GUARD STREET FRIDAY HARBOR, WASHINGTON 98250 (360) 378-9484 www.comminsmfg.com

#### **EVALUATION SUBJECT:**

### AT AUTOMATIC TAKE-UP™ SHRINKAGE COMPENSATOR

#### 1.0 EVALUATION SCOPE

Compliance with the following codes:

2018, 2015, and 2012 International Building Code® (IBC)

#### Property evaluated:

Structural

### 2.0 USES

The AT Automatic Take-Up™ Shrinkage Compensator device is used to remove slack in hold-down systems due to settlement or wood shrinkage in accordance with IBC Sections 2303.7 and 2304.3.3.

### 3.0 DESCRIPTION

#### 3.1 General:

The AT Automatic Take-Up™ Shrinkage Compensator is a self-expanding washer used in connections of shearwall hold-down connectors or tension tie connectors incorporating threaded rods or threaded anchor bolts. The shrinkage compensator is available with either a steel body or an aluminum body. The devices automatically expand, axially, to eliminate any gaps between the bearing surface and the nut on the threaded rod that occur due to settlement or wood shrinkage. Sizes, rod diameters, dimensions, maximum expansion (shrinkage compensation capacity), and capacities are listed in Table 1. See Figure 1 for a typical installation.

#### 3.2 Materials:

3.2.1 Auto Take-Up Device (AT Steel and ATA Aluminum): Steel AT's: The outer (body) component of

the device has internal threads. The inner (stud) component of the device has matching external threads. The inner components are manufactured from ASTM A108-13 Grade 12L14 steel with minimum yield and tensile strengths of 65 and 75 ksi (448 and 517 MPa), respectively. The outer components are manufactured from either ASTM A108-13 Grade 12L14 steel with minimum yield and tensile strengths of 65 and 75 ksi (448 and 517 MPa), respectively, or DOM 1020/1028 steel tubing with minimum yield and tensile strengths of 84 and 95 ksi (579 and 657 MPa), respectively, for the AT75-2.5, and 71 and 80 ksi (490 and 551 MPa), respectively, for all the other AT devices. For the AT200-2 the outer and inner components are manufactured from ASTM A513-15 Grade 1026 steel with minimum yield and tensile strengths of 75 and 85 ksi (517 and 568 MPa) respectively. A finish and lubricant, specified in the approved quality control manual, is applied to the outer and inner components to resist corrosion. The device has an internal spring manufactured from HDMB steel wire per ASTM A764-07(2017) or highcarbon steel music wire per ASTM A228-16.

**3.2.2** Aluminum AT's: The outer (body) component of the device has internal threads. The inner (stud) component of the device has matching external threads. The outer and inner components are manufactured from 6061-T6 aluminum with minimum yield and tensile strengths of 40 and 45 ksi (275 and 310 MPa), respectively. A lubricant, specified in the approved quality control manual, is applied to the outer and inner components to resist corrosion. The device has an internal spring manufactured from HDMB steel wire per ASTM A764-07(2017) or high-carbon steel music wire per ASTM A228-16.

### 4.0 DESIGN AND INSTALLATION

#### 4.1 Design and Allowable Loads:

The allowable compression loads for the AT Automatic Take-Up<sup>TM</sup> Shrinkage Compensator designed under allowable stress design are as shown in Table 1. The devices are to be used where the expected shrinkage does not exceed the expansion limit of the devices. Two devices may be used in-line where the expected shrinkage exceeds the expansion limit of one device.

When the devices are used in continuous rod systems that resist light-frame shear wall overturning forces, calculations must be submitted to the code official confirming that the total vertical displacement, which would include steel rod elongation and the shrinkage compensating device deflection, is less than or equal to

0.20-inch (5 mm) for each story, or between restraints, whichever is more restrictive, using allowable stress design (ASD). Shear wall drift limit calculations must consider the 0.20-inch (5 mm) vertical displacement limit. This 0.20-inch (5 mm) vertical displacement limit may be exceeded when it can be demonstrated that the shear wall story drift limit and the deformation compatibility requirements of IBC Section 1604.4 are met when considering all sources of vertical displacement.

#### 4.2 Installation:

The AT Automatic Take-Up™ Shrinkage Compensator must only be used where there is sufficient clearance along the sides of the device to permit the device to expand. The device must be installed over the hold-down or bearing plate with the threaded rod through the axial center of the device. An SAE flat washer and steel nut must be installed on the threaded rod and tightened prior to activation of the device. Activation occurs by removal of a factory-inserted screw from the side of the device. The continuous tie-down system in which the AT Automatic Take-Up™ Shrinkage Compensator is used must be installed plumb, such that the offset angle between the top of the floor and the bottom of the top plates or bridge block above does not exceed 1.33 degrees from vertical.

#### 5.0 CONDITIONS OF USE

The AT Automatic Take-Up™ Shrinkage Compensator described in this report complies with, or is a suitable alternative to what is specified in, those codes listed in Section 1.0 subject to the following conditions:

5.1 Calculations, demonstrating that the applied loads do not exceed the allowable loads and that the expected shrinkage does not exceed the expansion limits of the device, must be submitted to the code official for approval. The calculations must be prepared by a registered design professional where required by the statutes of the jurisdiction in which the project is to be constructed

- 5.2 The Commins AT Automatic Take-Up™ Shrinkage Compensator must be limited to installations in dry, interior locations
- 5.3 No increase in allowable stresses or loads for duration of load is permitted for the Commins AT Automatic Take-Up™ Shrinkage Compensator.
- 5.4 The AT Automatic Take-Up<sup>™</sup> Shrinkage Compensator must not be used to support dead load other than its own weight.

### 6.0 EVIDENCE SUBMITTED

Data in accordance with ICC-ES Acceptance Criteria for Shrinkage Compensating Devices (AC316), dated June 2013 (editorially revised November 2017).

#### 7.0 IDENTIFICATION

Each AT Automatic Take-Up™ Shrinkage Compensator must bear a label on the device or on the packaging indicating the manufacturer's name (Commins Manufacturing, Inc.), the model number, and the evaluation report number (ESR-1344).

TABLE 1—AT AUTOMATIC TAKE-UP™ SHRINKAGE COMPENSATOR DESCRIPTION AND ALLOWABLE LOADS<sup>1,3</sup>

MODEL	INSIDE DIAMETER	OUTSIDE DIAMETER	DEVICE LENGTH (inches)		MAXIMUM EXPANSION	SEATING INCREMENT <sup>2</sup>	ALLOWABLE AXIAL COMPRESSION	DEFLECTION AT ALLOWABLE
NO.	(inches)	(inches)	Minimum	Maximum	(inches)	Δ <sub>R</sub> (inches)	LOAD P <sub>A</sub> (pounds)	LOAD <sup>2</sup> Δ <sub>A</sub> (inch)
				-	Aluminum			
AT 4A-1.5	1/2	11/2	3.0	4.5	1.50	0.000	6,450	0.011
AT 4A-2.5	1/2	1 <sup>1</sup> / <sub>2</sub>	4.06	6.56	2.50	0.000	6,450	0.011
AT 6A-1.5	3/4	2 <sup>1</sup> / <sub>8</sub>	3.19	4.69	1.50	0.000	10,550	0.011
AT 6A-2.5	3/4	21/8	4.19	6.69	2.50	0.000	10,550	0.011
AT 8A-1.5	1	23/4	3.50	5.25	1.75	0.000	20,750	0.004
AT 10A-1.5	11/4	31/4	3.50	5.12	1.62	0.000	28,050	0.020
AT12A-1.5	11/2	31/4	3.50	5.12	1.62	0.000	28,050	0.020
AT16A-2.0	2	4	3.50	5.57	2.07	0.001	39,450	0.011
					Steel		•	
AT 75	3/4	2	2.80	3.90	1.10	0.002	16,450	0.024
AT 75-2.5	3/4	2	4.0	6.5	2.50	0.002	15,200	0.021
AT 100	1	21/4	2.90	4.00	1.10	0.002	25,300	0.032
AT 125	11/4	2 <sup>3</sup> / <sub>4</sub>	2.86	3.98	1.10	0.002	34,500	0.016
AT 200-2.0	2	4	3.88	6.06	2.18	0.000	83,200	0.009

For SI: 1 inch = 25.4 mm, 1 pound = 4.45 N.

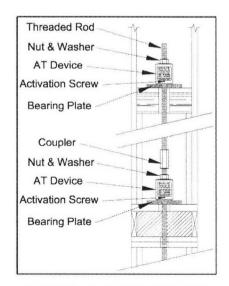


FIGURE 1—TYPICAL INSTALLATION

<sup>&</sup>lt;sup>1</sup>Listed values are for the AT Automatic Take-Up™ Shrinkage Compensator only. All other components in the system must be designed in accordance with the applicable code.

<sup>&</sup>lt;sup>2</sup>The device average travel and seating increment,  $\Delta_R$ , and deflection at allowable load,  $\Delta_A$ , are additive and describe the total movement of the device at allowable load,  $\Delta_T$ . For design loads,  $P_D$ , less than the allowable load,  $P_A$ , the total movement of the device,  $\Delta_T$ , is calculated as follows:  $\Delta_T = \Delta_R + \Delta_A(P_D/P_A)$ .

<sup>&</sup>lt;sup>3</sup>LRFD resistance capacity = ASD allowable load x 1.5.



### **ICC-ES Evaluation Report**

### **ESR-1344 CBC Supplement**

Reissued December 2017 Revised February 2018 This report is subject to renewal December 2018.

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### **EVALUATION SUBJECT:**

#### AT AUTOMATIC TAKE-UP™ SHRINKAGE COMPENSATOR

#### 1.0 REPORT PURPOSE AND SCOPE

#### Purpose:

The purpose of this evaluation report supplement is to indicate that the AT Automatic Take-Up™ Shrinkage Compensator, recognized in ICC-ES master report ESR-1344, has also been evaluated for compliance with the code noted below.

### Applicable code edition:

2016 California Building Code (CBC)

### 2.0 CONCLUSIONS

The AT Automatic Take-Up™ Shrinkage Compensator, described in Sections 2.0 through 7.0 of the master evaluation report ESR-1344, complies with CBC Chapter 23, provided the design and installation are in accordance with the 2015 International Building Code® (IBC) provisions noted in the master report and the additional requirements of with CBC Chapters 16, 16A, 17, 17A and 23, as applicable.

This supplement expires concurrently with the master report, reissued December 2017 and revised February 2018.



RUN START (CONCRETE, WOOD BEAM, STEEL BEAM)

Anchor Cumulative Tension Load (kips) **Cumulative Compression Load (kips)** Wall or Run Wall Height (ft-in) Floor Depth (inches) Run Run Start Diameter ID Termination 5th (in.) 6th 4th 3rd 2nd 1st 6th 5th 4th 3rd 2nd 1st 8th 5th Ath 3rd 2nd 1st 6th 5th 4th 3rd 2nd EW 2a 20.3 34.51 33.8 51.52 12'-1/8'12'-1/8" Concrete Through Slab SR12 11.88 11.88 Straps EW 2b Concrete Through Slab SR12 20.3 34.51 33.8 51.52 12'-1/8"12'-1/8" 11.88 11.88 Straps EW 6 SR10H 30.83 49.84 48.54 72.18 12'-1/8'12'-1/8" 11.88 11.88 Straps Concrete Through Slab 11.88 11.88 EW 6.5 SR9H 23.16 36.23 26.57 40.5 12'-1/8'12'-1/8" Straps Concrete Through Slab NS B1 Concrete Through Slab SR9H 38.82 39.52 29.06 43.39 12'-1/8'12'-1/8" 11.88 11.88 Straps 38.82 52.31 41.58 55.91 NS B2 Concrete Through Slab SR10H 12'-1/8'12'-1/8" 11.88 11.88 Straps NS C1 Concrete Through Slab SR9H 25.13 38.8 26.95 41.07 12'-1/8'12'-1/8" 11.88 11.88 Straps NS C2 21.8 | 33.99 24.55 37.42 12'-1/8"12'-1/8" 11.88 11.88 Straps SR10 Concrete Through Slab 12'-1/8'12'-1/8" NS D 26.9 31.19 11.88 11.88 Concrete Through Slab SR9 Straps NSE Concrete Through Slab SR12 28.63 46.96 57.55 83.5 12'-1/8'12'-1/8" 11.88 11.88 Straps Straps NS C.3 Concrete Through Stab SR8 15.06 21.8 12'-1/8'12'-1/8" 11.88

Tree Farm S702