Development Services

From Concept to Construction

Phone: 503-823-7300 Email: bds@portlandoregon.gov 1900 SW 4th Ave, Portland, OR 97201 More Contact Info (http://www.portlandoregon.gov//bds/article/519984)





APPEAL SUMMARY

Project Address: 1410 NW Johnson St
Appellant Name: Barry R Smith PC Architect
Appellant Phone: 503-295-6261
Plans Examiner/Inspector: Jody Orrison, Amit Kumar, Corey Stanley.
Stories: 4 Occupancy: F-2 Construction Type: III-B
Fire Sprinklers: Yes - NFPA 13 (Improvements Req'd)
LUR or Permit Application No.:
Proposed use: Factory Industry - Low Hazard

[File 4] [File 5]

APPEAL INFORMATION SHEET

Appeal item 1

Code Section	Section 1022 Interior Exit Stairways and Ramps, 1022.3.1 Extension
Requires	Where interior exit stairways and ramps are extended to an exit discharge or a public way by an exit passageway, the interior exit stairway and ramp shall be separated from the exit passageway by a fire barrier constructed in accordance with Section 707 or a horizontal assembly constructed in accordance with Section 711, or both. The fire-resistance rating shall be at least equal to that required for the interior exit stairway and ramp. A fire door assembly complying with Section 716.5 shall be installed in the fire barrier to provide a means of egress from the interior exit stairway and ramp to the exit passageway. Openings in the fire barrier other than the fire door assembly are prohibited. Penetrations of the fire barrier are prohibited.
Proposed Design	This factory building was granted occupancy December 30, 1908 and little or no improvements have been made since the original construction. The current owner [Seller] has occupied the building since the 1950's using it as an office building and print shop. Circulation and egress are constricted in the current configuration. Occupants have to travel through adjoin occupied spaces or through an enclosed stair to access tenant spaces. Door swing in the wrong direction and are redundant. The new Owner [Purchaser] wishes to simplify the enclosed stair to access the required two-hour fire resistive protection around the stairwell, correct the door swing and maneuvering distance condition and separate tenant access spaces by extending the stairwell footprint. (Fire Protection Engineer letters included for protection of existing heavy timber). Per Section 1022.2, the fire-resistive rating of the Interior Exit Stairway is required to be 2 hour as the stair is connecting four stories.

Building is equipped with an automatic sprinkler system and needs upgrading to current NFPA 13 standards. There are no combustible concealed attic spaces.

Where non-rated interior glass relite and doors are used, a 2HR rated fire curtain is provided (Tyco Model WS – 2HR Fire Barrier).

Stairwell protection will be extended to the basement.

RESPONSE: A Building Code appeal is required for substituting 2HR fire curtains in lieu of twohour fire resistive construction.

Reason for alternative The alternate gives the Owner flexibility to visually identify tenant access from egress components.

APPEAL DECISION

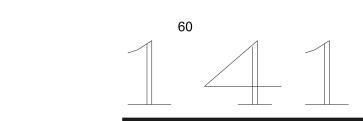
Extension of 2 hour fire rated stair enclosures: Granted provided Tyco Type WS sprinklers are installed per manufacturers specifications on the non-rated glazing, Non-glazed partitions are constructed as 2 hour fire barriers, doors are 2 hour fire rated assemblies and Type 13 sprinklers are installed throughout building.

Note: Char calculations will be reviewed as part of building permit review process.

Appellant may contact John Butler (503 823-7339) with questions.

The Administrative Appeal Board finds with the conditions noted, that the information submitted by the appellant demonstrates that the approved modifications or alternate methods are consistent with the intent of the code; do not lessen health, safety, accessibility, life, fire safety or structural requirements; and that special conditions unique to this project make strict application of those code sections impractical.

Pursuant to City Code Chapter 24.10, you may appeal this decision to the Building Code Board of Appeal within 180 calendar days of the date this decision is published. For information on the appeals process and costs, including forms, appeal fee, payment methods and fee waivers, go to www.portlandoregon.gov/bds/appealsinfo, call (503) 823-7300 or come in to the Development Services Center.



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GENERAL NOTES:

1. CONSTRUCTION SHALL COMPLY WITH ALL CODES AS ADMINISTERED BY THE AUTHORITIES HAVING JURISDICTION. ALL WORK SHALL CONFORM TO ORDINANCES OR REGULATIONS RELATING TO ENVIRONMENTAL POLLUTION AND PRESERVATION OF NATURAL RESOURCES.

2. THE CONTRACTOR SHALL BE RESPONSIBLE FOR MAINTAINING ALL BURIED SERVICES IN UNDAMAGED CONDITION DURING CONSTRUCTION. CONTRACTOR SHALL VERIFY UTILITY LOCATIONS AND CONNECTIONS.

3. CONTRACTOR SHALL INSURE ALL SCAFFOLDING, TEMPORARY FLOORS, ETC., FURNISHED BY HIMSELF OR SUBCONTRACTORS FOR INSTALLATION OF WORK TO BE BUILT AND MAINTAINED TO SAFELY SUPPORT REQUIRED LOADS. COMPLY WITH ALL APPLICABLE LOCAL SAFETY CODES AND SPECIFICALLY THE OCCUPATIONAL SAFETY AND HEALTH ACT FOR THE CONSTRUCTION INDUSTRY.

4. PERFORM ALL WORK IN A FIRE-SAFE MANNER AND SUPPLY AND MAINTAIN ADEQUATE FIRST-AID AND FIRE FIGHTING EQUIPMENT CAPABLE OF EXTINGUISHING INCIPIENT FIRES. COMPLY WITH LOCAL AND STATE FIRE PREVENTION **REGULATIONS.**

5. PROVIDE ADEQUATE SAFETY AND PROTECTIVE DEVICES FOR WORKMEN DURING EXCAVATION AND CLEARING. REVIEW LOCATION OF EXISTING SERVICES AND UTILITY LINES. PROVIDE PROTECTIONS NECESSARY TO PREVENT DAMAGE TO EXISTING IMPROVEMENTS AND SURVEY MARKERS. PROVIDE EROSION CONTROL PER BUILDING DEPARTMENT REQUIREMENTS.

6. PROVIDE SHORING, SHEETING AND BRACING WHEREVER NECESSARY TO PREVENT CAVING DURING EXCAVATION OR TO PROTECT ADJACENT IMPROVEMENTS, PROPERTY, WORKMEN AND THE PUBLIC.

7. SOILS ENGINEER SHALL INSPECT AND APPROVE CUT-OUT FOR FOUNDATION AND FOUNDATION PLAN.

8. CONCRETE TESTING SHALL BE REQUIRED SEE STRUCTURAL GENERAL NOTES FOR TESTING REQUIREMENTS.

9. FURNISH AND PLACE HOLDOWNS AND DEFORMED STEEL AS INDICATED BY THE STRUCTURAL ENGINEER. STRUCTURAL ENGINEER SHALL INSPECT ALL HOLDOWNS AND STEEL FOR CONFORMANCE. CONTRACTOR SHALL PROVIDE UL RATINGS FOR RATED STEEL PROTECTION, SEE DRAWINGS FOR RATED REQUIREMENTS.

10. RAPIDLY HANDLE CONCRETE FROM MIXER TO FORMS AND DEPOSIT AS NEAR AS POSSIBLE TO ITS FINAL POSITION TO AVOID SEGREGATION DUE TO HANDLING. SEE STRUCTURAL FOR ADDITIONAL REQUIREMENTS.

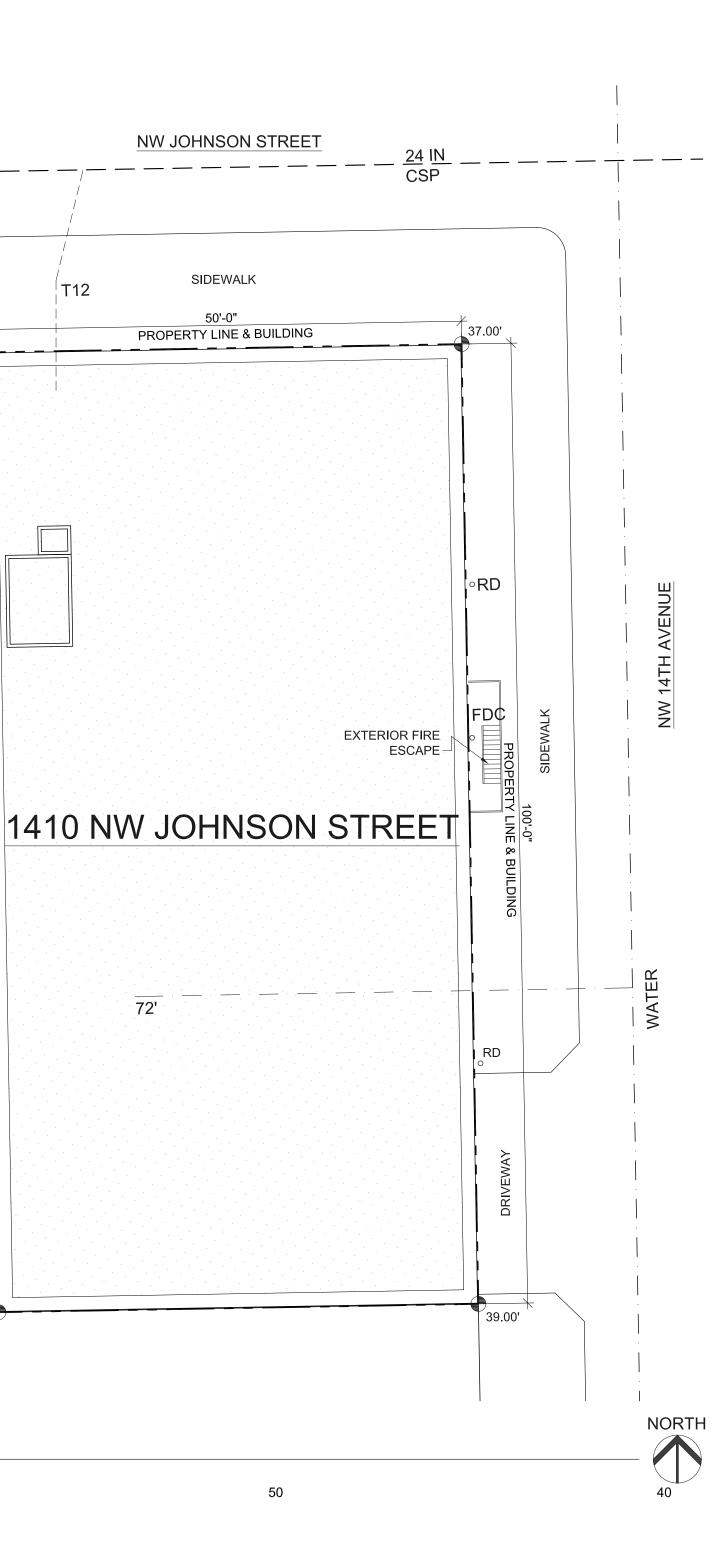
11. EXAMINE DRAWINGS FOR REQUIRED ROUGH CARPENTRY MATERIALS INCLUDING PLATES, STUDS, FIRE-STOPS, SOLID BLOCKING, BRIDGING, POSTS, BLOCKS, SUB-FLOORING AND SHEATHING. LUMBER SHALL BE DOUGLAS-FIR (STANDARD), TREATED LUMBER WITH A NET RETENTION OF 0.25 PCF. GYPSUM BOARD SHALL BE AS NOTED ON DRAWINGS. USE EXTERIOR GYPSUM BOARD FOR SOFFITS AND PORCH CEILINGS AND WATERPROOF IN BATHROOMS. PROVIDE ALL GLUE LAMINATED MEMBERS AS INDICATED BY STRUCTURAL. BUILDING PAPER SHALL BE NO. 15 LB. ASPHALT SATURATED ROOFING FELT. ALL HANGERS AND HOLDOWNS SHALL BE HOT DIPPED GALVANIZED. USE KRAFT FACE FIBERGLASS INSULATION; SEE ENERGY CODE COMPLIANCE. I-JOISTS BY TRUSS JOIST CORPORATION SHALL HAVE HOLES KNOCKED OUT AT FACTORY. INSTALL WITH HOLES UP. SIZE AND DETAILS OF JOISTS SHALL FIT DIMENSIONS AND LOADS AS INDICATED ON DRAWINGS.

12. ALL MANUFACTURED MATERIALS, COMPONENTS, FASTENERS, ASSEMBLIES, ECT., SHALL BE HANDLED AND INSTALLED IN ACCORDANCE WITH THE MANUFACTURER'S INSTRUCTIONS AND PROVISIONS OF APPLICABLE ICBO RESEARCH RECOMMENDATIONS.

13. PROVIDE SHOP DRAWINGS FOR ALL PRE-ENGINEERED PRODUCTS (I-JOISTS, ROOF TRUSSES, ETC.) FOR STRUCTURAL REVIEW.

14. IMMEDIATELY NOTIFY ARCHITECT IN WRITING OF ANY DISREPINCIES BETWEEN CONSTRUCTION DOCUMENTS AND ACTUAL CONDITIONS. CORRECTIONS SHALL BE THE RESPONSIBILITY OF THE OWNER/CONTRACTOR.

15. MECHANICAL AND ELECTRICAL SYSTEMS SHALL BE BIDDER DESIGNED AND UNDER SEPARATE PERMIT. CONTRACTOR SHALL PROVIDE ALL REQUISITE SYSTEM DESIGN DOCUMENTS, LOAD CALCULATIONS AND SHOP DRAWINGS REQUIRED FOR REVIEW.





PROJECT DESCRIPTION

THE PROJECT IS TO HARDEN THE EXISTING EXIT STAIR SYSTEM WHILE EXPANDING THE FIRST FLOOR LOBBY AREA FOR TENANT ACCESS. HARDENING TO SOME EXTENT OCCURS ON ALL FLOORS. ADD ADA BATHROOMS TO UPPER THIRD FLOOR. BRING EXISTING AUTOMATIC SPRINKLER SYSTEM UP TO NFPA13 STANDARDS. PAINT AND REPAIR EXISTING EXTERIOR FIRE ESCAPE AND ASSOCIATED ELEMENTS.

PROPERTY:

SITE ADDRESS:

1410 NW JOHNSON STREET PORTLAND, OREGON 97209

PROPERTY ID: STATE ID: NEW STATE ID: ALT ACOUNT #: MAP #:

R140740 1N1E33AD 2000 1N1E33AD -02000 R180211050 2928 OLD

OWNER/DEVELOPER:

GANN BUILDING LLC 1410 NW JOHNSON STREET PORTLAND OREGON 97209 contact: MARTIN KEHOE

ARCHITECT:

BARRY R. SMITH, PC, ARCHITECT 715 SW MORRISON STREET, SUITE 909 PH: 503.295.6261 PORTLAND, OREGON 97205-3105 contact: BARRY SMITH

PH: 503.244.3838 FAX: N/A EM: mkehoe03@gmail.com

FAX: N/A EM: barry@barryrsmith.com

SEPARATE PERMITS REQUIRED

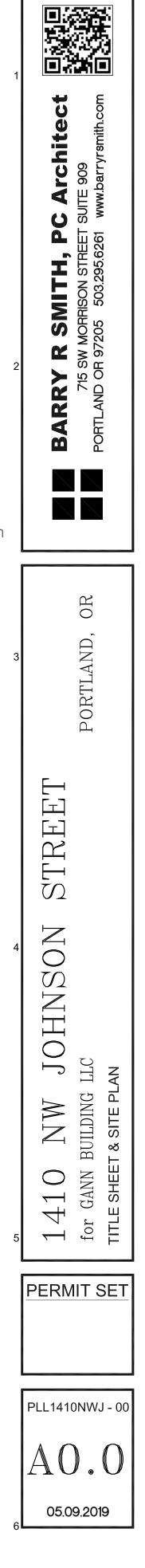
- 1. MECHANICAL PLANS
- 2. ELECTRICAL PLANS
- 3. PLUMBING PLANS

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DRAWING INDEX:

- ARCHITECTURAL
- A0.0 TITLE SHEET + SITE PLAN A0.1 BUILDING CODE ANALYSIS - SUMMARY
- A0.2 BUILDING CODE ANALYSIS HARDENING PLANS
- A0.3 BUILDING CODE ANALYSIS HARDENING PLANS A1.0 EXISTING CONDITION PLANS
- A2.0 DEMOLITION PLANS
- A3.0 HARDENING PLANS + DOOR SCHEDULE
- A3.1 ENLARGED HARDENING PLANS + RATED DETAILS A5.0 EXTERIOR ELEVATIONS
- STRUCTURAL
- S1 PLANS S2 DETAILS





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	TYPE	OCCUPANCY	AREA - SF	AREA - SF	SPRINKLER	ALARM	DETEC
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SEE ALSO:

REMOVAL IMPROVEMENT PLAN.

DETECTION	<u>SECTION 3406 - FIRE ESCAPES</u> 3406.1 WHERE PERMITTED: FIRE ESCAPES SHALL BE PERMITTED ONLY AS PROVIDED FOR IN SECTIONS 3406.1.1 THROUGH 3406.1.4.
NO NO NO	3406.1.2 EXISTING FIRE ESCAPES: EXISTING FIRE ESCAPES SHALL BE CONTINUED TO BE ACCEPTED AS A COMPONENT IN THE MEANS OF EGRESS IN EXISTING BUILDINGS.
NO	3406.1.4 LIMITATIONS: FIRE ESCAPES SHALL COMPLY WITH THIS SECTION AND SHALL NOT CONSTITUTE MORE THAN 50 PERCENT OF THE REQUIRED NUMBER OF EXITS NOR MORE THAN 50 PERCENT OF THE REQUIRED EXIT CAPACITY.
<u>SHERS</u>	SECTION 3411 - ACCESSIBILITY FOR EXISTING STRUCTURES 3411.1 SCOPE: THE PROVISIONS OF SECTION 3411.1 THROUGH 3411.9 APPLY TO MAINTENANCE, CHANGE OF OCCUPANCY, ADDITIONS AND ALTERATIONS TO EXISTING BUILDINGS, INCLUDING THOSE IDENTIFIED AS HISTORIC BUILDINGS.
EGRESS AD AREA ALLOWANCES PER OCCUPANT: FLOOR FACTOR 100 GROSS	 3411.6 ALTERATIONS: A FACILITY THAT IS ALTERED SHALL COMPLY WITH THE APPLICABLE PROVISIONS IN CHAPTER 11 OF THIS CODE, UNLESS TECHNICALLY INFEASIBLE. WHERE COMPLIANCE WITH THIS SECTION IS TECHNICALLY INFEASIBLE, THE ALTERATION SHALL PROVIDE ACCESS TO THE MAXIMUM EXTENT FEASIBLE. <u>EXCEPTIONS:</u> 1. THE ALTERED ELEMENT OR SPACE IS NOT REQUIRED TO BE ON AN ACCESSIBLE ROUTE, UNLESS REQUIRED BY SECTION 3411.7. 2. ACCESSIBLE MEANS OF EGRESS REQUIRED BY CHAPTER 10 ARE NOT REQUIRED TO BE PROVIDED IN EXISTING FACILITIES.
ESS ILLUMINATION IG THE EXIT DISCHARGE, SHALL BE ILLUMINATED AT ALL TIMES THE BUILDING EGRESS IS OCCUPIED S: HE EXTERIOR OF THE BUILDING.	SECTION 3412 - COMPLIANCE ALTERNATIVES 3412.1 COMPLIANCE: THE PROVISIONS OF THIS SECTION ARE INTENDED TO MAINTAIN OR INCREASE THE CURRENT DEGREE OF PUBLIC SAFETY, HEALTH AND GENERAL WELFARE IN EXISTING BUILDINGS WHILE PERMITTING REPAIR, ALTERATION, ADDITION AND CHANGE OF OCCUPANCY WITHOUT REQUIRING FULL COMPLIANCE WITH CHAPTERS 2 THROUGH 33, OR SECTION 3401.3, AND 3403 THROUGH 3409M EXCEPT WHERE COMPLIANCE WITH OTHER PROVISIONS OF THIS CODE IS SPECIFICALLY REQUIRED IN THIS SECTION.
IE EXTERIOR OF THE BUILDING. NG: IRE HAS A FIRE-RESISTANCE RATING OF 2-HOURS.	3412.2.4 ALTERATIONS OR REPAIRS AN EXISTING BUILDING OR PORTION THEREOF, WHICH DOES NOT COMPLY WITH THE REQUIREMENTS OF THIS CODE FOR NEW CONSTRUCTION, SHALL NOT BE ALTERED OR REPAIRED IN SUCH A MANNER THAT RESULTS IN THE BUILDING BEING LESS SAFE OR SANITARY THAN SUCH BUILDING IS CURRENTLY. IF, IN THE ALTERATION OR REPAIR, THE CURRENT LEVEL OF SAFETY OR SANITATION IS TO BE REDUCED, THE PORTION ALTERED OR REPAIRED SHALL CONFORM TO THE REQUIREMENTS OF CHAPTERS 2 THROUGH 12 AND CHAPTERS 14 THROUGH

. BE MARKED BY AN APPROVED EXIT SIGN READILY VISIBLE FROM ANY ATH OF EGRESS TRAVEL TO EXITS AND WITHIN EXITS SHALL BE MARKED EARLY INDICATED THE DIRECTION OF EGRESS TRAVEL IN CASES WHERE AVEL IS NOT IMMEDIATELY VISIBLE TO THE OCCUPANTS. INTERVENING TS SHALL BE MARKED BY EXIT SIGNS. EXIT SIGN PLACEMENT SHALL BE SS CORRIDOR OR EXIT PASSAGEWAY IS MORE THAN 100 FT OR THE LISTED ICHEVER IS LESS, FROM THE NEAREST VISIBLE EXIT SIGN.

NG SPACES:

HALL NOT PASS THROUGH ADJOINING OR INTERVENING ROOMS OR AREAS, MS OR AREAS AND THE AREA SERVED ARE ACCESSORY TO ONE OR THE NCY AND PROVIDE A DISCERNIBLE PATH OF EGRESS TRAVEL TO AN EXIT. OT PROHIBITED THROUGH INTERVENING ROOMS OR SPACES IN A GROUP OINING ROOMS OR SPACES ARE THE SAME OR A LESSER HAZARD

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ANCE RATING: CORRIDOR IS 0-HOUR, FOR F OCCUPANCY AND AN OCCUPANT LOAD

CTLY TO THE PUBLIC WAY.

RWAYS AND RAMPS

ARE CONSTRUCTED AS 2-HOUR FIRE BARRIERS.

EXTERIOR OF THE BUILDING. THE EXIT DISCHARGE PROVIDSE DIRECT RGE DOES NOT REENTER THE BUILDING.

MENTS:

ITH SECTION 3411.

DINGS AND STRUCTURES

ALL CONTROL THE ALTERATION, REPAIR, ADDITION, AND CHANGE OF ND STRUCTURES.

1.4 OR THIS SECTION, ALTERATIONS TO ANY BUILDING SHALL COMPLY DE FOR NEW CONSTRUCTION. ALTERATIONS SHALL BE SUCH THAT THE NO LESS COMPLYING WITH THE PROVISIONS OF THIS CODE THAN THE AS PRIOR TO THE ALTERATION.

E REQUIRED TO COMPLY WITH THE REQUIREMENTS OF SECTION 1009 ISTRUCTION DOES NOT ALLOW A REDUCTION IN PITCH OR SLOPE. RED TO COMPLY WITH SECTION 1009.15 SHALL NOT BE REQUIRED TO SECTION 1012.6 REGARDING FULL EXTENSION OF THE HANDRAILS WHERE OUS DUE TO PLAN CONFIGURATION.

NTS CARRYING GRAVITY LOAD:

IG STRUCTURAL ELEMENT FOR WHICH AN ALTERATION CAUSES AN F MORE THAN 5 PERCENT SHALL BE STRENGTHENED, SUPPLEMENTED, S NEEDED TO CARRY THE INCREASED GRAVITY LOAD REQUIRED BY THIS STING GRAVITY LOAD-CARRYING STRUCTURAL ELEMENT WHOSE GRAVITY SED AS PART OF THE ALTERATION SHALL BE SHOWN TO HAVE THE DESIGN GRAVITY LOADS REQUIRED BY THIS CODE FOR NEW

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FIXED, OPERABLE, AND DOORS WITH GREATER

THAN 50% GLAZING

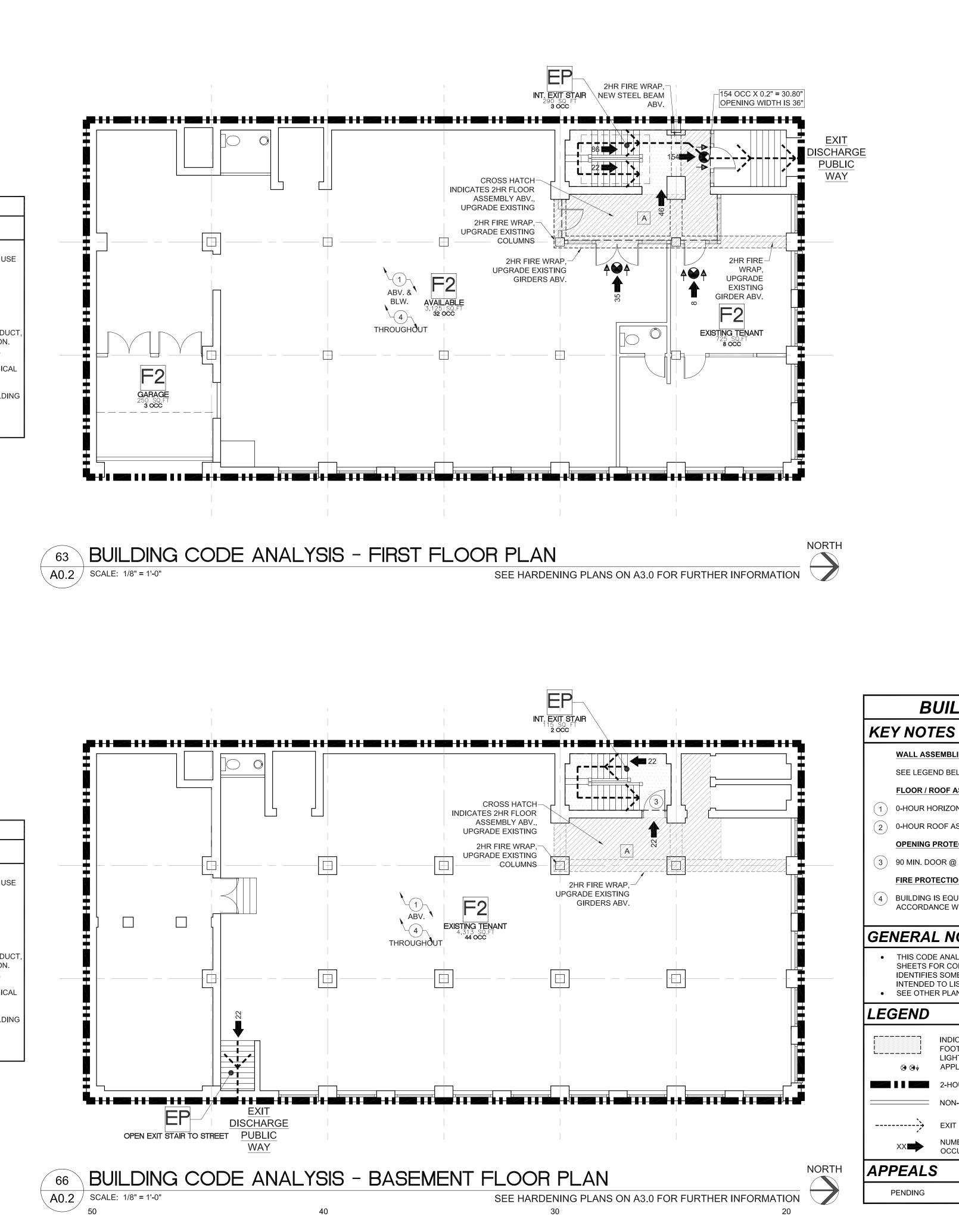
SHGC-ALL FRAME TYPES

BUILDING ENVELOPE REQU	JIREMENTS - OPAQUE AS	SEMBLIES		
	5 AND MA	RINE 4		
CLIMATE ZONE	ALL OTHER	GROUP R		
ROOFS				
ATTIC AND OTHER	R-38			
WALLS, ABOVE GRADE				
WOOD FRAMED AND OTHER	R-13 + R-3.8 <u>OR</u> R-21			
FLOORS				
JOIST / FRAMING (STEEL / WOOD)	R-30	R-30		
SLAB-ON-GRADE FLOORS				
UNHEATED SLABS	NR	NR		
OPAQUE DOORS				
SWINGING	U-0.70			
ROLL-UP OR SLIDING	U-0.50			
BUILDING ENVELOPE R	EQUIREMENTS - FENESTI	RATION		
CLIMATE ZONE	5 AN	ND MARINE 4		
VERTICAL FENESTRATION (30% MAX	IMUM OF ABOVE-GRADE WA	.LL)		
FENESTRATION TYPE	U	-FACTOR		
FRAMING MATERIALS OTHER THAN I REINFORCMENT OR CLADDING	METAL WITH OR WITHOUT ME	ETAL		

ORS 447.241 STANDARDS FOR RENOVATION, ALTERATION OR MODIFICATION OF CERTAIN BUILDINGS; BARRIER

00	CUPANCY SEPARATION
	<u>T FLOOR</u> - 5,000 GROSS SQ. FT. DTAL OCCUPANT LOAD ALLOWED
F2	4,100 SQ. FT 43 OCCUPANTS FACTORY OCCUPANIES INCLUDE THE U OF A BUILDING OR STRUCTURE OR PORTION THEROF, FOR LOW-HAZARD FACTORY INDUSTRIAL <u>100 GROSS SF</u> <u>ALLOWANCE PER OCCUPANT.</u>
EP	290 SQ. FT 3 OCCUPANTS EXIT STAIR ENCLOSURE OR EXIT PASSAGEWAY: BOTH WITH OPENING, D PENETRATION, AND JOINT PROTECTION SEE WALL TYPES AND JOINT DETAILS, DOOR AND WINDOW SCHEDULES, PENETRATION DETAILS, AND MECHANIC DRAWINGS. (PART OF FACTORY OCCUPANCY DESIGNATION AND CALCULATED AS PART OF IT FOR BUILD AREA CALCULATION PURPOSES.) 100 GROSS SF ALLOWANCE PER OCCUPANT.

<u>00</u>	CCUPANCY SEPARATION
	<u>EMENT FLOOR</u> - 5,000 GROSS SQ. FT. DTAL OCCUPANT LOAD ALLOWED
F2	4,313 SQ. FT 44 OCCUPANTS FACTORY OCCUPANIES INCLUDE THE US OF A BUILDING OR STRUCTURE OR PORTION THEROF, FOR LOW-HAZARD FACTORY INDUSTRIAL <u>100 GROSS SF</u> ALLOWANCE PER OCCUPANT.
EP	115 SQ. FT 2 OCCUPANTS EXIT STAIR ENCLOSURE OR EXIT PASSAGEWAY: BOTH WITH OPENING, DL PENETRATION, AND JOINT PROTECTION SEE WALL TYPES AND JOINT DETAILS, DOOR AND WINDOW SCHEDULES, PENETRATION DETAILS, AND MECHANIC DRAWINGS. (PART OF FACTORY OCCUPANCY DESIGNATION AND CALCULATED AS PART OF IT FOR BUILDI AREA CALCULATION PURPOSES.) 100 GROSS SF ALLOWANCE PER OCCUPANT.



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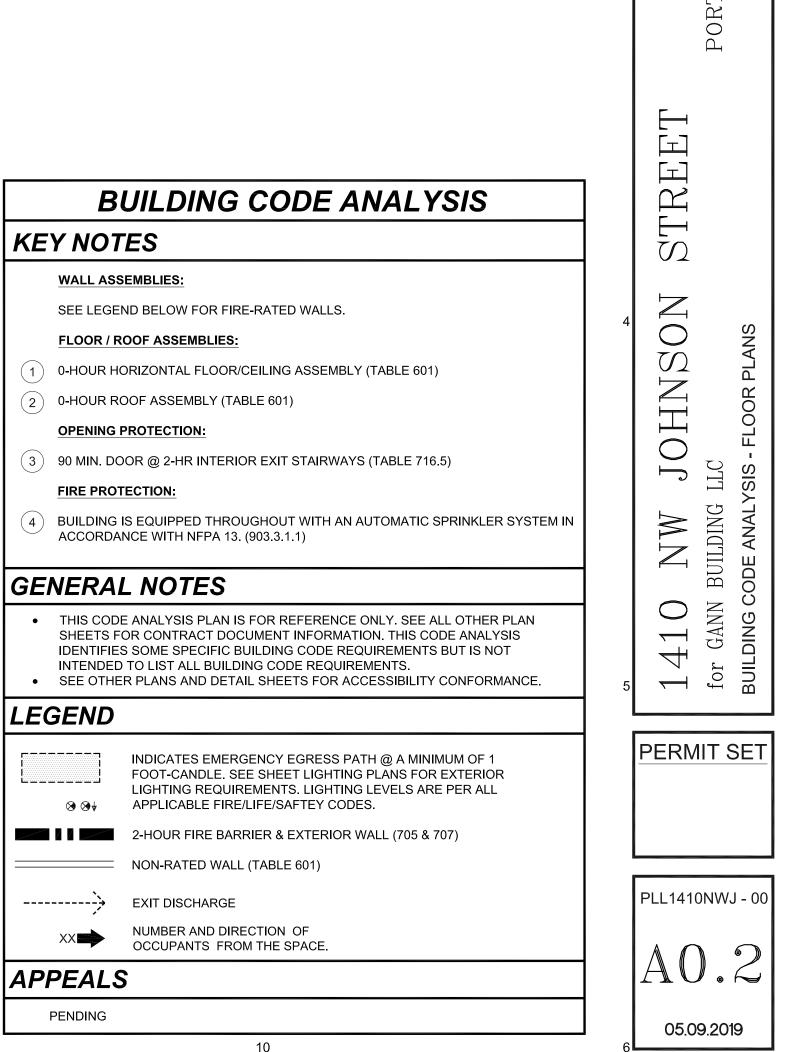
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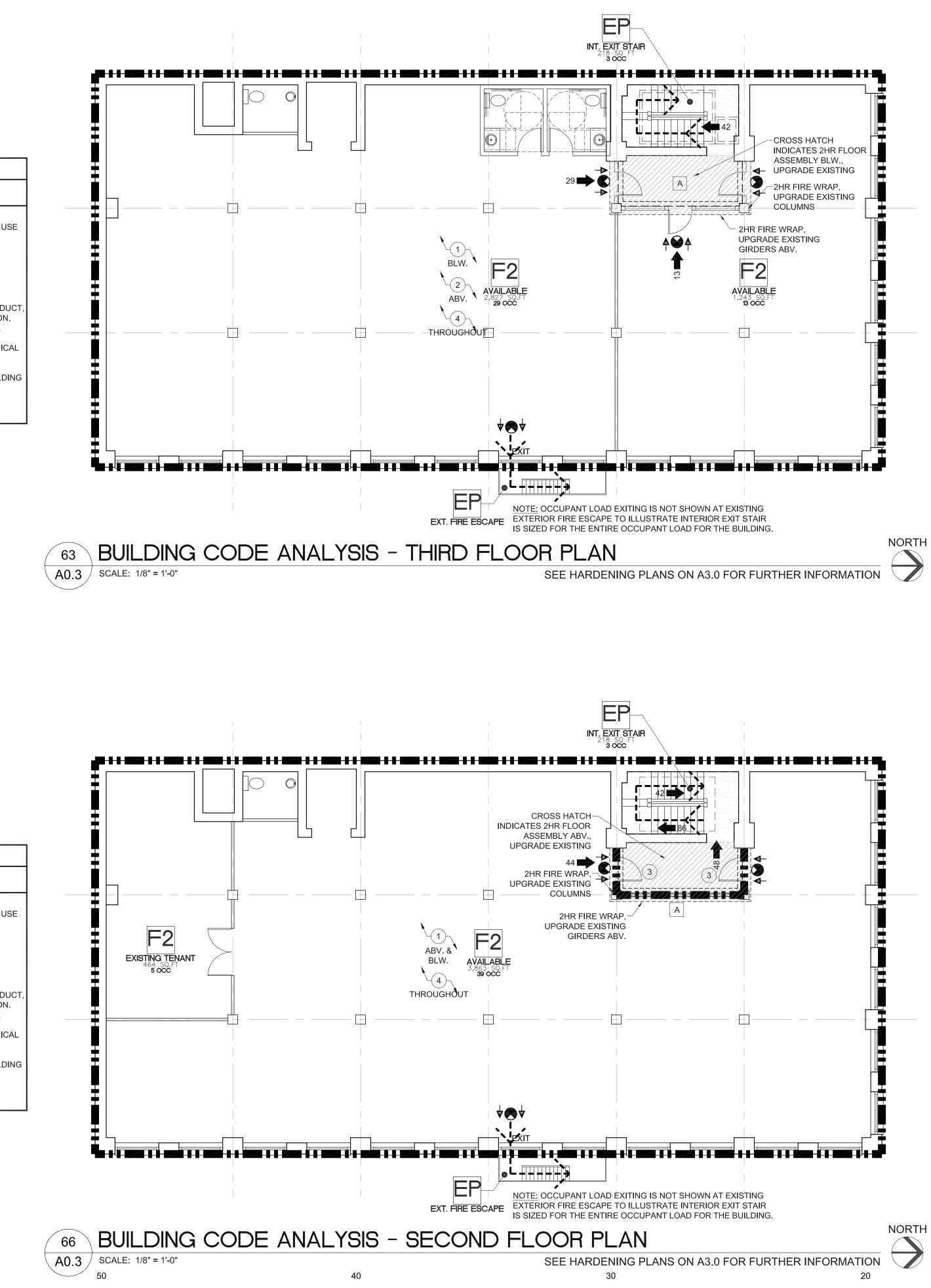


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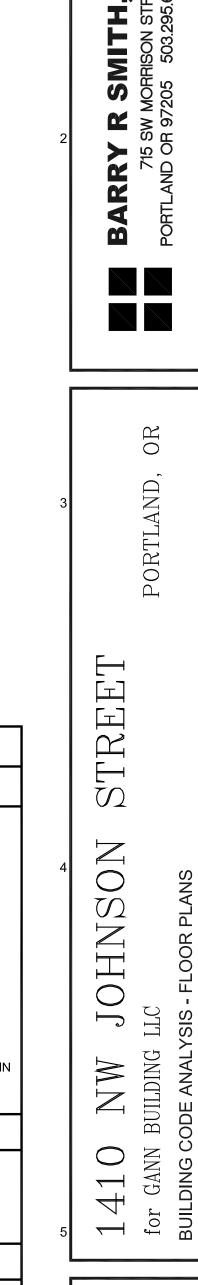
00	CUPANCY SEPARATION
	<u>D FLOOR</u> - 5,000 GROSS SQ. FT. TAL OCCUPANT LOAD ALLOWED
F2	4,103 SQ. FT 42 OCCUPANTS FACTORY OCCUPANIES INCLUDE THE U OF A BUILDING OR STRUCTURE OR PORTION THEROF, FOR LOW-HAZARD FACTORY INDUSTRIAL <u>100 GROSS SF</u> <u>ALLOWANCE PER OCCUPANT.</u>
EP	218 SQ. FT 3 OCCUPANTS EXIT STAIR ENCLOSURE OR EXIT PASSAGEWAY: BOTH WITH OPENING, D PENETRATION, AND JOINT PROTECTION SEE WALL TYPES AND JOINT DETAILS, DOOR AND WINDOW SCHEDULES, PENETRATION DETAILS, AND MECHANIC DRAWINGS. (PART OF FACTORY OCCUPANCY DESIGNATION AND CALCULATED AS PART OF IT FOR BUILD AREA CALCULATION PURPOSES.) 100 GROSS SF ALLOWANCE PER OCCUPANT.

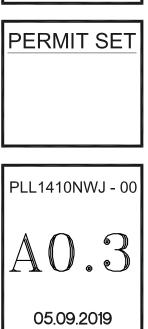
00	CCUPANCY SEPARATION
	<u>OND FLOOR</u> - 5,000 GROSS SQ. FT. OTAL OCCUPANT LOAD ALLOWED
F2	4,358 SQ. FT 45 OCCUPANTS FACTORY OCCUPANIES INCLUDE THE US OF A BUILDING OR STRUCTURE OR PORTION THEROF, FOR LOW-HAZARD FACTORY INDUSTRIAL <u>100 GROSS SF</u> ALLOWANCE PER OCCUPANT.
EP	218 SQ. FT 3 OCCUPANTS EXIT STAIR ENCLOSURE OR EXIT PASSAGEWAY: BOTH WITH OPENING, DL PENETRATION, AND JOINT PROTECTION SEE WALL TYPES AND JOINT DETAILS, DOOR AND WINDOW SCHEDULES, PENETRATION DETAILS, AND MECHANIC DRAWINGS. (PART OF FACTORY OCCUPANCY DESIGNATION AND CALCULATED AS PART OF IT FOR BUILDI AREA CALCULATION PURPOSES.) 100 GROSS SF ALLOWANCE PER OCCUPANT.

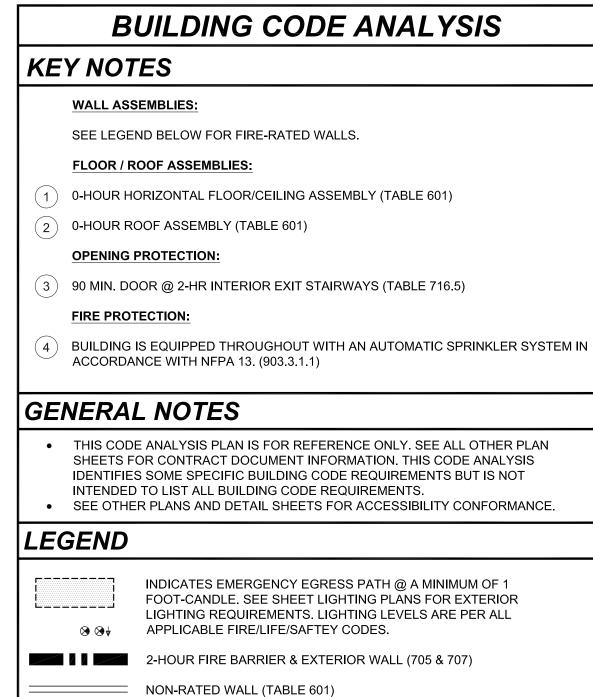




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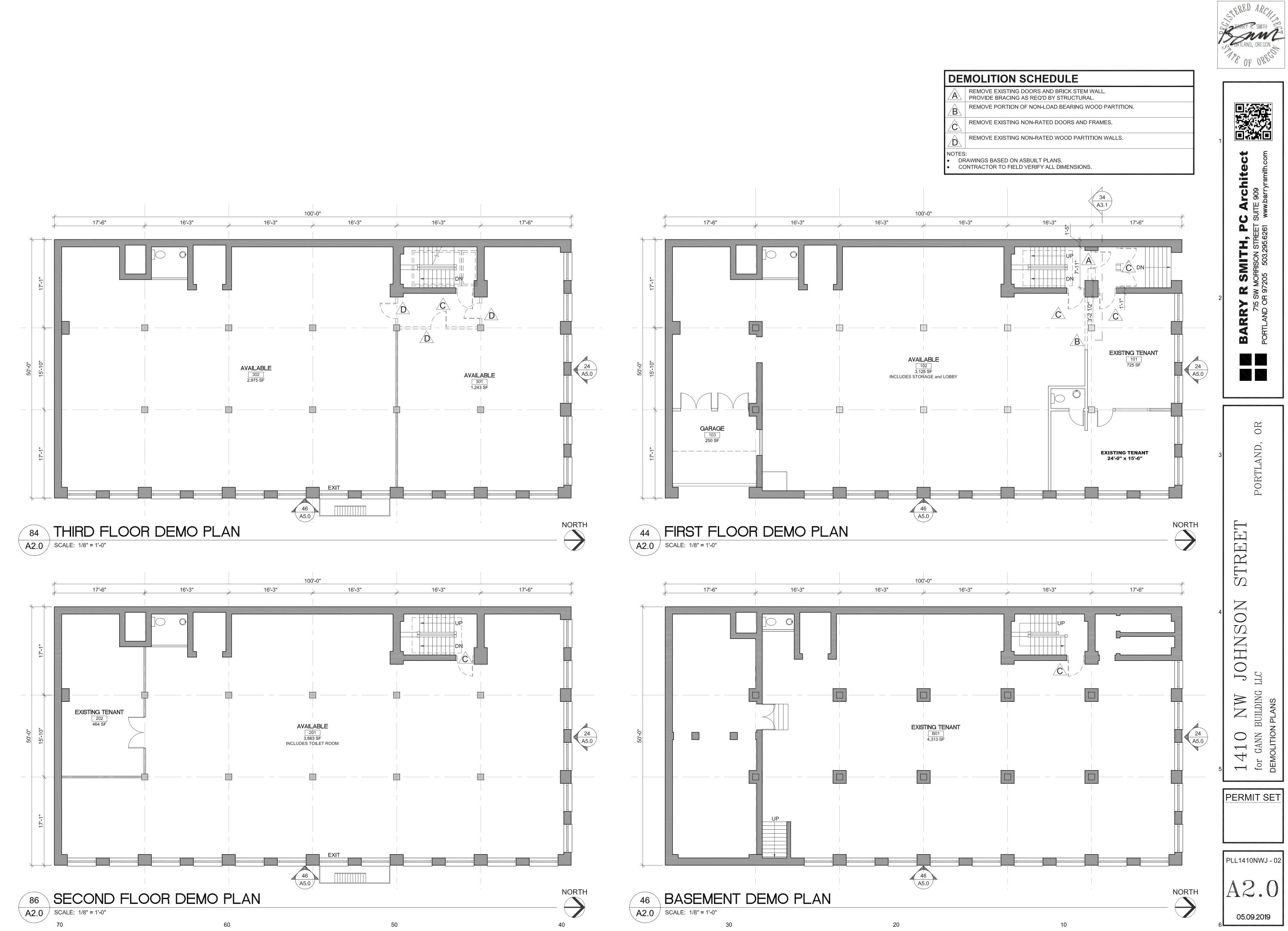
----- EXIT DISCHARGE

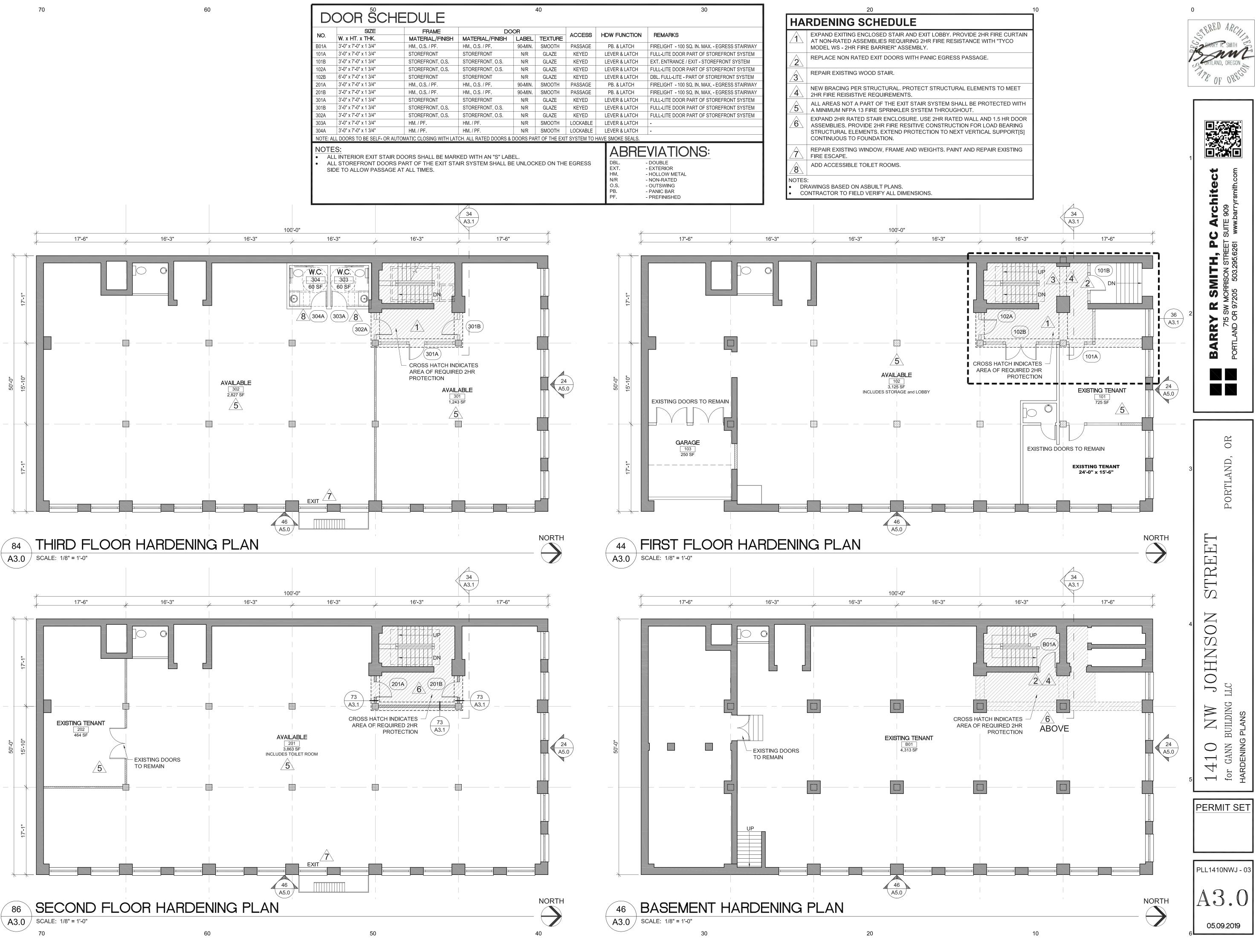
APPEALS

PENDING

XX NUMBER AND DIRECTION OF OCCUPANTS FROM THE SPACE.







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CONSTRUCTION BASE LAYER 5/8" TYPE X GYPSUM WALLBOARD OR VEENER BASE APPLIED PARALLEL OR AT RIGHT ANGLES TO EACH SIDE OF 2X6 STUDS 16" O.C. WITH 1-1/4" TYPE W DRYWALL SCREWS 12" O.C.. FACE LAYER 5/8" TYPE X GYPSUM WALLBOARD OR VENEER BASE APPLIED PARALLEL OR AT RIGHT ANGLES TO EACH SIDE WITH 1-7/8" TYPE W DRYWALL SCREWS 12" O.C. AND OFFSET 6" FROM SCREWS IN BASE LAYER. JOINTS STAGGERED 16" EACH LAYER AND SIDE. (LOAD BEARING) FIRE TEST: SWRI 01-5920-614, 12-5-94 SOUND TEST: SEE WP 4135 (NGC 2363, 4-1-70) 73 2 HR. INT. 5 1/2" WOOD A3.1 SCALE: 1" = 1' - 0" GA FILE No.: WP 4136 - (E) STEEL JOINT — (N) 1/2" LAYER TYPE C GYP. BD. - (N) METAL STUDS - (N) CORNER BEADS

—(2) LAYERS 5/8" TYPE "X" GYP. BD.

__(2) LAYERS 5/8" TYPE "X" GYP. BD.

2x6 STUDS @ 16" O.C.

1/2" LAYER NOM. 3/32" THICK GYPSUM TYPE C GYPSUM BOARD ATTACHED WITH 1" LONG SELF-DRILLING, SELF-TAPPING STEEL SCREWS, SPACED VERTICALLY 12" O.C. TO STEEL STUDS 1-5/8" WIDE WITH LEG DIMENSIONS OF 1-5/16" AND 1-7/16" WITH A 1/4" FOLDED FLANGE IN LEGS FABRICATED FROM 25 MSG GALV STEEL, 3/4" BY 1-3/4" RECTANGULAR CUTOUTS PUNCHED 8" AND 16" FROM THE ENDS. STEEL STUD CUT 1/2" LESS IN LENGTH THAN ASSEMBLY HEIGHT. CORNER BEADS NO. 28 MSG GALV STEEL, 1-1/4" LEGS ATTACHED TO GYPSUM BOARD BY CRIMPING SPACED 6" O.C.

FIRE TEST: UL X520 AND CITY OF PORTLAND BUILDING CODE APPEAL APPROVAL.

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A3.1



ر "5 1/2 ر

- (E) 1" FINISHWOOD FLOOR (E) 3X6 T&G WOOD DECKING - (E) 7X14 HEAVY TIMBER PURLINS BEYOND (N) 2X JOISTS (2X8 MIN.) @ 24" O.C. MAX. FOR FURRED DOWN CEILING, SET FLUSH w/ (E) PURLINS TO PROVIDE 2HR PROTECTION @ (E) PURLINS — (N) BASE LAYER 5/8" TYPE X GYP. BD. - (N) SECOND LAYER 5/8" TYPE X GYP. BD.

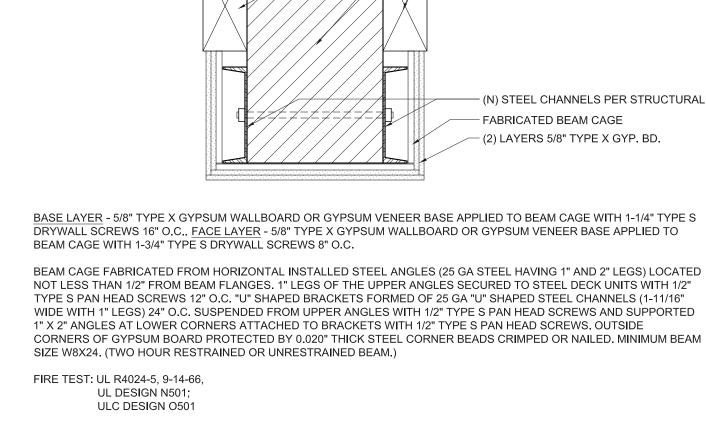
> - (N) THIRD LAYER 5/8" TYPE X GYP. BD. - (N) 7/8" RIGID FURRING CHANNEL - (N) FACE LAYER 5/8" TYPE X GYP. BD. (E) 14X16 HEAVY TIMBER GIRDERS w/ (N) 2HR PROTECTION, WHERE OCCURS

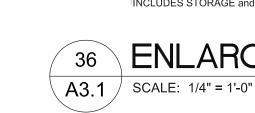
BASE LAYER - 5/8" TYPE X GYPSUM WALLBOARD APPLIED AT RIGHT ANGLES TO 2X8 WOOD JOISTS 24" O.C. WITH 1-1/4" TYPE W DRYWALL SCREWS 12" O.C. <u>SECOND LAYER</u> - 5/8" TYPE X GYPSUM WALLBOARD APPLIED AT RIGHT ANGLES TO JOISTS WITH 2" TYPE W DRYWALL SCREWS 12" O.C. SECOND LAYER JOINTS OFFSET 24" FROM BASE LAYER JOINTS. THIRD LAYER - 5/8" TYPE X GYPSUM WALLBOARD APPLIED AT RIGHT ANGLES TO JOISTS WITH 2-1/2" TYPE W DRYWALL SCREWS 12" O.C. THIRD LAYER JOINTS OFFSET 12" FROM SECOND LAYER JOINTS. HAT-SHAPED 7/8" RIGID FURRING CHANNELS 24" O.C. APPLIED AT RIGHT ANGLES TO JOISTS OVER THIRD LAYER WITH TWO 2-1/2" LONG TYPE W DRYWALL SCREWS AT EACH JOIST. FACE LAYER - 5/8" TYPE X GYPSUM WALLBOARD APPLIED AT RIGHT ANGLES TO FURRING CHANNELS WITH 1-1/8" TYPE S DRYWALL SCREWS 12" O.C. WOOD JOISTS SUPPORTING 3/4" T&G EDGE PLYWOOD FLOOR APPLIED AT RIGHT ANGLES TO JOISTS WITH 8d NAILS 6" O.C. AT JOINTS AND 12" AT INTERMEDIATE JOISTS. CEILING PROVIDES TWO-HOUR FIRE-RESISTANCE PROTECTION FOR WOOD FRAMING.

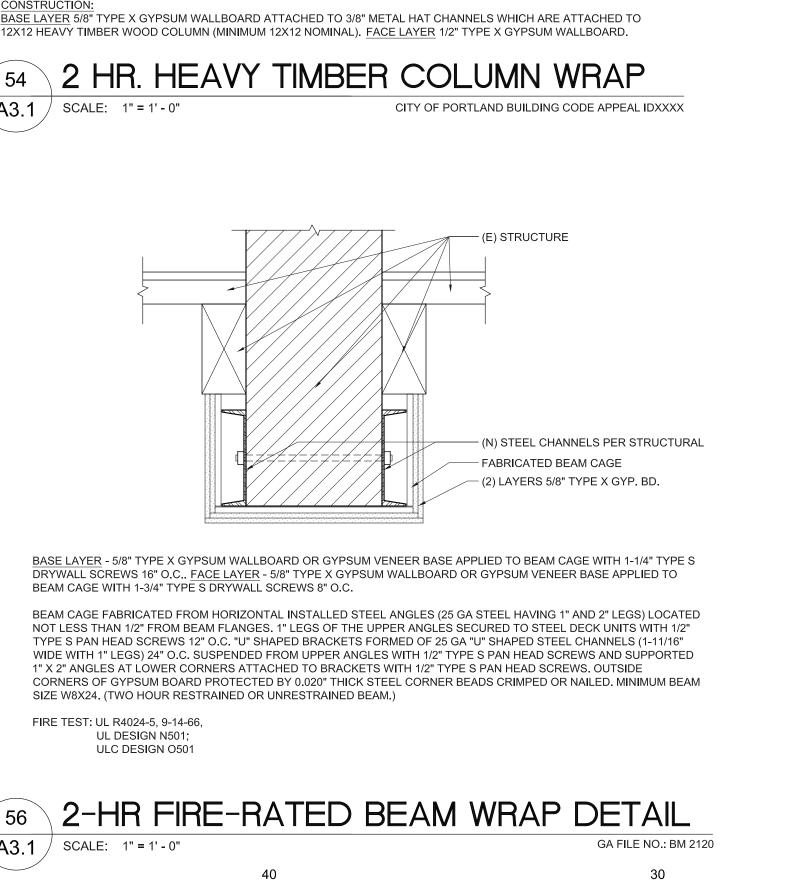
FIRE TEST: UL R4024, 00NK26545, 4-27-01; UL R4024, 03NK11206, 3-19-03; UL DESIGN L556; ULC DESIGN M514 76 2-HR FIRE-RATED FLOOR/CEILING DETAIL

60









CONSTRUCTION: BASE LAYER 5/8" TYPE X GYPSUM WALLBOARD ATTACHED TO 3/8" METAL HAT CHANNELS WHICH ARE ATTACHED TO



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A3.1 / SCALE: 1" = 1' - 0"

A3.1 / SCALE: 1" = 1' - 0"

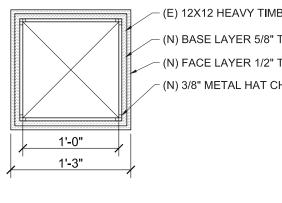
56

GA FILE NO.: FC 5725

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A3.1 / SCALE: 1" = 1' - 0"

2 HR. HEAVY TIMBER COLUMN WRAP 54



(E) 12X12 HEAVY TIMBER COLUMN – (N) BASE LAYER 5/8" TYPE X GYP. BD - (N) FACE LAYER 1/2" TYPE X GYP. BD. - (N) 3/8" METAL HAT CHANNELS

CITY OF PORTLAND BUILDING CODE APPEAL IDXXXX

2 HR. HEAVY TIMBER BEAM WRAP

BASE LAYER 5/8" TYPE X GYPSUM WALLBOARD ATTACHED TO 3/8" METAL HAT CHANNELS WHICH ARE ATTACHED TO 14X16 HEAVY TIMBER WOOD BEAM NOMINAL (MINIMUM 8X12 NOMINAL). FACE LAYER 1/2" TYPE X GYPSUM WALLBOARD.

OSSC 2014 SECTION 707 - FIRE BARRIERS

INTERIOR EXIT STAIRWAY

- (E) 1" FINISHWOOD FLOOR 76 — (E) 3X6 T&G DECKING A3.1 — (E) 7X14 PURLINS - (N) 2HR FLOOR/CEILING ASSEMBLY 74 A3.1 / - SEE STEEL JOINT DETAIL FOR FIRE PROTECTION - (N) BASE LAYER 5/8" TYPE X GYP. BD. - (N) FACE LAYER 1/2" TYPE X GYP. BD. (N) 3/8" METAL HAT CHANNELS 1'-2" 1'-5" – (E) 16X14 HEAVY TIMBER BEAM/GIRDER

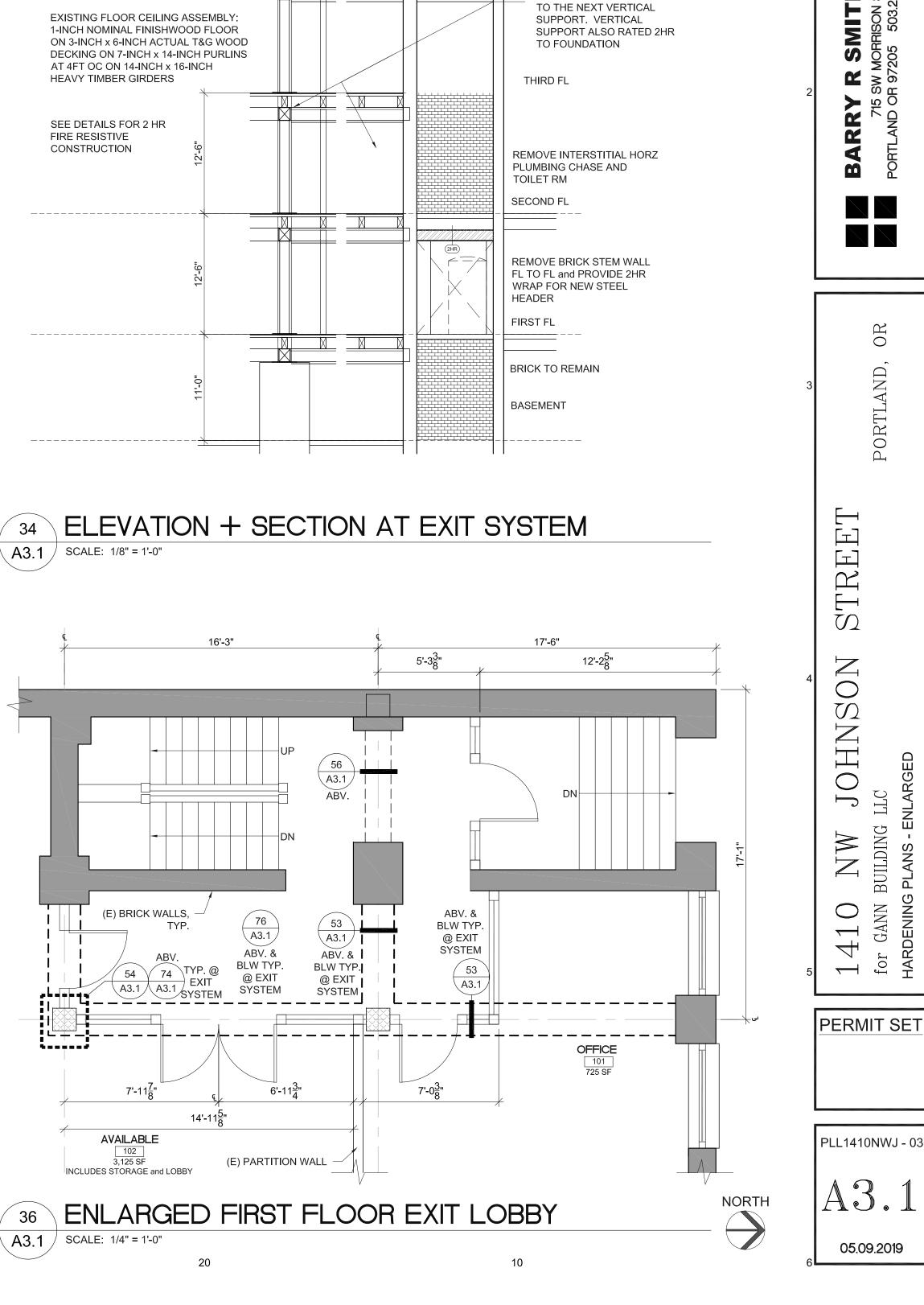
SEE DETAILS FOR 2 HR FIRE RESISTIVE CONSTRUCTION

34

HEAVY TIMBER GIRDERS

EXISTING FLOOR CEILING ASSEMBLY:

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AT AREA OF 2HR STAIRWELL

STRUCTURAL ELEMENTS

IMPROVED TO 2HR FIRES

TO THE NEXT VERTICAL

SUPPORT. VERTICAL

RESISTIVE CONSTRUCTION

EXTENSION - ALL

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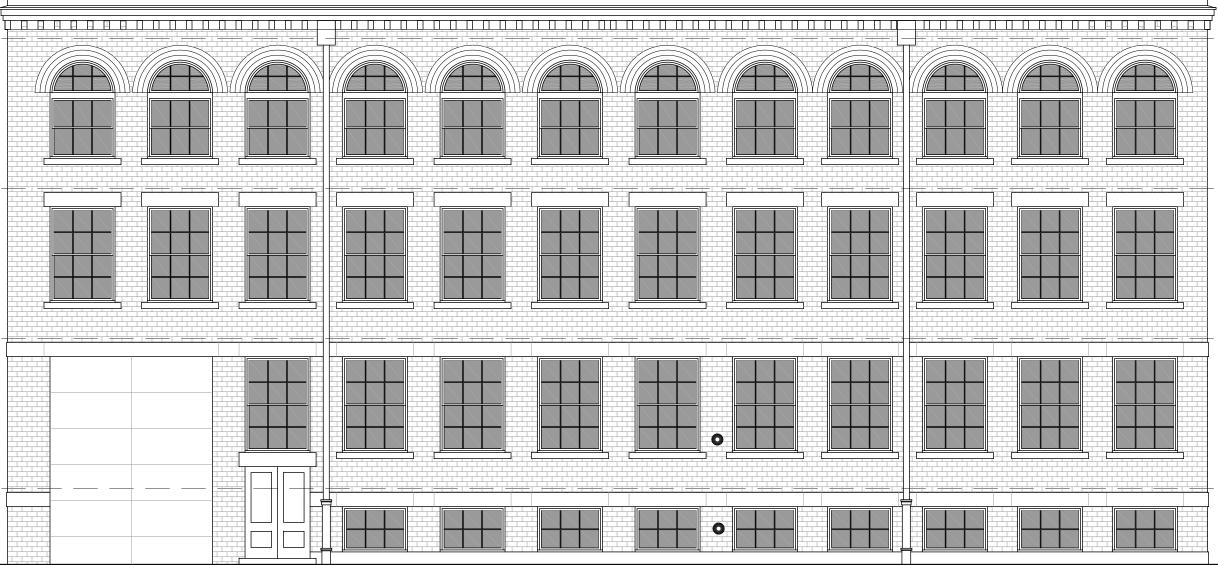
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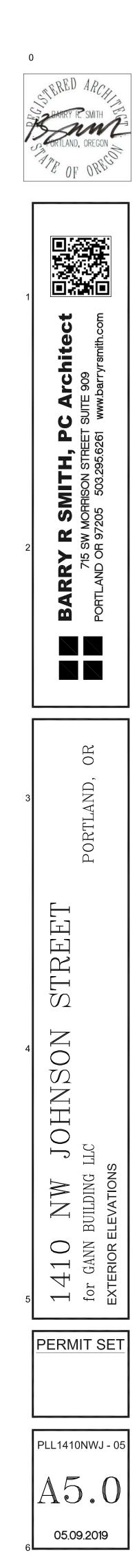
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A5.0 SCALE: 1/8" = 1'-0"





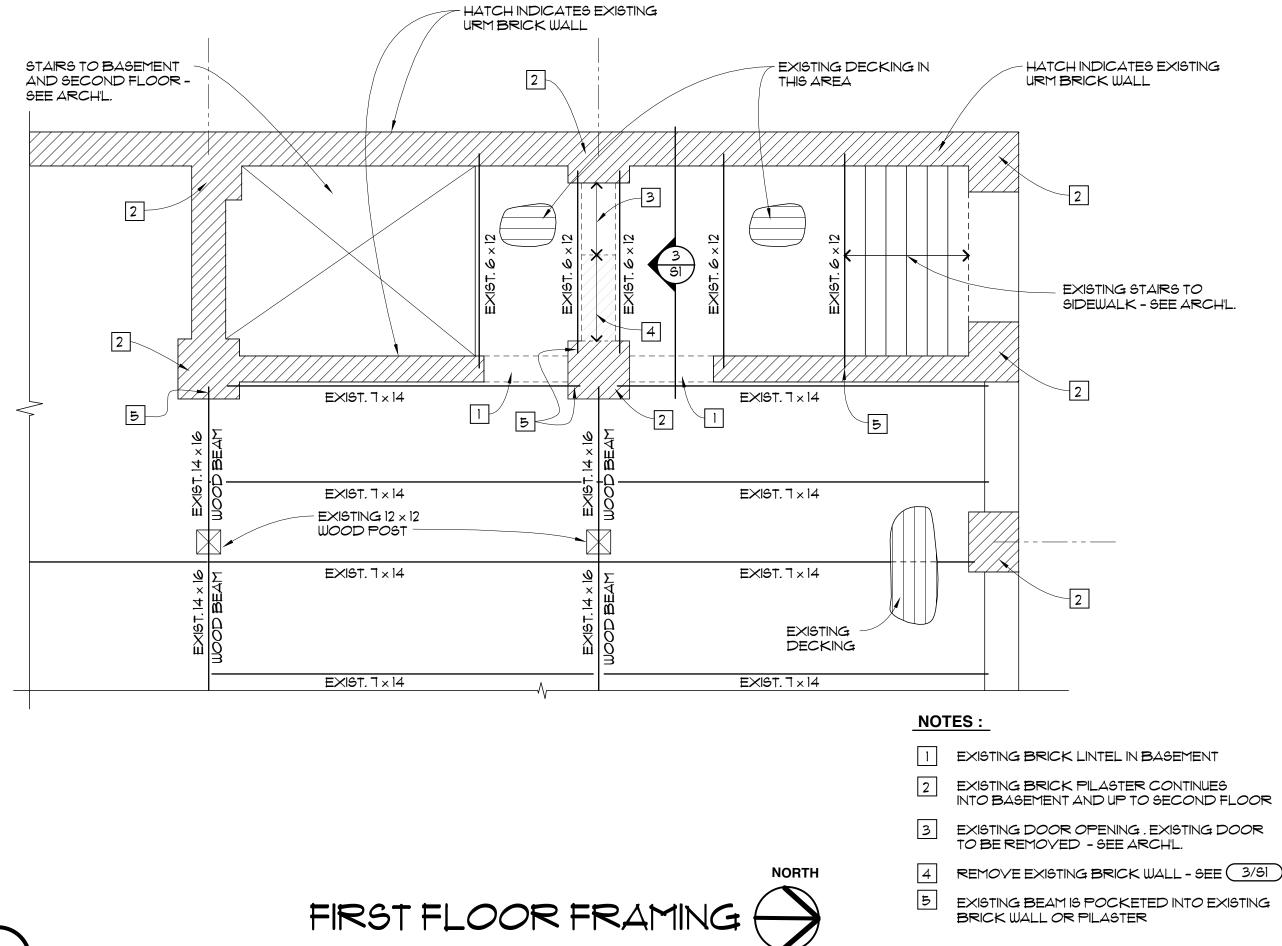
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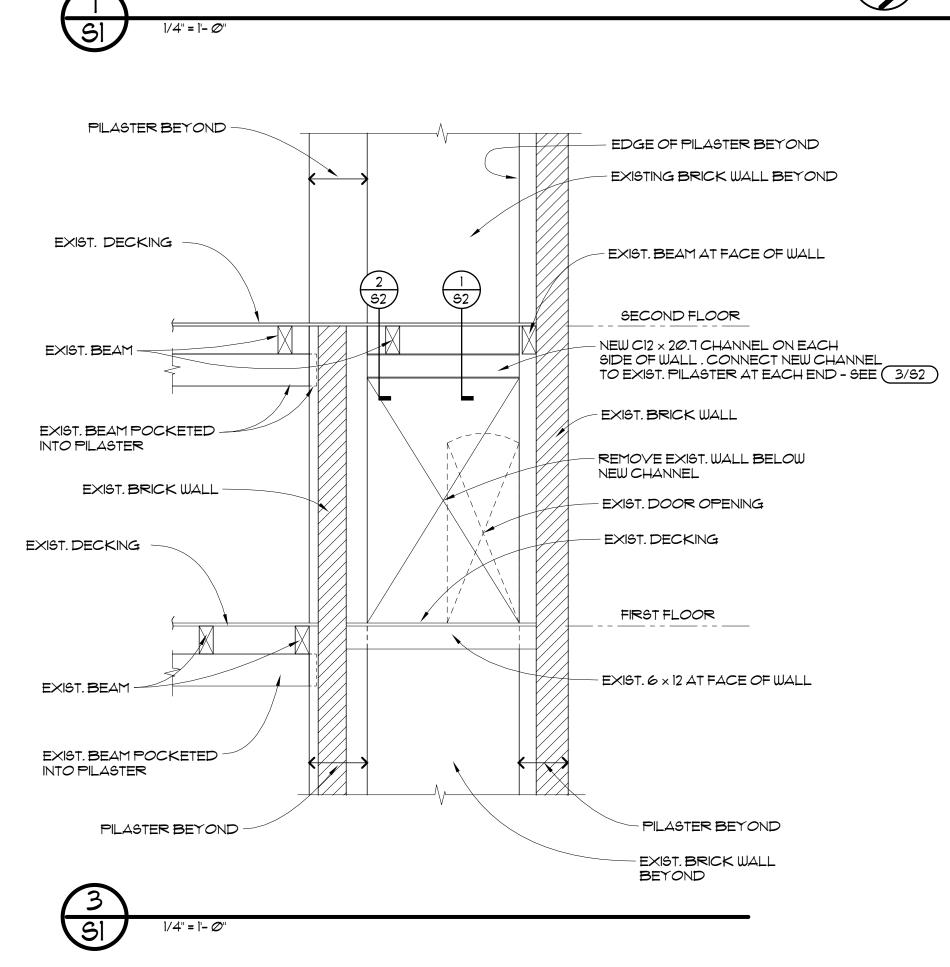
NOTE LOCATION OF EXISTING FDC AND BELL







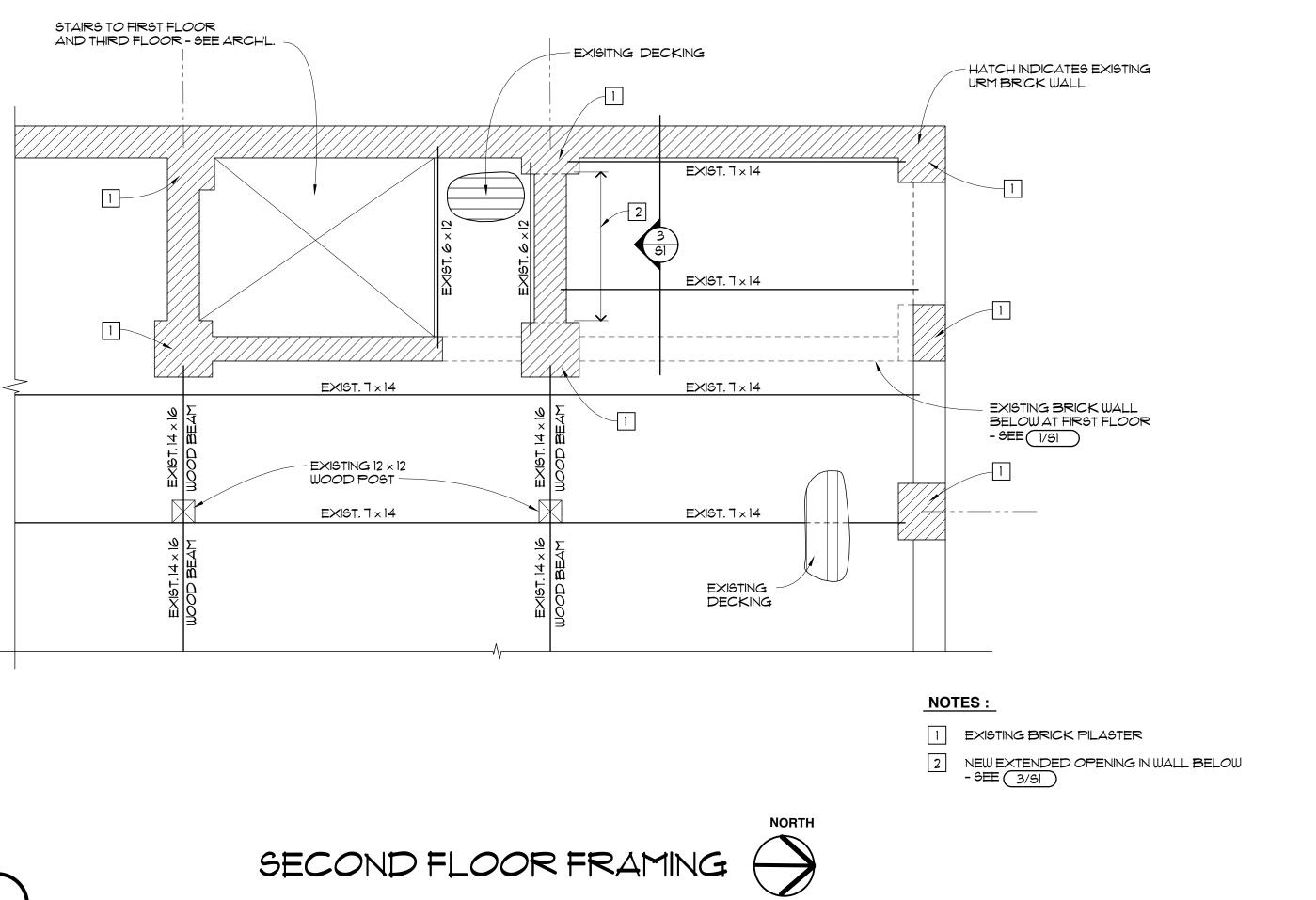


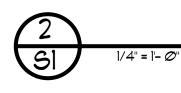


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GENERAL NOTES

SPECIAL INSPECTION

- Required special inspections shall be performed by an independent special inspector per Section 1701 of the International Building Code (IBC) for the following:
- a. Visual inspection of all structural welding except welding done in an approved fabricator's shop. b. Installation of post installed anchors.
- For more specific information regarding special inspections see Tables I
- 2. The special inspector shall provide a copy of their report to the owner, architect, structural engineer, contractor, and building official.

GENERAL

- 1. These notes set the minimum standards for construction. The drawings govern over the General Notes to the extent shown.
- 2. Contractor shall verify all dimensions and conditions on drawings and in the field. Coordinate locations of openings with architectural. Notify design
- agency of any discrepancies. 3. Contractor shall provide all necessary temporary support prior to completion
- of vertical and lateral load systems. 4. The contractor shall be responsible for all required safety precautions and
- methods, techniques, sequences, and procedures required to perform his work. Where reference is made to ASTM, AISC, ACI or other standards, the latest 5.
- issue shall apply. 6. All work shall be in strict compliance with the International Building Code as
- amended by the State of Oregon and all other state and local codes and building requirements that apply.
- 7. Design Criteria: a. Floors
- 5Ø psf 15 psf

STRUCTURAL AND MISCELLANEOUS STEEL

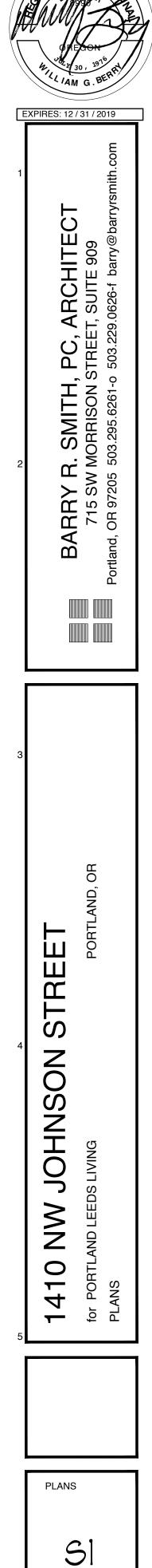
- 1. Detailing, fabrication and erection shall conform to the Steel Construction Manual
- of AISC. 2. All steel to be A36 or better except as noted.
- 3. All welds to be made by Certified Welders to AWS Standards with $E \ T \varnothing \times X$
- electrodes.

b Floor partition allowance

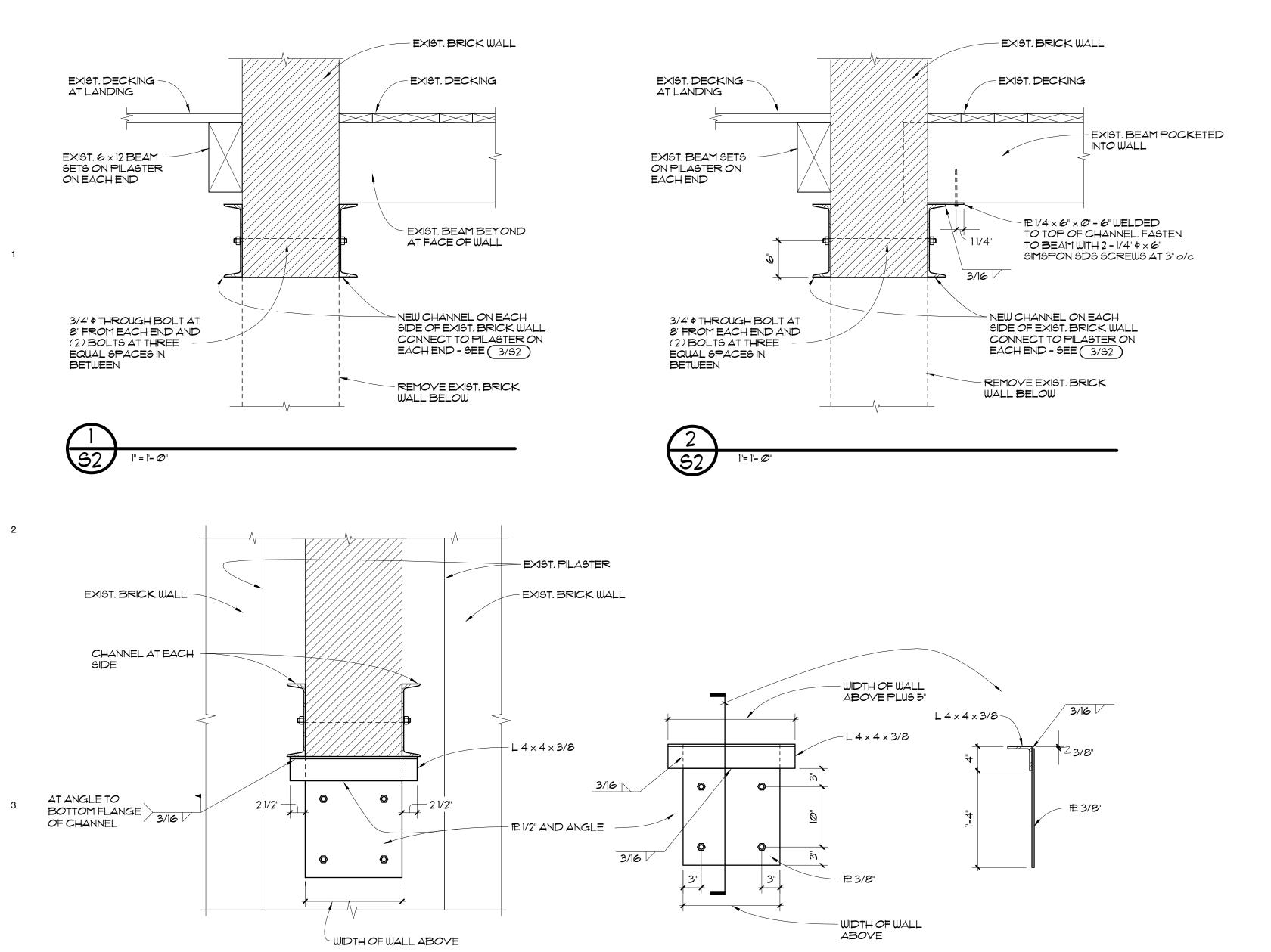
Bolts to be A307 unless noted otherwise. 5. Do not oversize drilled or punched holes with burning torch.

IBC CODE SYSTEM or MATERIAL REFERENC FABRICATION OF STRUCTURAL ELEMENTS 1704.2 MATERIAL VERIFICATION OF WELD FILLER METALS 1704.3 VERIFYING USE OF PROPER WPS'S VERIFYING WELDER QUALIFICATIONS 1704.3.1 SINGLE PASS FILLET WELDS LESS THAN OR EQUAL TO 5/16" INSTALLATION IN HARDENED CONCRETE AND COMPLETED MASONRY 1703.4.2 1704.13.3

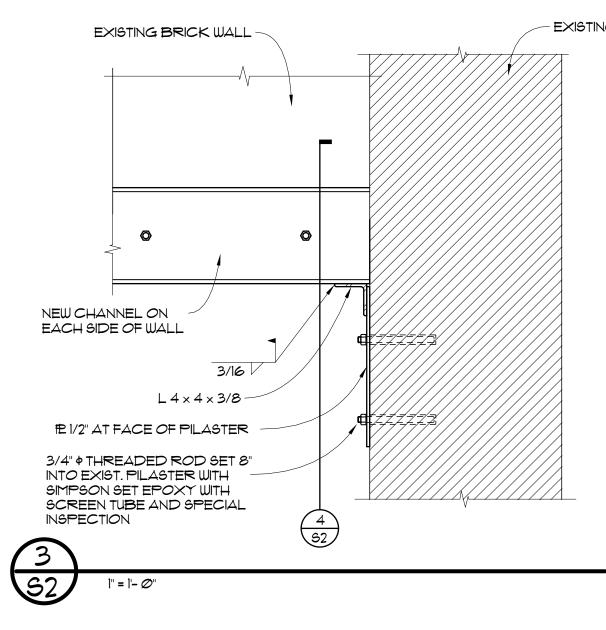
	TABLE 1									
REQUIRED STRUCTURAL SPECIAL INSPECTION										
	INSPE	CTION								
	CODE or STANDARD	FREQUE	NCY	REMARKS						
ICE	REFERENCE	CONTINUOUS	PERIODIC	HEMANIKO						
	STEEL									
2			х	REFER TO INSPECTION OF FABRICATOR REQUIREMENTS						
3	AISC 360 A3.5		х	MANUFACTURER'S CERTIFIED TEST REPORTS						
			х	COPY OF WELDING PROCEDURE SPECIFICATIONS						
.1	AWS D1.1 SECTION 6		х	COPY OF QUALIFICATION CARDS						
			х	ALL WELDS VISUALLY INSPECTED PER AWS D1.1 6.9						
F	OST INSTALLED C	ONCRETE		DRS						
.2 3.3	ICC EVALUATION REPORT	x		SPECIAL INSPECTIONS APPLY TO ANCHOR PRODUCT NAME, TYPE, AND DIMENSIONS, HOLE DIMENSIONS, COMPLIANCE WITH DRILL BIT REQUIREMENTS, CLEANLINESS OF THE HOLE AND ANCHOR, ADHESIVE EXPIRATION DATE, ANCHOR / ADHESIVE INSTALLATION, ANCHOR EMBEDMENT, AND TIGHTENING TORQUE						

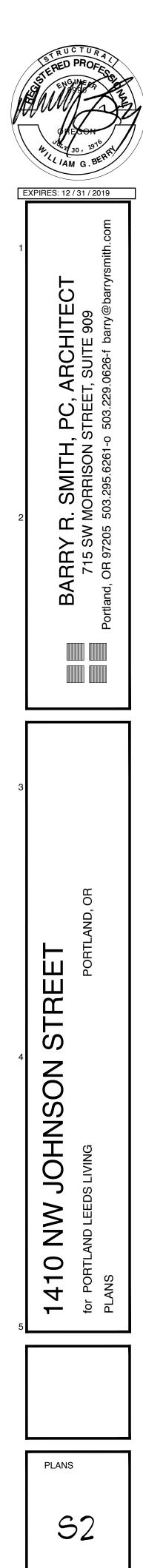


04.22.2019



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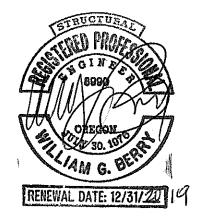


04.22.2019

- EXISTING BRICK PILASTER

STRUCTURAL CALCULATIONS FOR

Net Section Analysis for Posts and Floor Beams 1410 NW Johnson St. Portland, OR



ENGINEER WAS RETAINED IN A LIMITED CAPACITY FOR THIS PROJECT. DESIGN IS BASED UPON INFORMATION PROVIDED BY THE CLIENT WHO IS SOLELY RESPONSIBLE FOR ACCURACY OF THAT INFORMATION. NO RESPONSIBILITY AND/OR LIABILITY ARE ASSUMED BY, OR ARE TO BE ASSIGNED TO, THE ENGINEER FOR ITEMS BEYOND THAT SHOWN IN THESE CALCULATIONS.



Project: Post and Beam Analysis @ NW Johnson St.

By: BB

____ Proj. No.:<u>19-045</u>____

Sheet No.: COVER

2700 SE HARRISON ST. STE. B, MILWAUKIE OR, 97222, 503-607-0481, FAX 503-607-0486. matt@bkengineers.com

Date: 05/2019

Client: Marty Kehoe

DESIGN SUMMARY

The intent of these calculations is to verify the load capacity for floor beams and posts in an area of two-hour protection adjacent to the stairs after a fire. A Fire Protection Engineer has determined the depth of char on the members. For the floor beam the depth of char is 2" on two sides and the bottom. For the post the depth of char is 2" on all four sides. The existing floor beam is a 14x16 wood member. The effective size will be reduced to 10x14. The existing post is a 12x12 wood member. The effective size after the fire is 8x8. The calculations show that the floor beam and post will be adequate as reduced sections.

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B		NGINEERS	L		5/20/			Proj. No.: Sheet No.:	7

CALCULATE LONDS ONE FLOOR BEAM AND POST IN TWO HAR RATED AREA AD JACKENT TO STAR WELL LOADING: ROOF ; SALOW 25 PST-DENO 15 PSF FLOORS OFFICE GAMING " LIVE GARD : 50 PST-ADJACENT TO PANJITUONS : 15 pest-STANE WELL PEAD: 15 PSF -> II = 22 PSF -> II LIVE GAND = 1000 STE PEAD COME 22 POIT PARTITION WANT OPST [] DEND WIND DUCE TU PAR FINISH, DECKING PRAMING [2] ADD T PSE DUE TO GYP CEILING Project: 14th & JOHNSON STRUCTURAL KP HOE Client: MARTY Proj. No.: ENGINEERS Date: 5/2019 By: Sheet No.: 2700 SE HARRISON ST. STE. B, MILWAUKIE OR, 97222, 503-607-0481, FAX 503-607-0486, bill@bkengineers.

CHTELLE FLOOR ISTEAM NW 1 FEAST END SFETS WIEST END POORERED ON WOOD POST IN TO MASORY, -L= 5, 67 (NET) DETERMINE FLOOR UND !! LIVE LOW = 100 PSF MUOWMENTE FIFNDING DEAD LOND : 22 PSR SPREAS FOIZ GX MATEMATERE PARTITION - O PSE DELLHI. B= 1300 1251 N= (122 psz)(16,5 + 16,25)/2 = 1998 4/ OTELEINAL BIEAM' 14×16 NET = 131/2×152 M= 1998 #1, × 5,677 8 = BO 30 H-1 KETGR PIRE WITH 2ª CAME ON (3) SIDES 9.5"× 13.5" 5= (9,5)(13,5)2/6 = 288 IN 3 Project: 14th & JOHNSON STRUCTURAL Client: MARTY SCHOR Proj. No.: ENGINEERS Date: 5/2019 3 Sheet No.: 2700 SE HARRISON ST. STE, B. MILWAUKIE OR. 97222, 503-607-0481, FAX 503-607-0486, bill@bken

K1 M= g030#-1 SNET AFTER FIRIT = 288 IN 3 4= gono (12) 238 335 ps(**3** FB = 1300 psi 7 335 BIE AM IS OKAY INC. Project: 14th & JOHNSON Client: MARTY KEHOE STRUCTURAL Proj. No.: ENGINEERS Date: 5/2019 By: Sheet No.: 2700 SE HARRISON ST. STE. B, MILWAUKIE OR. 97222, 503-607-0481, FAX 503-607-0486. bill@bkengineer

AT SRE FLR DETERMINE TOTAL LOND on POST P= (100+22) (14,27) (6/2) + (50+15+15)(16,37)(15,83/2) TRIPHERRY AREA FOIL = 59924+10,3654 LOND ON POST = 16357# TRIBUTMEN WIPTH = (16,25+16,5) 2 AT ZNO FLR = 16,371 LOND on POST 15 THRE TRIBUTARY LENGTH SAME AS AT 3PD = (6+15.83)/2 Fin = 10.92' P= 16357H ST ROOF: AT 1ST FER SNOW = 25 py= PEAND GAMES IS PSF & 22 PSF LOND UN POST 15 7/172 SAME AS AT 342 FLO P= (25+15) (16,37) × 6/2 P= 16357# + (25+22)(16,37)(15.83/2) = 19654 + 6090 H = 80554 Project: 14th & JOHNSON INC. STRUCTURAL Client: MARTY SCHOR Proj. No.: ENGINEERS Date: 5/2019 Sheet No.: 2700 SE HARRISON ST. STE. B, MILWAUKIE OR. 97222, 503-607-0481

CHIZELC LIVE LOAD TOTAL MLOW MINE REPUCTION UN POST REDUCTION 15 60%0 0% ATCHER = (16,37) (6/2) +(16,37)(15,33/2) REPULTER LOANS = 50, + 130 AT ROOF DIVIDRELDAD = 180 山 194 1,15 FOR LOMD NO REALETUNA AT BOT DURNTION FACTOR = 70054 IN UFRIOR POST. Kin = 4 AT THER FROOR Ku A1 = 720 1 AT STANES: L= Lo (0:25 + 15 LIVE WADE 100 X, 57 - 60 14F (KUNT)2 AT DEFICE L = Lo (0,25 + 15 (720)1/2 4145 WAN - 50 x 0.57 = 30105F 1- Lo (0:25+0.56) P= (60+22)(16,37)(0/2) L= Lo (0.81) + (30+15+15)(16,37)(15,83(2) = 4030 # + 7775 K RENUCIE LIVE WORD AT FERCH LIEVER BY 1990 = 11,805 # FOR (3) LEVERS COAD SAMIE AT TOTAL REPUETION 15 SECOND AND FIRST 19×3= 57%0 MAR



Project: 14th & JOHNSON Client: MARTI KEHOE Proj. No.: Date: 5/2019 By: 85 Sheet No.:

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CHECK WAR CLARACITY FOR POST 9.31 NET HEAGHT OF POST, 9'9'4" AT FIRST FOR TO STECUMD PLR p- 70054 + 11,8054 + 11,8054 FINISILLED FLA TO FIN. FLA = 30,61517 1+ = 121-6" AT 7,5' x 7.5' POST HET HEAGHT OF POST Penp = 141.5K FIN. 1942 = 3/4" $p_{TECILING} = 2'/2''$ p_{LR} $p_{URLIN} = 7 \times 14'' (13'/2')$ Pur BEAM = 14+109 (151/2") MET = 12'6' - (34+22+132+152) = 12'6' - (2.69')= 9.81 Project: 14th & JOHNSON STRUCTURAL Client: MAPTI SEHOE Proj. No.: IGINEERS Date: 5/2019 Bv: Sheet No.: 2700 SE HARRISON ST, STE, B. MILWAUKIE OR, 97222, 503-607-0481, FAX 503-607-0486, bill@bkepgipeers.com



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Code References	}		4.7.6	1	~~ (~	ert and a	. (*			
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General Information										
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Wood Column

Lic. # : KW-05007984 DESCRIPTION: 9'-9.75" Column

Maximum Reactions

Maximum Reactions							Note: C	only non	-zero r	eactions a	re listed.
	X-X Axis	X-X Axis Reaction k		Y-Y Axis	Reaction	Axial Reaction	My - End Moments k-ft		k-ft	Mx - End Moment	
Load Combination	@ Base	@ Top		@ Base	@ Top	@ Base	@ Base	@ To	р	@ Base	@ Тор
+D+S+H						30.735					
+D+0.750Lr+0.750L+H						30.735					
+D+0.750L+0.750S+H						30.735					
+D+0.60W+H						30.735					
+D+0.750Lr+0.450W+H						30.735					
+D+0.750S+0.450W+H						30.735					
+0.60D+0.60W+0.60H						18.441					
+D+0.70E+0.60H						30.735					
+D+0.750L+0.750S+0.5250E+H						30.735					
+0.60D+0.70E+H						18.441					
D Only						30.735					
Lr Only											
L Only											
0.01											

S Only W Only

E Only H Only

Maximum Deflections for Load Combinations

Load Combination	Max. X-X Deflection	Distance	Max. Y-Y Deflection	Distance	
+D+H	0.0000 in	0.000 ft	0.000 in	0.000 ft	
+D+L+H	0.0000 in	0.000 ft	0.000 in	0.000 ft	
+D+Lr+H	0.0000 in	0.000 ft	0.000 in	0.000 ft	
+D+S+H	0.0000 in	0.000 ft	0.000 in	0.000 ft	
+D+0.750Lr+0.750L+H	0.0000 in	0.000 ft	0.000 in	0.000 ft	
+D+0.750L+0.750S+H	0.0000 in	0.000 ft	0.000 in	0.000 ft	
+D+0.60W+H	0.0000 in	0.000 ft	0.000 in	0.000 ft	
+D+0.750Lr+0.450W+H	0.0000 in	0.000 ft	0.000 in	0.000 ft	
+D+0.750S+0.450W+H	0.0000 in	0.000 ft	0.000 in	0.000 ft	
+0.60D+0.60W+0.60H	0.0000 in	0.000 ft	0.000 in	0.000 ft	
+D+0.70E+0.60H	0.0000 in	0.000 ft	0.000 in	0.000 ft	
+D+0.750L+0.750S+0.5250E+H	0.0000 in	0.000 ft	0.000 in	0.000 ft	
+0.60D+0.70E+H	0.0000 in	0.000 ft	0.000 in	0.000 ft	
D Only	0.0000 in	0.000 ft	0.000 in	0.000 ft	
Lr Only	0.0000 in	0.000 ft	0.000 in	0.000 ft	
L Only	0.0000 in	0.000 ft	0.000 in	0.000 ft	
S Only	0.0000 in	0.000 ft	0.000 in	0.000 ft	
W Only	0.0000 in	0.000 ft	0.000 in	0.000 ft	
E Only	0.0000 in	0.000 ft	0.000 in	0.000 ft	
H Only	0.0000 in	0.000 ft	0.000 in	0.000 ft	

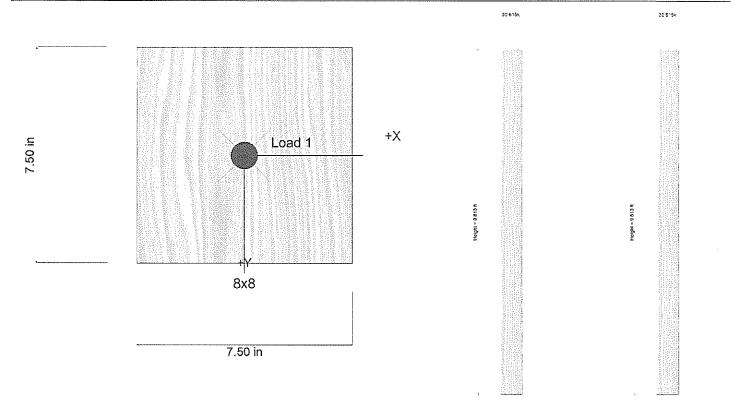


BK Engineers 2700 SE Harrison St.

Wood Column

Lic. # : KW-06007984 DESCRIPTION: 9'-9.75" Column

Sketches



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1410 NW Johnson Street

Engineering Judgement Report #1 Protection of 2-hour Rated Column

Client Name: Barry R. Smith, PC, Architect Client Address: 715 SW Morrison Street, Suite 909, Portland, OR 97205 Date: 4/19/2019

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1. PROJECT OVERVIEW

Barry R. Smith, PC, Architect, is renovating the existing 1410 NW Johnson Street building. The existing building is 3 stories with a basement of Type III-B construction and includes Group F-2 occupancy. An NFPA 13 fire sprinkler system is provided throughout.

Code Unlimited has been asked to provide engineering analysis for the fire protection of a column member adjacent to the west stair to ensure 2-hour protection is provided as required by OSSC.

2. APPLICABLE CODES, STANDARDS, AND GUIDES

- 2014 Oregon Structural Specialty Code (OSSC)
- 2015 National Design Standard (NDS) Technical Report No. 10 Fire Resistance of Exposed Wood Members – American Wood Council

3. DISCUSSION

3.1 Approach

- The proposed column assembly has been analyzed in accordance with 2014 OSSC Section 703.3 Alternative Methods for Determining Fire Resistance.
- NDS TR-10 is utilized to calculate wood char protection.
- The proposed design has been evaluated by an Oregon Licensed Fire Protection Engineer.

4. PROPOSED DESIGN

The 2-hour assembly design is composed of (1) 1/2" face layer and (1) 5/8" base layer of Type "X" gypsum wallboard wrapped around 3/8" metal hat channels which are attached to the greater than or equal to 12" x 12" in size timber column. The members are analyzed per NDS guidelines for structural requirements following a fire event. The column is not encased in an assembly and is not tested per ASTM E119 / UL 263. Therefore, the provided fire resistance will be calculated using the component added method per OSSC Section 703.2 and NDS TR-10 wood char analysis. Table 1 portrays the assembly design in detail:

Engineering Judgement Report

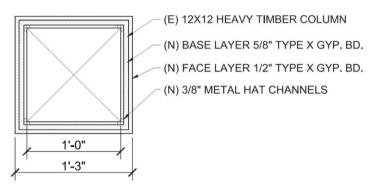


Figure 1. Proposed column assembly detail for structural column for 2-hour fire protection

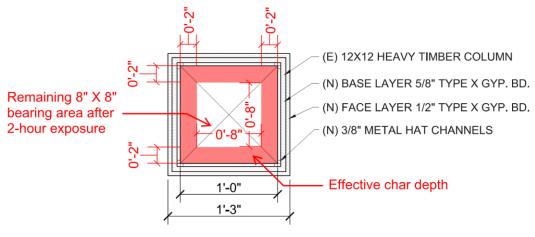


Figure 2. Bearing area of column after 2-hours (losing char on each side)

Table 1: Summary of Fire Resistance	(Condition #1-Exposed Column)
-------------------------------------	-------------------------------

Timber Column Size	Location on Column	Rating Provision	Code Section / Additional Provision	Equivalency
	12 x 12 Any side of nominal the column	(1) 5/8" Type X Gyp	OSSC Table 722.2.1.4(2)	40 minutes
		(1) 1/2" Type X Gyp	OSSC Table 722.2.1.4(2) / NDS TR-10	+ 12.5 minutes
		3/8" Hat Channels		Air Gap
		2" char depth	NDS TR-10	+ 67.5 minutes (see Section 5.1)
		TOTAL ASSEMBLY		2-hour (calculated protection)

5. ASSEMBLY ANALYSIS

There are three technical elements in the assembly design:

- Item 1. Finish materials on fire-exposed side of wall that includes Type X gypsum wallboard
- Item 2. Hat channel and clips to provide air separation between the wood member and finish materials for walls
- Item 3. Design equations for unprotected fire-resistant exposed wood members.

The analysis will follow.

Item 1. 2014 OSSC Table 722.2.1.4(2) allows for equivalent fire protection time of 40 minutes for 5/8" Type X gypsum wallboard and 25 minutes for 1/2" Type X gypsum wallboard on fire-exposed side of walls. Per NDS TR-10, time assigned to the last layer (1/2" Type X gypsum wallboard) can only be multiplied by 0.50 which, in this case, is equivalent to 12.5 minutes.

Item 2. Since we are evaluating this application with respect to a 2-hour timber column rather than wall, 3/8" hat channels will be provided. The hat channels will prevent conductive heat transfer between the interior face of the gypsum board and timber member, reducing preheating and delaying ignition of wood column in a fire event.

Item 3. Fire resistance of unprotected/exposed wood column on all four sides will be provided by the 2" wood charring. This is based on the NDS, TR-10 wood char analysis (see calculations below).

5.1 Wood Column Char

The minimum wood thickness used as a protective material (effective char thickness) is required to meet the minimum protection (in addition to the protection provided by the Type X gypsum boards). The fire resistance of the wood is permitted to be calculated by ANSI/AF&PA *National Design Specifications for Wood Construction (NDS-TR10)*. The NDS specifies an effective char layer depth of 1.8" where 1-hour of fire resistance is required based on *equation 16.2-1* shown in *Figure 3*. *Table 16.2.1A* of the NDS is reproduced below in *Figure 4*.

$$\begin{split} \beta_{eff} &= \frac{1.2\beta_n}{t^{0.187}} \end{tabular} \tag{16.2-1} \end{split}$$
 where:

$$\begin{split} \beta_{eff} &= effective \mbox{ char rate (in./hr.), adjusted for exposure time, t} \\ \beta_n &= nominal \mbox{ char rate (in./hr.), linear char rate based on 1-hour exposure} \\ t &= exposure \mbox{ time (hr.)} \end{split}$$

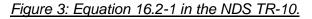


Table 16.2.1AEffective Char Rates and ChaDepths (for $\beta_n = 1.5$ in./hr.)								
Required Fire	Effective Char Rate,	Effective Char Depth,						
Endurance	β_{eff}	a _{char}						
(hr.)	(in./hr.)	(in.)						
1-Hour	1.8	1.8						
$1\frac{1}{2}$ -Hour	1.67	2.5						
2-Hour	1.58	3.2						

Figure 4: Table 16.2.1A of the NDS TR-10.

5.1.1 NDS TR-10 Evaluation

As noted in the table above, 1.8" minimum actual wood thickness is necessary for load bearing for 1-hour of fire resistance. Non-Linear char rate provides the following for the evaluated period:

$$\beta_{eff} = \frac{1.2 \beta_n}{t^{0.187}}$$

 $\beta_{eff} = \frac{1.2 X 1.5}{1.125^{0.187}}$

 $\beta_{eff} = 1.761 \text{ in./hr}$

Effective char for 67.5 minutes (1.125 hour) is: 2"

Note: Char is classified by the discoloration of the wood, while the effective char is the wood material that is no longer structurally reliable for load bearing.

6. SUMMARY

The 2-hour fire protection of the column will be achieved by the protection provided from the Type X gypsum boards and limited char protection.

From the component additive method detailed in AWC-TR10, (2) layers (5/8" + 1/2") of Type "X" gypsum wallboard provides 52.5 minutes of protection while the char will provide additional fire protection for the column exposed sides. When we consider the convective and conductive heat transfer reduction by positioning 3/8" hat channels between the wood member and gypsum wrap assembly, the assembly will have a conservative total effective equivalent time of more than 2 hours. Therefore, the assembly will easily satisfy the design requirements for 2 hours of equivalent protection.

The project structural engineer verified that the remaining wood bearing area is acceptable for support of the assembly following the evaluated fire duration.

Code Unlimited LLC

7. CONCLUSION

The proposed design of the primary structural column meets the code requirement to provide 2-hour fire resistance. The NDS calculation confirms that 2" of sacrificial wood will provide the effective char for 67.5 minutes of fire resistance, while the component additive method from AWC-TR10 provides 52.5-minute duration of fire resistance with multiple layers of Type X gypsum board. The column will maintain an adequate cross-sectional load bearing area following a fire event.

As evaluated in this EJ, the column will maintain a 2-hour fire resistance as required by the OSSC.



Franklin Callfas Principal/Fire Protection Engineer Code Unlimited



1410 NW Johnson Street

Engineering Judgement Report #2 Protection of 2-hour Rated Beam

Client Name: Barry R. Smith, PC, Architect Client Address: 715 SW Morrison Street, Suite 909, Portland, OR 97205 Date: 4/19/2019

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1. PROJECT OVERVIEW

Barry R. Smith, PC, Architect, is renovating the existing 1410 NW Johnson Street building. The existing building is 3 stories with a basement of Type III-B construction and includes Group F-2 occupancy. An NFPA 13 fire sprinkler system is provided throughout.

Code Unlimited has been asked to provide engineering analysis for the fire protection of a beam member adjacent to the west stair to ensure 2-hour protection is provided as required by OSSC.

2. APPLICABLE CODES, STANDARDS, AND GUIDES

- 2014 Oregon Structural Specialty Code (OSSC)
- 2015 National Design Standard (NDS) Technical Report No. 10 Fire Resistance of Exposed Wood Members – American Wood Council

3. DISCUSSION

3.1 Approach

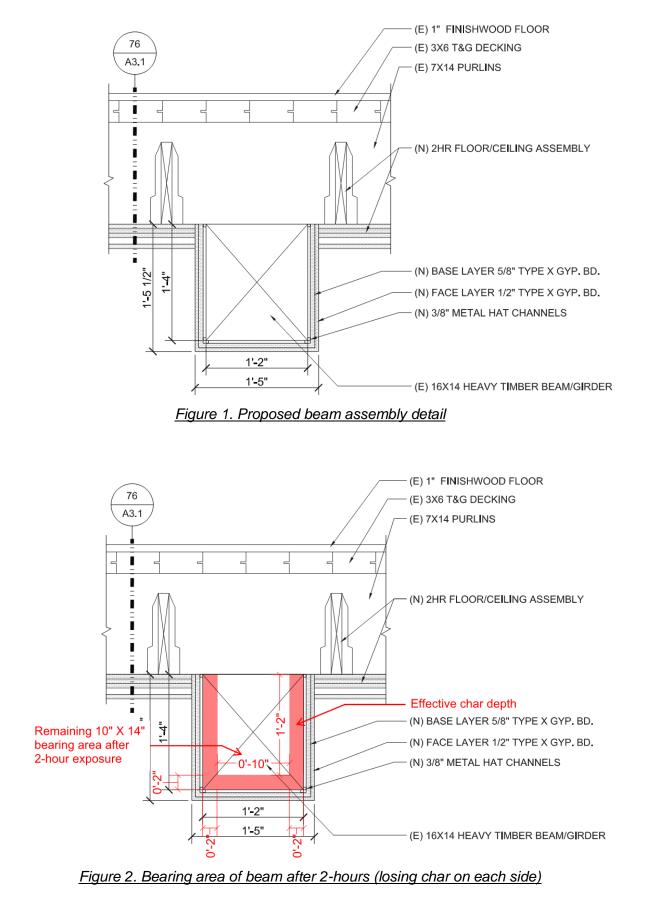
- The proposed beam assembly has been analyzed in accordance with 2014 OSSC Section 703.3 Alternative Methods for Determining Fire Resistance.
- NDS TR-10 is utilized to calculate wood char protection.
- The proposed design has been evaluated by an Oregon Licensed Fire Protection Engineer.

4. PROPOSED DESIGN

The 2-hour assembly design is composed beam exposed on three sides and consists of (1) 1/2" face layer and (1) 5/8" base layer of Type "X" gypsum wallboard wrapped around 3/8" metal hat channels which are attached to the 14" x 16" timber beam.

The beam is analyzed per NDS guidelines for structural requirements following a fire event. The beam is not tested per ASTM E119 / UL 263. Therefore, the provided fire resistance will be calculated using the component added method per OSSC Section 703.2 and NDS TR-10 wood char analysis. Table 1 portrays the assembly design in detail:

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Timber Beam Size	Location on Beam	Rating Provision	Code Section / Additional Provision	Equivalency
8" x 12" nominal (14" x 16")	Bottom three side of the beam	(1) 5/8" Type X Gyp	OSSC Table 722.2.1.4(2)	40 minutes
		(1) 1/2" Type X Gyp	OSSC Table 722.2.1.4(2) / NDS TR-10	+ 12.5 minutes
		3/8" Hat Channels		Air Gap
		2" char depth	NDS TR-10	+ 67.5 minutes (see Section 5.1)
		TOTAL ASSEMBLY		2-hour (calculated protection)

Table 1. Timber beam size and summary of equivalency for EJ of 2-hour rated wood beam.

5. ASSEMBLY ANALYSIS

There are three technical elements in the assembly design:

- Item 1. Finish materials on fire-exposed side of wall that includes Type X gypsum wallboard
- Item 2. Hat channel and clips to provide air separation between the wood member and finish materials for walls
- Item 3. Design equations for unprotected fire-resistant exposed wood members.

The analysis will follow.

Item 1. 2014 OSSC Table 722.2.1.4(2) allows for equivalent fire protection time of 40 minutes for 5/8" Type X gypsum wallboard and 25 minutes for 1/2" Type X gypsum wallboard on fire-exposed side of walls. Per NDS TR-10, time assigned to the last layer (1/2" Type X gypsum wallboard) can only be multiplied by 0.50 which, in this case, is equivalent to 12.5 minutes.

Item 2. Since we are evaluating this application with respect to a 2-hour timber beam rather than wall, 3/8" hat channels will be provided. The hat channels will prevent conductive heat transfer between the interior face of the gypsum board and timber member, reducing preheating and delaying ignition of wood beam in a fire event.

Item 3. Fire resistance of unprotected/exposed wood beam on all three sides will be provided by the 2" wood charring. This is based on the NDS, TR-10 wood char analysis (see calculations below).

5.1 Wood Beam Char

The minimum wood thickness used as a protective material (effective char thickness) is required to meet the minimum protection (in addition to the protection provided by the Type X gypsum boards). The fire resistance of the wood is permitted to be calculated by ANSI/AF&PA *National Design Specifications for Wood Construction (NDS-TR10)*. The NDS specifies an effective char layer depth of 1.8" where 1-hour of fire resistance is required based on *equation 16.2-1* shown in *Figure 3*. *Table 16.2.1A* of the NDS is reproduced below in *Figure 4*.

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$$\begin{split} \beta_{eff} &= \frac{1.2\beta_n}{t^{0.187}} \end{split} \tag{16.2-1} \\ \textbf{where:} \\ \beta_{eff} &= effective \ char \ rate \ (in./hr.), \ adjusted \ for \ exposure \\ time, \ t \\ \beta_n &= nominal \ char \ rate \ (in./hr.), \ linear \ char \ rate \ based \\ on \ 1-hour \ exposure \\ t &= exposure \ time \ (hr.) \end{split}$$

Figure 3: Equation 16.2-1 in the NDS TR-10.

Table 16.2.1AEffective Char Rates and ChaDepths (for $\beta_n = 1.5$ in./hr.)				
Required Fire Endurance (hr.)	Effective Char Rate, β _{eff} (in./hr.)	Effective Char Depth, a _{char} (in.)		
1-Hour 1½-Hour 2-Hour	1.8 1.67 1.58	1.8 2.5 3.2		

Figure 4: Table 16.2.1A of the NDS TR-10.

5.1.1 NDS TR-10 Evaluation

As noted in the table above, 1.8" minimum actual wood thickness is necessary for load bearing for 1-hour of fire resistance. Non-Linear char rate provides the following for the evaluated period:

$$\beta_{eff} = \frac{1.2 \,\beta_n}{t^{0.187}}$$

 $\beta_{eff} = \frac{1.2 X \, 1.5}{1.125^{0.187}}$

$$\beta_{eff} = 1.761 \text{ in./hr}$$

Effective char for 67.5 minutes (1.125 hour) is: 2"

Note: Char is classified by the discoloration of the wood, while the effective char is the wood material that is no longer structurally reliable for load bearing.

6. SUMMARY

The 2-hour fire protection of the beam will be achieved by the protection provided from the Type X gypsum boards and fire-resistance of the heavy timber beam.

From the component additive method detailed in AWC-TR10, (2) layers (5/8" + 1/2") of Type "X" gypsum wallboard provides 52.5 minutes of protection while the char will provide additional fire protection for the beam exposed sides. When we consider the convective and conductive heat transfer reduction by positioning 3/8" hat channels between the wood member and gypsum wrap assembly, the assembly will have a conservative total effective equivalent time of more than 2 hours. Therefore, the assembly will easily satisfy the design requirements for 2 hours of equivalent protection.

The project structural engineer verified that remaining wood bearing area is acceptable for support of the assembly following the evaluated fire duration.

7. CONCLUSION

The proposed design of the primary structural beam meets the code requirement to provide 2-hour fire resistance. The NDS calculation confirms that 2" sacrificial wood will provide the effective char for 67.5 minutes of fire resistance, while the component additive method from AWC-TR10 provides 52.5-minute duration of fire resistance with multiple layers of Type X gypsum board. The beam will maintain an adequate cross-sectional load bearing area following a fire event.

As evaluated in this EJ, the beam will maintain a 2-hour fire resistance as required by the OSSC.



Franklin Callfas Principal/Fire Protection Engineer Code Unlimited



1410 NW Johnson Street

Engineering Judgement Report #3 Protection of support for 2-hour Rated Beam

Client Name: Barry R. Smith, PC, Architect

Client Address: 715 SW Morrison Street, Suite 909, Portland, OR 97205

Date: 5/1/2019

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Joint Protection Engineering Judgement Report

1. PROJECT OVERVIEW

Barry R. Smith, PC, Architect, is renovating the existing 1410 NW Johnson Street building. The existing building is 3 stories with a basement of Type III-B construction and includes Group F-2 occupancy. An NFPA 13 fire sprinkler system is provided throughout.

Code Unlimited has been asked to provide engineering analysis for the fire protection of the support for the 2hour beam assembly as required by OSSC.



Figure 1: Existing condition between the 2-hour column and 2-hour beam assemblies

2. APPLICABLE CODES, STANDARDS, AND GUIDES

• 2014 Oregon Structural Specialty Code (OSSC) including the recently adopted Appendix N.

3. DISCUSSION

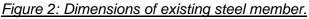
3.1 Approach

- The proposed assembly has been analyzed in accordance with 2014 OSSC Section 703.3 Alternative Methods for Determining Fire Resistance.
- The fire protection has been compared against a 2-hour fire rated column, UL Design No. X520.
- Portions of the tested assembly are modified to suit the unique design condition. The modification is analyzed for equivalency using published fire test data and accepted fire science principles.

4. PROPOSED DESIGN

The proposed 2-hour assembly design utilizes (1) 1/2" thick layer of Type C gypsum wallboard wrapped around a steel support assembly which connects 2-hour rated column and beam. The steel member protection is compared to a 2-hour fire rated column per UL X520. The steel is a continuation of the wood column below and requires equivalent protection to a tested assembly tested per ASTM E119 / UL 263. The provided fire resistance will be based on the UL assembly comparison per OSSC Section 703.3. Table 1 portrays the assembly design in detail:





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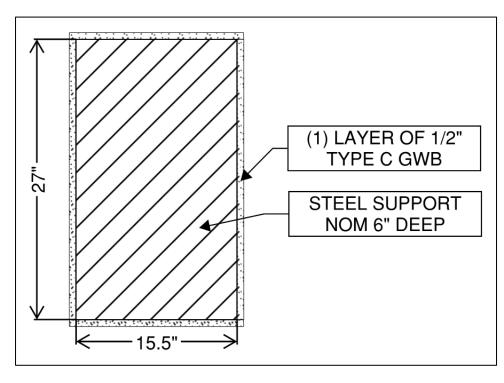


Figure 3: Proposed protection of steel joint, plan view.

5. ASSEMBLY ANALYSIS

5.1 W/D Ratio

The calculated W/D ratio of the steel member is determined for comparison of inherent fire-resistance against the tested column. The W/D value is a ratio between the linear weight of the steel (W), and the perimeter exposed to fire (D). The linear weight of the existing support member is determined with the known density of ³/₄" nominal thick steel plates (30.60 lbs/ft²) (Engineering Toolbox *Steel Plates – Size and Weight*, 2009).

Joint Weight, using surface areas in Figure 2

Top plate: $30.60 \text{ lbs/ft}^2 \times 2.91 \text{ ft}^2 = 89.05 \text{ lbs}$ Side plates: $30.60 \text{ lbs/ft}^2 \times (0.80 \text{ ft}^2 \times 2) = 48.96 \text{ lbs}$ Front and back plates: $30.60 \text{ lbs/ft}^2 \times (0.46 \times 2) = 28.15 \text{ lbs}$ Approximate total weight = 166.16 lbsDistributed across length of L1 = 27" = 2.25 ft: 166.16 lbs / 2.25 ft =**73.85 \text{ lbs/ft}**

Heated Perimeter

Nominal depth x 4 sides = 6.75 in. x 2 = **13.5 in**. Calculated W/D ratio = 5.47 The minimum W/D ratio per the tested UL X520 (Figure 5) is:

W14x228 W/D = 2.44

Wide Flange Steel Specifications				
Steel Size	W/D	HP/A		
W12X279	3.48	39		
W14X311	3.26	41		
W12X252	3.19	42		
W14X283	3.00	45		
W12X230	2.94	46		
W14X257	2.75	49		
W12X210	2.72	49		
W14X233	2.52	53		
W14X228	2.44	55		

Figure 4: W/D ratio per UL X520.

5.2 UL Design No X520 Comparison

The proposed is a steel assembly, protected with (1) layer of 1/2" Type C gypsum board. It is compared to the 2-hour fire rated column per the tested assembly UL X520 as shown below.

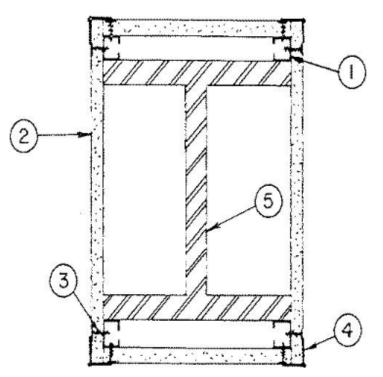
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Design No. X520

October 24, 2017

Rating - 2 Hr.

* Indicates such products shall bear the UL or cUL Certification Mark for jurisdictions employing the UL or cUL Certification (such as Canada), respectively.



1. Steel Studs — 1-5/8 in. wide with leg dimensions of 1-5/16 and 1-7/16 in. with a 1/4 in. folded flange in legs fabricated from 25 MSG galv steel, 3/4 by 1-3/4 in. rectangular cutouts punched 8 and 16 in. from the ends. Steel stud cut 1/2 in. less in length than assembly height. Alternate Construction, Steel Framing Members* — Clips attached to column flange 4 ft. OC and 1-1/4 in. from the top and bottom of column. 1-1/4 in. by 1-1/4 in. 28 MSG angle laid in place over clip. Angle cut 1 in. less in length than assembly height. JOHN WAGNER ASSOCIATES INC, DBA GRABBER — Types CB, CB1 Clips.

 Gypsum Board* — 1/2 in. thick, one layer. Nom 3/32 in. thick gypsum veneer plaster may be applied to the entire surface of Classified veneer baseboard.
 ACADIA DRYWALL SUPPLIES LTD — Type C.

AMERICAN GYPSUM CO - Type AG-C

CERTAINTEED GYPSUM INC - Type FRPC, SF3 or Type C.

CONTINENTAL BUILDING PRODUCTS OPERATING CO, L L C - Type LGFC-C/A.

GEORGIA-PACIFIC GYPSUM L L C - Types 5, C, DAP, DA, DAPC, TG-C.

NATIONAL GYPSUM CO - Types -eXP-C, FSW-G, FSW-1, FSK-G, FSW-C, FSK-C.

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PAECO BUILDING PRODUCT S L L C, DBA PABCO GYPSUM — Types PG-3, PG-C.
THAI GYPSUM PRODUCT S PCL — Type C.

Sterws — 1 in. long self-drilling, self-tapping steel screws, spaced vertically 12 in. O.C.
Steel Column — Min size of column, a W14X228, with outside dimensions of 16 by 15-7/8 in. with a flange
tickness of 1-11/16 in., a web thickness of 1-11/16 in., and a cross-sectional area of 67.06 sq in.

Indicates such products shall bear the UL or cUL Certification Mark for jurisdictions employing the UL or cUL
Ertification (such as Canada), respectively.

Lat Updated on 2017-10-24

Table 1: Comparison between the proposed design and the 2-hour fire rated UL X520 assembly

Element	UL Assembly Design No. X520	Proposed Design
1. Steel Member	Steel Column: W14x228 (W/D = 2.44 – Column) (Figures 4 and 5)	Steel Support (W/D = 5.47) (Figure 1 and Section 5.1) Significantly Higher Inherent Fire- Resistance
2. Gypsum Board	1/2 in. thick, one layer . Nom 3/32 in. thick gypsum veneer plaster may be applied to the entire surface of Classified veneer baseboard.	One (1) layer of 1/2" thick Type C gypsum board wrapped around the joint to provide encasement protection. Equivalent
Fire-Resistance Rating	2-Hour	2-Hour (minimum)

6. SUMMARY

The 2-hour fire protection of the steel connection will be achieved by a GWB membrane provided through 1 layer of Type C gypsum board and the inherent fire-resistance of steel, as compared to UL X520 (Table 1).

While evaluating fire resistance requirement of members, different sized beam and columns are compared against each other through a factor referred to as the W/D Ratio. The weight per unit length of a member is divided by the length of exposed heated perimeter area to determine the inherent fire resistance of a member. Lower W/D ratios correspond with thinner steel members that will be subject to earlier failure when heated.

During this evaluation, an encased column assembly UL X520 was referenced, where the minimum required W/D ratio (2.44) is far less than the proposed design W/D ratio (5.47). The proposed support member is protected with ½" Type C gypsum, which is the equivalent protection used in UL X520. The greater W/D ratio and equivalent Type C gypsum board encasement ensures a minimum of 2-hour fire-resistance as compared to the 2-hour fire rated column assembly, UL X520.

Adjacent Beam and Column protection will utilize 2-hour assemblies as provided in EJ#1 an EJ#2 (See Appeal #20220).

7. CONCLUSION

The proposed assembly meets the code requirement to provide 2-hour fire-resistance and continuous fire protection of the adjacent 2-hour rated beam and column. The proposed design provides greater fire-resistance compared to the tested W-column in UL X520.

The significantly greater inherent fire-resistance of the steel member in addition to the equivalent Type C gypsum board encasement per UL X520 exceeds the protection of the tested column. Therefore, the proposed design for the steel support member encased with 1/2" Type C gypsum board will exceed the required minimum 2-hour fire-resistance required by code, as detailed in the report.



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