



September 27, 2012

Mr. Sean Murray
Alliant Systems
1600 NW 167th Place, Suite 330
Beaverton, Oregon 97006

RE: HVAC Work for KEEN 3rd Floor Server Room; Cooling Units, Roof Top Condensing Units & Piping
Application 12-172563-000-00-FA
Structural Plan Check Response

Dear Sean:

Below is our response to the structural plan check sheets that we received from the City of Portland Bureau of Development Services dated September 27, 2012. This response is intended to be reviewed in conjunction with the attached structural calculations and drawing SK1, dated September 27, 2012.

Item 1

Please address the adequacy of the roof structure to support the new condensing units located on top of the roof.

KPFF: Please reference attached structural calculations verifying the adequacy of the roof structure to support the new condensing units located on top of the roof.

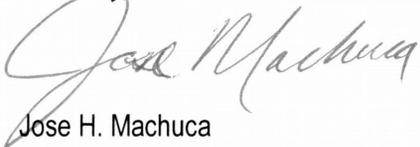
Item 2

The detail for the attachment between the rooftop condensing unit sleeper and the roof structure is indicated to be by others. Please provide the detail for that connection.

KPFF: Please reference sheet SK1 for the connection detail.

If you have any questions or need further information, please call me.

Sincerely,

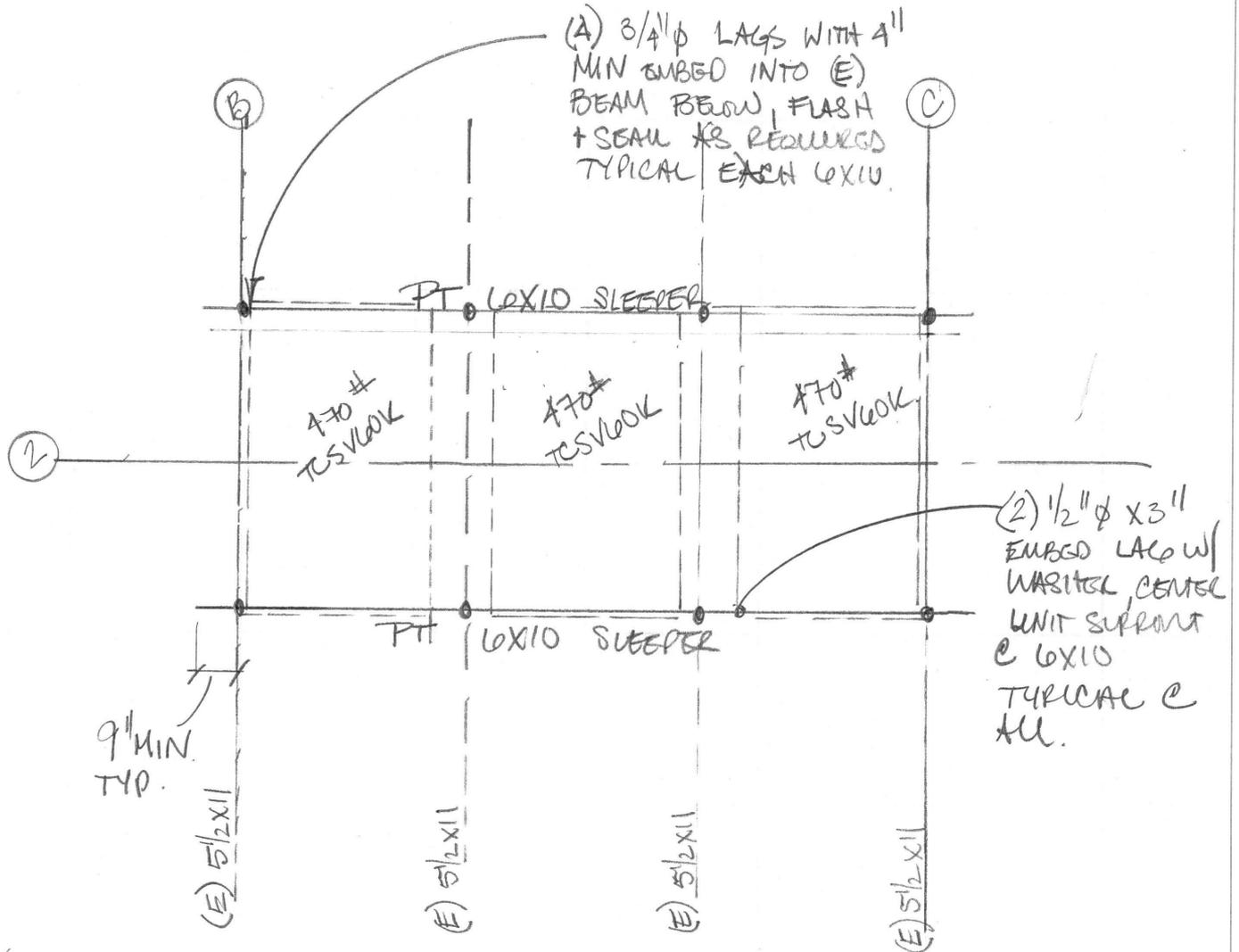


Jose H. Machuca

JHM/jkd
212221\10 - pes - hvac - 9-27-12.doc



Project PERL	By	Sheet No.
Location 1313 LOUISAN	Date 9/4	SK1
Client ACHANT.	Revised	Job No.
COORNER TOWER.	Date	



NOTE

1. AMBER SHALL BE DFL No 1, PRESSURE TREATED.
2. ALL LAGS SHALL BE GALVANIZED
3. SEAL + FLASH SLEEPER TO EXISTING ROOF STRUCTURE AS REQUIRED
4. NOTIFY ENGINEER IF FIELD CONDITIONS VARY FROM THOSE SHOWN

SK1 CONNECTION BETWEEN ROOFTOP & SLEEPER

CHECK STRUCTURE FOR ADDITIONAL
3 UNITS @ 470# EACH DISTRIBUTED
TO 2 POSTS

$$\text{TOTAL ADDITIONAL PER POST} \\ = 3 \cdot 470\# / 2 = 705\#$$

TOTAL ADD PER COLUMN + 7% INCREASE

$$147.2 + 0.705 / 147.2 \\ = < 0.5\% \text{ OK.}$$

CHECK TOTAL ADDITIONAL ON
ROOF ALONG 28 UNIFORM ASSUMING
20 PSF BASE

$$705\# \times 2 / 6' \times 20' \text{ (INFLUENCE AREA BETWEEN)}$$

11.8 PSF.

ASSUME 1/2 TOTAL LOAD UNIFORM
DIST ON (E) 5 1/2' X 11' BEAM.
CHECK BEAM FOR LOAD.

$$\begin{array}{r} 20 + \dots = 20 \text{ DL.} \\ 25 \text{ LL.} \\ \hline 45.0 \text{ TL.} \end{array}$$

$$M = \left(\frac{45.0 \times 705\#}{5.25' \times 20'} \right) (11')^2 / 8 \\ = 8688 \# \cdot \text{ft}$$

$$S = 110 \text{ in}^3 \quad A = 60.5 \text{ in}^2$$

$$f_b = 8688 \times 12 / 110 = \underline{948 \text{ PSI}} \text{ OK}$$

$$f_v = 2172 (3/2) / 60.5 = \underline{54 \text{ PSI}} \text{ OK}$$

$$F_b' = 1508 \quad F_v' = 195$$

BEAM OK TO SUPPORT ADDL
LOADING BY UNIT.

GIRDELS OK BY INSPECTION
W/ ADDITIONAL
 $705\# / 2 = 353\# \text{ SHEAR.}$

COOLING TOWER SEISMIC DESIGN AND BASE CHECK.

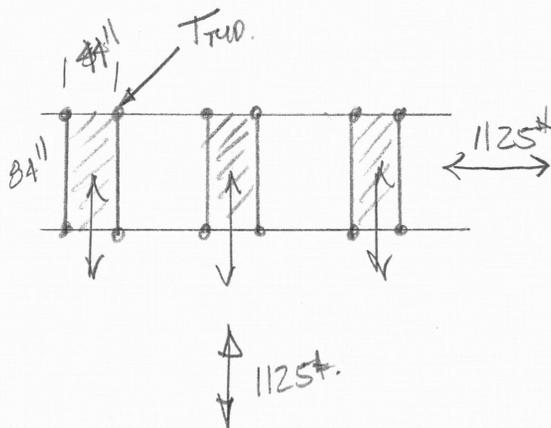
$$W_p = 170 \# \times 3 = 1410 \#$$

$$F_{ph} = 0.7 - 1.14 \cdot 1410 \# = \underline{1125 \#}$$

$$F_{pv} = 0.7 - 0.2 \cdot S_d \cdot 1410 \# = \underline{100 \#}$$

↑
0.506

DESIGN SLEEPER TO RESIST D.T + SHEAR BY (3) UNITS



$$T_{E/W} = \frac{0.6 \cdot 470 \#}{4} - \frac{1125 \# (27.5'')}{3 \cdot 12 \cdot 44'' \cdot 2} - 33 \# / 4$$

$$= 70.5 \# - (118 \# + 8 \#)$$

$$= \underline{55 \#} \uparrow \text{ MAX. } \longleftrightarrow$$

$$T_{N/S} = \frac{0.6 \cdot 470 \#}{4} - \frac{1125 \# (27.5'')}{3 \cdot 12 \cdot 44'' \cdot 2} - 33 \# / 4$$

$$= 70.5 \# - (118 \# + 8 \#)$$

= ϕ No NET T.

$$V_{BOUL} = 1125 \# / 4 \cdot 3 \text{ units} = \underline{94 \#}$$

$$T_{BOUL} = 55 \#$$

(2) 9/16 HOLES PROVIDED FOR UCL. USE 1/2" ϕ UCL INTO SLEEPER.

$$V_{AU} = 1.6 \cdot 320 \# = \underline{512 \#}$$

$$T_{AU} = 1.6 \cdot (607 \# / \text{IN} \cdot 3'') = \underline{1761 \#}$$

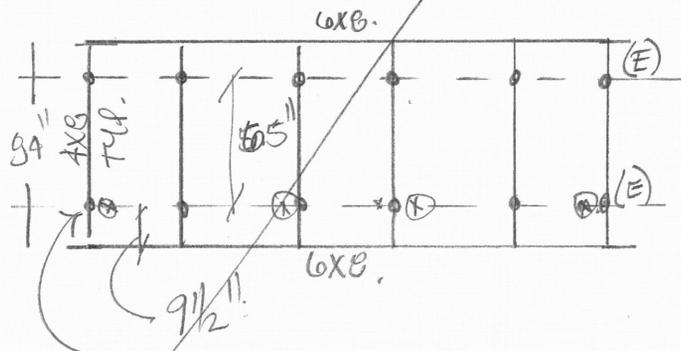
$$\frac{94}{2 \cdot 512 \#} + \frac{55 \#}{2 \cdot 1761 \#} =$$

$$0.09 + 0.016 = \underline{0.106} \ll 1.$$

USE (2) 1/2" ϕ GALV UCL SCREWS W/ MIN 3" PENETRATION

DESIGN SLEEPER ATTACHMENT TO STRUCTURE.

USE LXB W/NO SLEEPER + 4XB. PERPENDICULAR SLEEPER TO SUPPORT + ACCOMMODATE FEET.

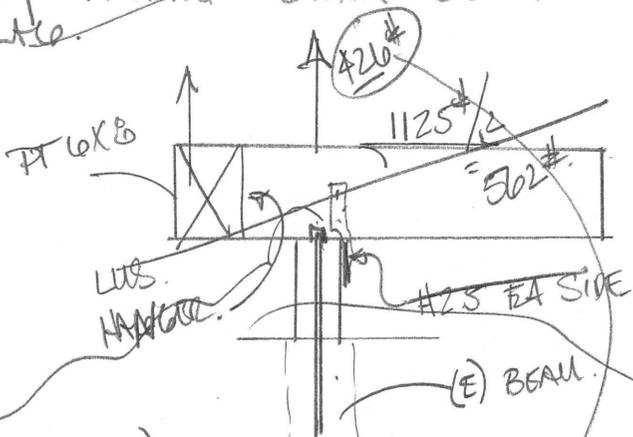


$$T_{SUPPORT} = \frac{94}{65} \cdot 55 \# = 71 \# \text{ PER BOX.}$$

$$\text{OR } 142 \# / \text{UNIT}$$

$$\text{OR } \underline{426 \#} \text{ TOTAL}$$

USE PT 4X8 SLEEPER ALONG
w/ EXISTING 5X11 BEAM.
LACE.



MIN (4) LACES PER SIDE.

$$T = 420 / 4 = 100 \#$$

$$V = 502 / 4 = 125 \#$$

(A) 5/8" ϕ LACE w/ 4" PENETRATION
DL INTO (E) BEAM.

PT 4X8 TO SUBSTRATE
USE SIMPSON H25A (MIN).

$$T = 502 \# / 6 = 84 \#$$

130# OK.

ADJUST.

$$420 \# / 6 = 70 \#$$

535# OK.

HANGER TO 6X8
LWS 46 T=1000#
OK.

BY INSPECTION ALL LUMBER OK.
MAX V ON 4X8.

$$\frac{470 \#}{2} + 920 \# + 375 \#$$

$$= 244 \# \text{ MAX SHEAR}$$

$$244 / 3.25 \cdot 7.5 = 15 \text{ psi OK}$$

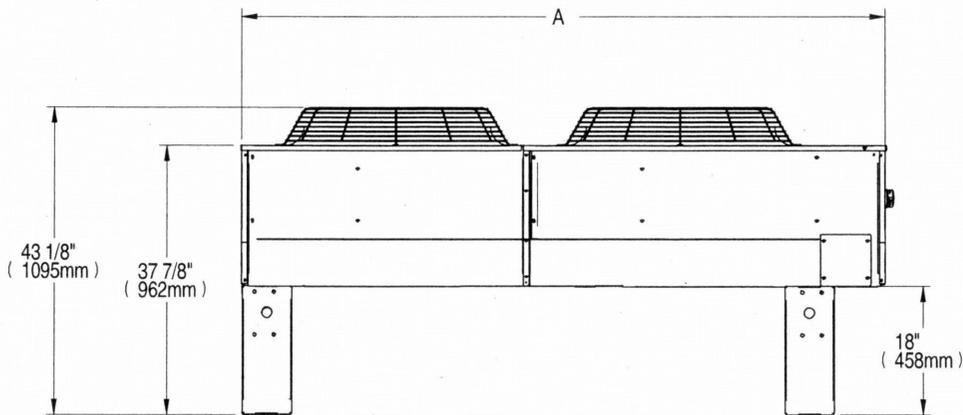
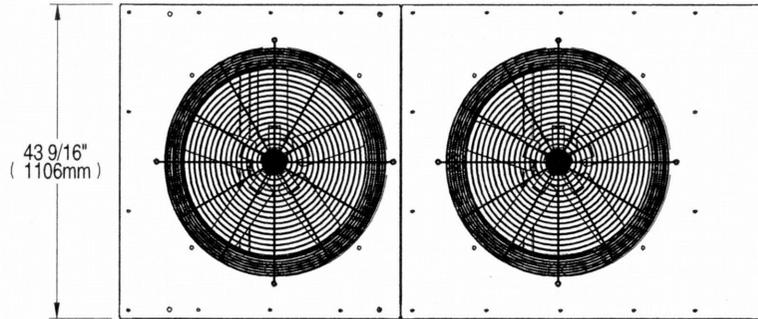
4X8 PT OK

BENDING OK -

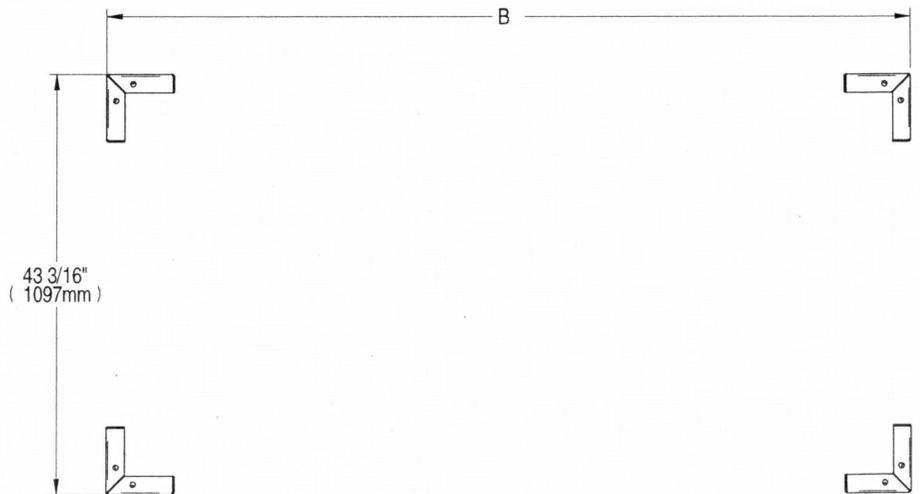
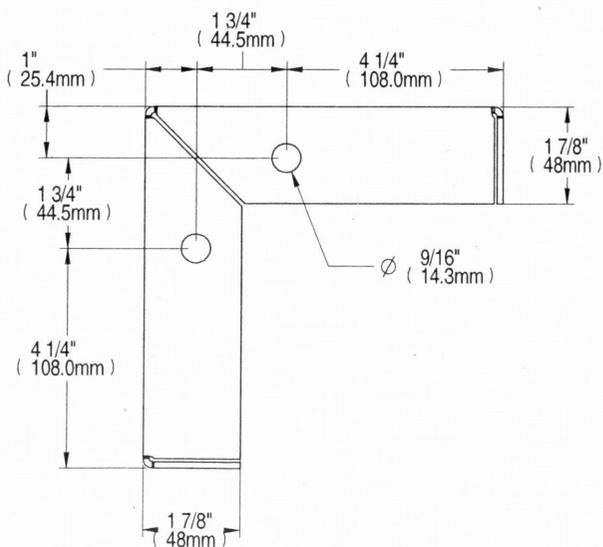
4

CABINET & ANCHOR DIMENSIONAL DATA

R-410A VFD CONTROL SINGLE CIRCUIT CONDENSERS 60 Hz

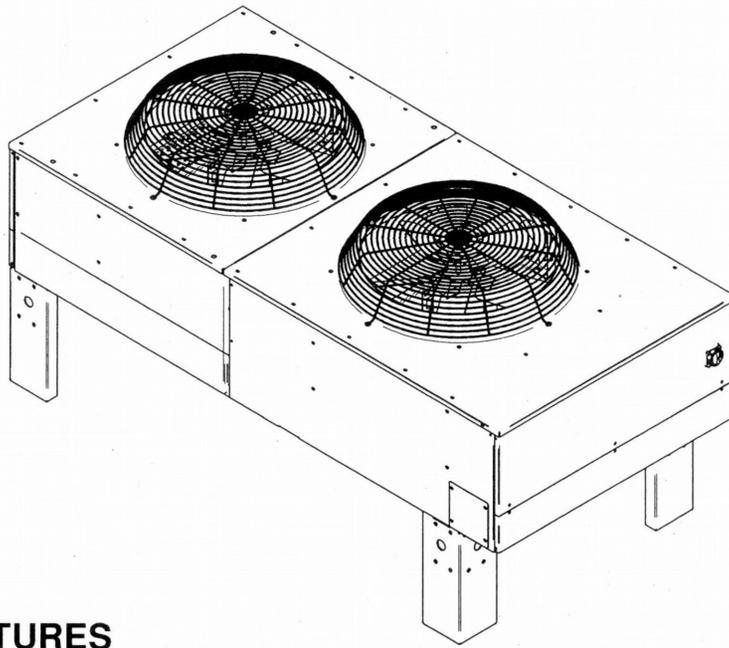


LIEBERT MODEL NO.	NO. FANS	A		B		NET WEIGHT	
		IN.	MM	IN.	MM	LBS.	KG
TCSV28K	1	51 1/2	1308	44	1118	325	148
TCSV60K	2	91 1/2	2324	84	2134	470	213
TCSV90K	3	131 1/2	3340	124	3150	670	304



LIEBERT AIR COOLED R-410A VFD CONTROL CONDENSERS

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STANDARD FEATURES

COIL The coil is constructed of copper tubes in a staggered tube pattern. Tubes are expanded into continuous, rippled or enhanced aluminum type fins. The fins have full depth fin collars completely covering the copper tubes which are connected to heavy wall type L headers. Inlet coil connector tubes pass through relieved holes in the tube sheet for maximum resistance to piping strain and vibration. Coils are factory leak tested at a minimum of 475 PSIG, dehydrated, then filled and sealed with a nitrogen holding charge for shipment.

FANS Blades are constructed of zinc plated steel or aluminum with a diameter of 26 inches and secured to the fan shaft by a heavy duty hub with set screw. Fan guards are heavy gauge, close meshed, steel wire with corrosion resistant finish. Fans are factory balanced and tested before shipment.

FAN MOTORS The variable speed fan motor is a specifically designed inverter duty motor with permanently lubricated ceramic bearings. The Liebert variable frequency drive (VFD) control system provides overload protection for the variable speed motor. Each ambient-temperature-controlled fan motor has built-in overload protection. All motors have rain slingers, permanently lubricated bearings and are rigidly mounted on die-formed galvanized steel supports.

HEAD PRESSURE CONTROL The Liebert VFD Condenser control system is complete with variable frequency drive (VFD), inverter duty fan motor operating from 0% to 100% motor RPM based on head pressure, refrigerant pressure transducers, ambient-temperature thermostat(s), motor overload protection, and electrical control circuit factory wired in the control panel. VFD control is always furnished on the fan adjacent to the connection end of the condenser which runs continuously with the compressors. Other condenser fans are controlled by ambient thermostats and are either "on" or "off". This system allows for operation at ambient conditions as low as -20°F (-28.9°C).

HOUSING The condenser housing is constructed of bright aluminum sheet and divided into individual fan sections by full width baffles. Structural support members, including coil support frame, motor, and drive support, are galvanized steel for strength and corrosion resistance. Aluminum legs are provided with rigging holes for hoisting the unit into position.

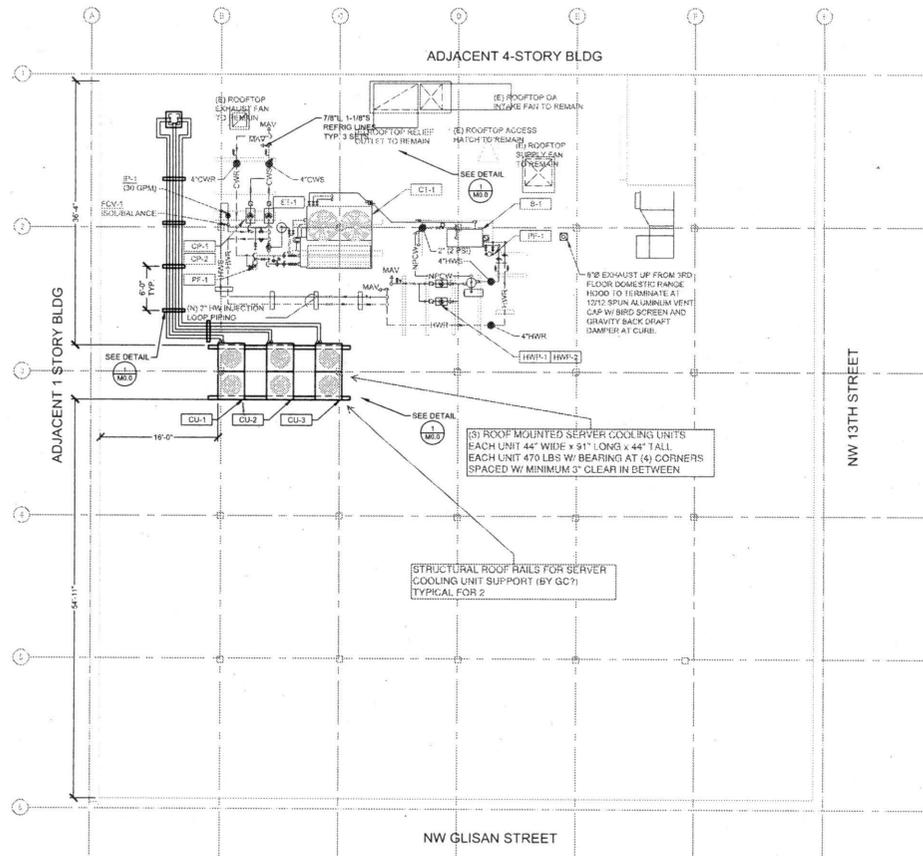
SPD & UNIT DISCONNECT SWITCH Surge Suppression Device and locking disconnect factory installed and wired in enclosed condenser control section.

ALARM CONTACTS Normally open dry contacts provided for indication of VFD and SPD alarm condition.

OPTIONAL FEATURES

FUSIBLE PLUG SERVICE KIT Provides compliance for local codes requiring fusible-plug-type pressure relief devices. Shipped loose for field installation on each liquid line.

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ALLIANT SYSTEMS, LLC
 1600 NW 167th PL, STE 330
 BEAVERTON, OR 97006
 PHONE: 503/619-4000
 FAX: 503/230-9238
 WWW.ALLIANT-SYSTEMS.COM
 CCB# 153420



REVISIONS: DATE

KEEN
 SERVER ROOM

1313 NW GLISAN ST.
 PORTLAND, OR

DRAWING REVIEW		
DEPT	INITIALS	DATE
CAD		
DESIGNER		
P.M.		
ENGINEER		
FIELD		

MECHANICAL
 ROOF LEVEL
 HVAC PLAN

DESIGNED BY: S. MURRAY
 CHECKED BY: E. STOYAN
 PROJECT NUMBER: C-0330-22074

PRELIMINARY

DATE: 12/11/11
M2.5

1

STRUCTURAL CALCULATIONS

FOR:

Alliant Systems

REGARDING:

HVAC Seismic Connections

LOCATION:

Keen Server Room
1313 NW Glisan St., Portland, OR

AE1242

September 21, 2012



Expires 12/31/13

Project: HVAC Seismic Connections - Keen Server Room
 Location: 1313 NW Glisan St., Portland, OR
 Client: Alliant Systems

Page: 2 of 3
 Job #: AE1242
 Date: Sept. 21, 2012

Design of the connection of a HVAC unit to wood floor system

2010 OSSC /ASCE 7-05 Sec. 13.6 - Mechanical and Electrical Component Seismic Design Requirements

Loading : IRC-1,2,3
 Unit Weight = 850 lbs. (Wp) maximum
 Centroid Height = 3.5 ft (h)
 Floor Height = 20.00 ft. (hr) maximum

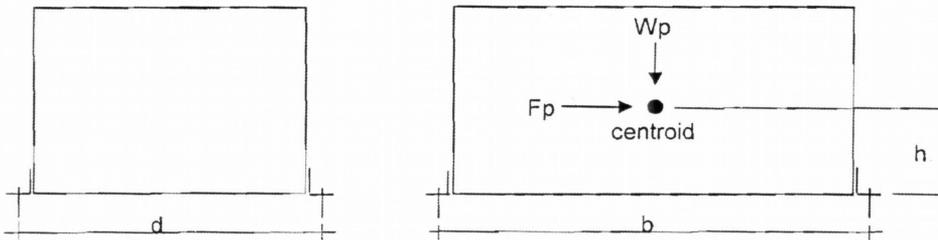
Design Forces :

Use Loads For: ASD (ASD or USD)

Equipment Element :

Fp = 0.254 (see page 1)

850 lbs x Fp = 215.90 lbs.



Connection Design :

Tension Load: Overturning Moment 10579 in. lbs. (Fp x h)
 Resisting Moment 18742.5 in. lbs. (Wp/2 x d x .9)
 Mr > Mo - No Tension Force

Shear connections:

Unit to Floor:

of anchor attachments (n): 2 per side of unit d= 49 in.
 Base Material: I-joists w/ 3/4 ply & 4x4 blocking b= 89 in.
 h= 49 in.
 Perimeter = 276 in.

Shear force per fastener = 108 lbs (Fp / n)

Use (4) L2x4x12 gage angles w/(2) Simp SDS screws at SUBFLOOR and (3) #10 sheet metal screws at unit base flange
 Allowable Shear per angel connection = 840 lbs (3x6)

STRUCTURAL NOTES

GENERAL

THE CONTRACTOR IS RESPONSIBLE FOR CHECKING THE PLANS PRIOR TO THE START OF CONSTRUCTION AND SHALL NOTIFY THE ENGINEER OF ANY ERRORS OR INCONSISTANCY WITH THE MECHANICAL OR SUPPLIER DRAWINGS. SHOULD QUESTIONS ARISE REGARDING THE INFORMATION SHOWN ON THESE DRAWINGS THE CONTRACTOR SHALL CONTACT THE ENGINEER BEFORE PROCEEDING. THE ENGINEER IS NOT RESPONSIBLE FOR IMPROPER CONSTRUCTION PRACTICES DUE TO MISUNDERSTANDING OR MISUSE OF THE INFORMATION ON THESE DRAWINGS.

THE CONTRACTOR SHALL BE SOLELY AND COMPLETELY RESPONSIBLE DURING THE CONSTRUCTION PERIOD FOR ALL CONDITIONS AT THE CONSTRUCTION SITE, INCLUDING SAFETY OF PROPERTY AND PERSONS. THE ENGINEER'S VISITS TO THE SITE AREA ARE NOT INTENDED, NOR SHALL THEY BE CONSTRUED TO INCLUDE A REVIEW OF THE ADEQUACY OF THE CONTRACTOR'S SAFETY MEASURES. THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE STRENGTH AND STABILITY OF ALL SHORING, BRACING, SCAFFOLDING AND TEMPORARY SUPPORTS.

THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE WATERPROOFING AND FLASHING DETAILS OF ALL STRUCTURAL ELEMENTS INDICATED ON THESE DRAWINGS.

WRITTEN DIMENSIONS SHALL TAKE PRECEDENCE OVER SCALE DIMENSIONS. DO NOT SCALE DRAWINGS. ALL STRUCTURAL DIMENSIONS ARE TO FACE OF FRAMING, UNLESS NOTED OTHERWISE.

CONTRACTOR SHALL REVIEW DRAWINGS WITH RESPECT TO MATERIALS, LAYOUT, ELEVATIONS, AND DIMENSIONS BEFORE STARTING WORK. ANY APPARENT DISCREPANCY, AMBIGUITY, OR CONFLICT IN THESE DRAWINGS SHALL BE BROUGHT TO THE ENGINEER'S ATTENTION. ANY REVISION TO THESE DRAWINGS SHALL BE COMPLETED BEFORE PROCEEDING WITH THE WORK AFFECTED.

CODES AND STANDARDS

2010 OREGON STRUCTURAL SPECIALTY CODE

DESIGN LOADS

DEAD LOAD - ALL COMPONENT WEIGHTS

SEISMIC LOAD - $S_s = .983$; $S_1 = .346g$; $F_p = .254 W_p$ (ASD)

SCOPE OF WORK

THESE DRAWINGS AND CALCULATIONS ONLY PERTAIN TO THE SEISMIC CONNECTIONS BETWEEN THE INDICATED UNITS TO THEIR IMMEDIATE SUPPORTING STRUCTURAL ELEMENT (FLOOR SYSTEM, ROOF-TOP SLEEPERS, ETC). THE VERTICAL LOAD ANALYSIS OF THE STRUCTURE ITSELF IS NOT PART OF THIS WORK AND ARE BY OTHERS.



EXP. 12/31/13

HVAC UNITS - SEISMIC CONNECTIONS

KEEN SERVER ROOM
1313 NW GLISAN ST., PORTLAND, OR

STRUCTURAL NOTES



2345 NE 37th Ave., Portland, OR 97212 P 503.281.6441 F 503.281.6441 C 503.730.3357 E archereng@comcast.net

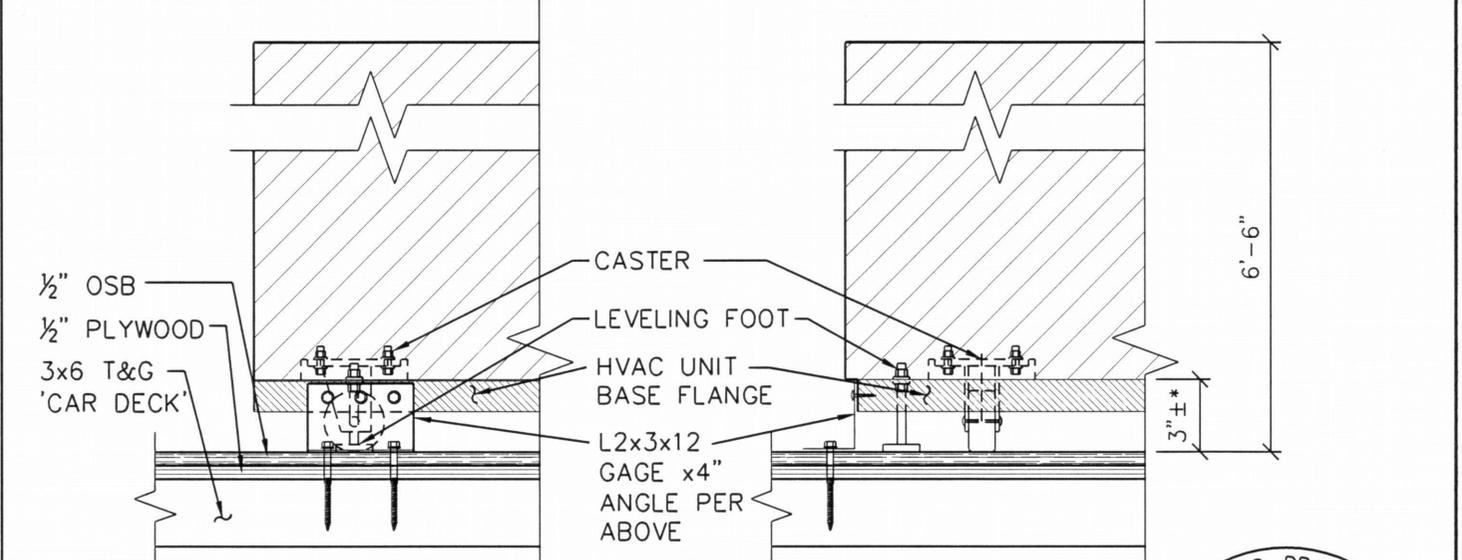
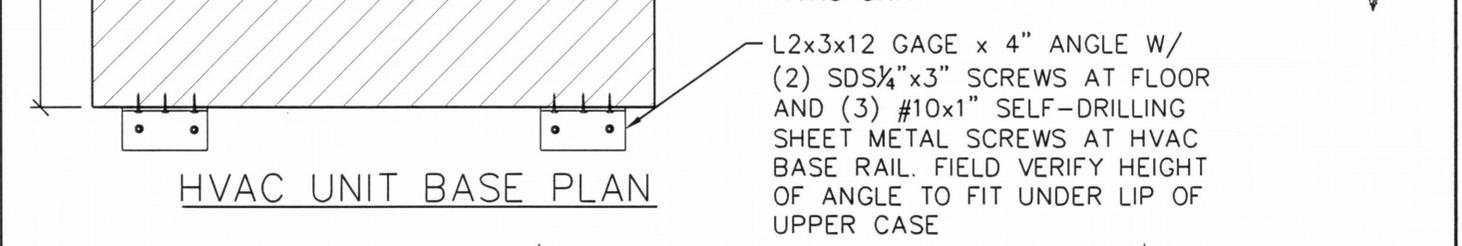
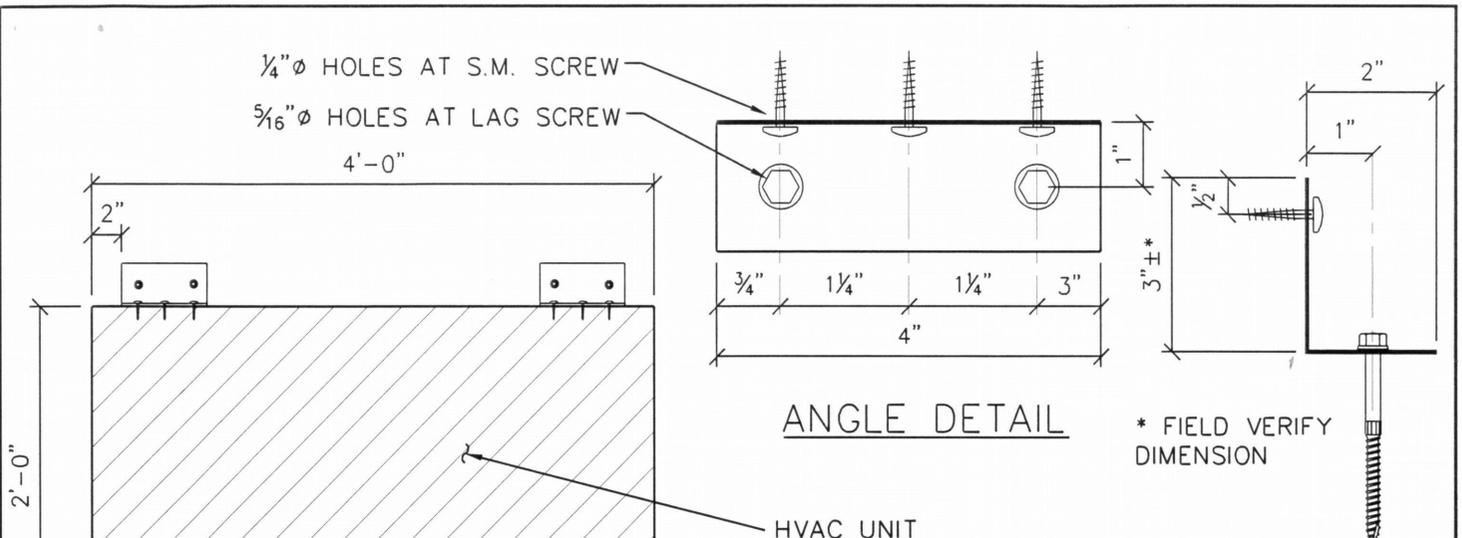
ALLIANT SYSTEMS
1600 NW 167TH PL
BEAVERTON, OR 97006

BY: MDA

DATE: 9/21/12

PROJECT: AE1242

DETAIL
1/S1



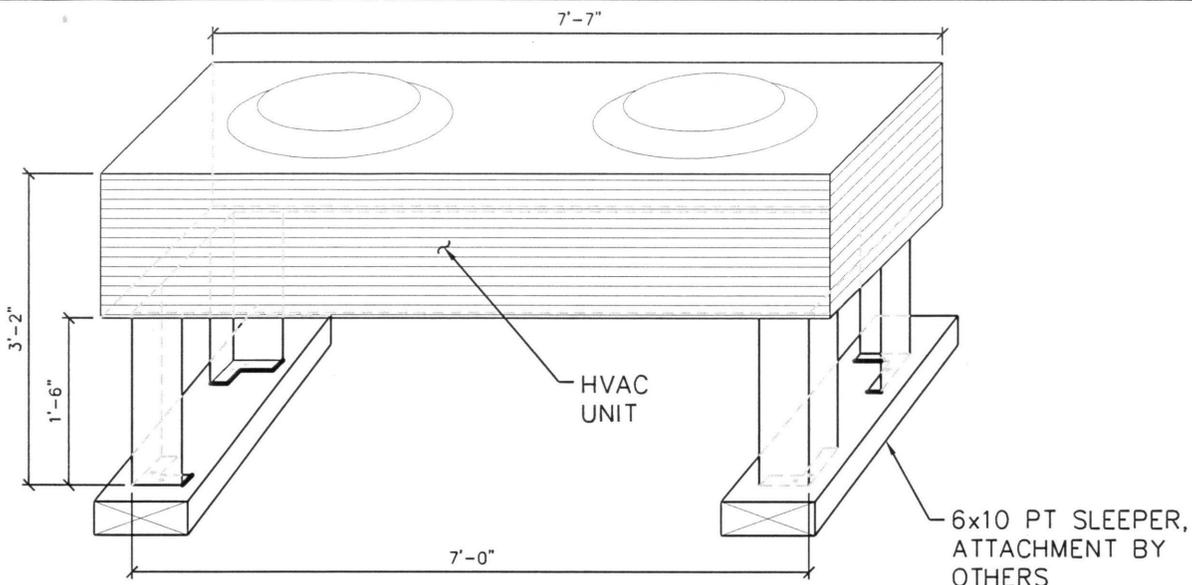
1 HVAC CONNECTION DETAIL
S2 NTS CURB6



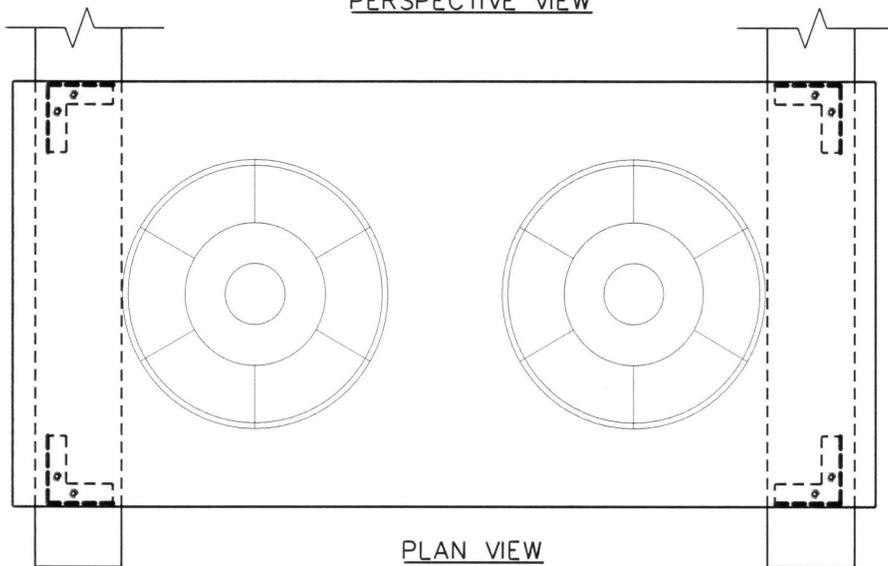
EXP. 12/31/13

<p>HVAC UNITS - SEISMIC CONNECTIONS KEEN SERVER ROOM 1313 NW GLISAN ST., PORTLAND, OR</p>	<p>ROW COOLER UNITS IRC-1,2,3 MAXIMUM OPERATING WEIGHT 850 LBS.</p>
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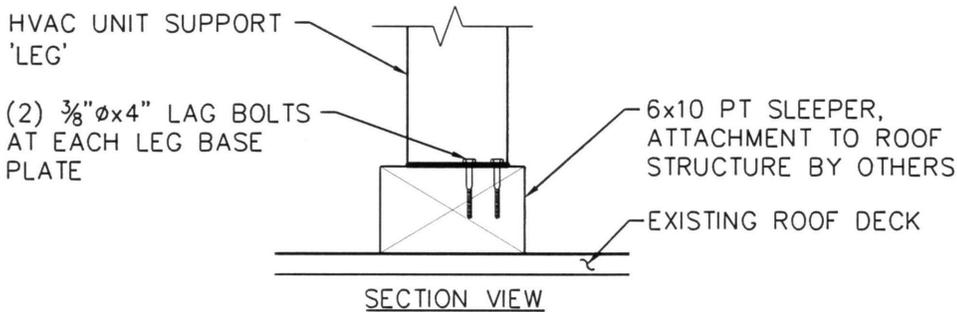
 <p>2345 NE 37th Ave, Portland, OR 97212 P 503.2816441 F 503.2816441 C 503.730.3357 E archereng@comcast.net</p>	<p>ALLIANT SYSTEMS 1600 NW 167TH PL BEAVERTON, OR 97006</p> <p>BY: MDA</p>	<p>DATE: 9/21/12 PROJECT: AE1242 DETAIL S2</p>
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PERSPECTIVE VIEW



PLAN VIEW



SECTION VIEW



1 HVAC CONNECTION DETAIL
S3 NTS

EXP. 12/31/13

HVAC-ROOF FAN

HVAC UNITS - SEISMIC CONNECTIONS
 KEEN SERVER ROOM
 1313 NW GLISAN ST., PORTLAND, OR

ROOF-TOP COOLING UNITS CU-1,2,3
 MAXIMUM OPERATING WEIGHT 500 LBS.



ALLIANT SYSTEMS
 1600 NW 167TH PL
 BEAVERTON, OR 97006

DATE: 9/20/12
 PROJECT: AE1238
 DETAIL
S3

BY: MDA

1



September 21, 2012

Mr. Kevin Grant
C2K Architecture Inc.
107 SE Washington St. Suite 740
Portland, Oregon 97214

RE: Pearl Building – KEEN
3rd Floor HVAC

Dear Kevin,

Attached please find calculations, sheets C1 through C2, dated September 20, 2012, which verify the structural adequacy of the existing wood framing system to support the new HVAC units being installed, as shown on drawing M2.3 dated August 14, 2012. Design is based on the requirements of the 2010 Oregon Structural Specialty Code, based on the 2009 International Building Code.

If you have any questions or need further information, please call me.

Sincerely,

Jose Machuca

JM:kw
212316/3rd Floor HVAC Calcs.docx



• MECH. UNIT

WT = 800#

AREA = 2' x 4' = 8#

LOAD = 800#/8# = 100 PSF

DL = 25 PSF

LL = 65 PSF

DF.L #2 : $f_b = 900$

DF.L #1 : $f_b = 1000$

$C_D = 1$

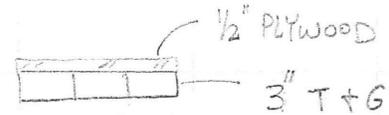
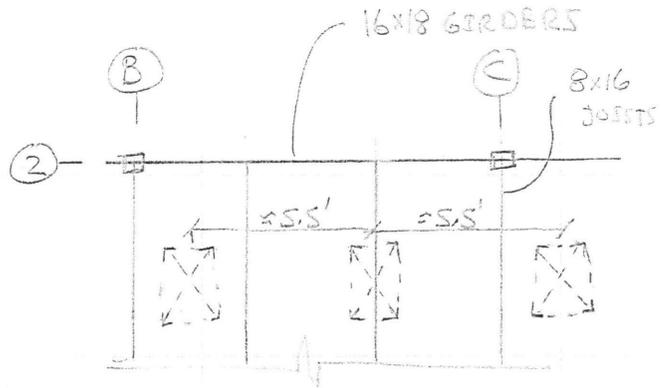
$C_{FI} = 1.5$

$C_{Fu} = 1$

$C_r = 1.15$

#2 $\Rightarrow F_b = 900(1)(1.5)(1)(1.15) = 1550 \text{ PSI}$

#1 $\Rightarrow F_b = 1725 \text{ PSI}$



FLOORING

FLOORING

FOR SIMPLICITY, CALCULATE AS LOAD OVER ENTIRE SPAN, T+G DECKING ONLY.

$W = 25 + 65 + 100 = 190 \text{ PSF}$

$M = \frac{(190)(4')^2}{8} = 4560 \text{ #-IN}$

$M/S = 4560/18 = 253 \text{ PSI} < 1550 \text{ PSI} \checkmark$

• 3" T+G

$S' = \frac{(12')(3')^2}{6} = 18 \text{ IN}^3/\text{FT}$

JOISTS

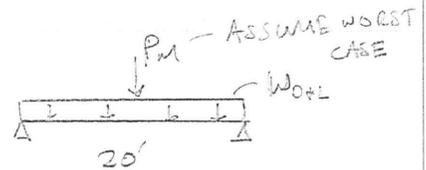
$W_{D+L} = (25+65)(4) = 360 \text{ PLF}$

$P_M = 800\#$

$M_{DL} = \frac{360(20')^2}{8} = 18,000 \text{ #-FT}$

$M_{PM} = \frac{800\#(20')}{4} = 4,000 \text{ #-FT}$

$M/S = (18,000 + 4,000)(12)/280 = 942 \text{ PSI} < 1550 \text{ PSI} \checkmark$



$S' = \frac{(7.25')(15.25')^2}{6} = 280 \text{ IN}^3$



Consulting Engineers

Portland, Oregon

Project KEEN

Location

Client

3RD FLOOR MECH. UNITS

By JWH

Date 9/20

Revised

Date

Sheet No.

C2

Job No.

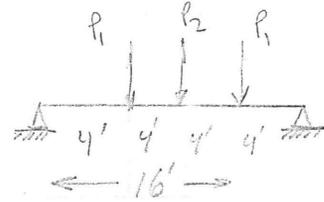
GIRDERS

$$P_1 = (25 + 65)(4')(20') + 800\# = 8,000\#$$

$$P_2 = (25 + 65)(4')(20') = 7,200\#$$

$$M = \frac{(7200\#)(16')}{4} + 2[(8000\#)(4')] = 1.11 \times 10^6 \# \cdot \text{IN} \quad S_{\text{GIRDER}} = \frac{(575)(17.25'')^2}{6} = \underline{\underline{781 \text{ IN}^3}}$$

$$M/S = 1.11 \times 10^6 \# \cdot \text{IN} / 781 \text{ IN}^3 = 1425 \text{ PSI} < 1550 \text{ PSI} \checkmark$$



COLUMNS

$$\text{LOAD: } (25 + 65)(16' \times 19') \times 2 + (25)(16' \times 19') = 62,320\#$$

$$\text{MECH: } 800\# \text{ ADDITIONAL, MAX}$$

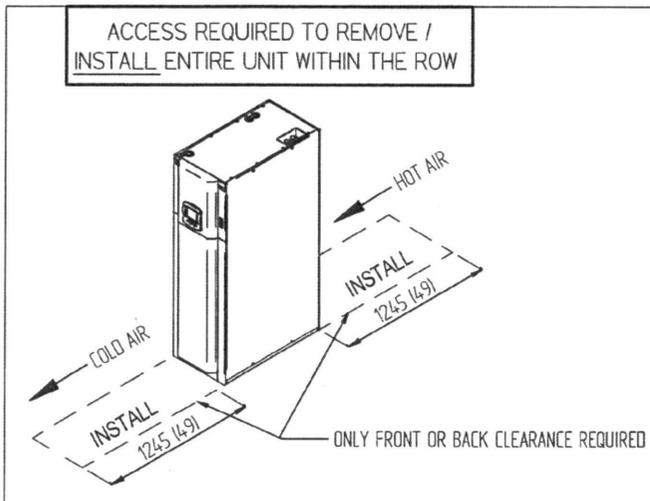
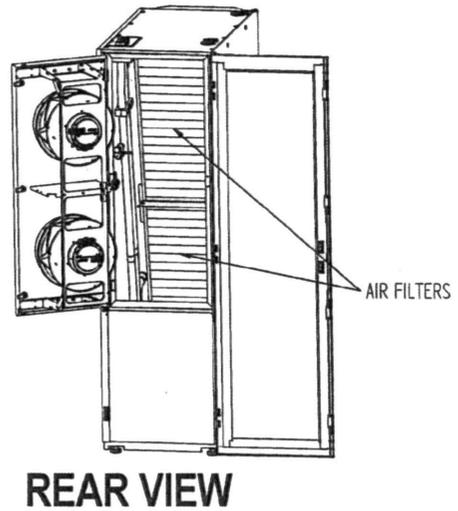
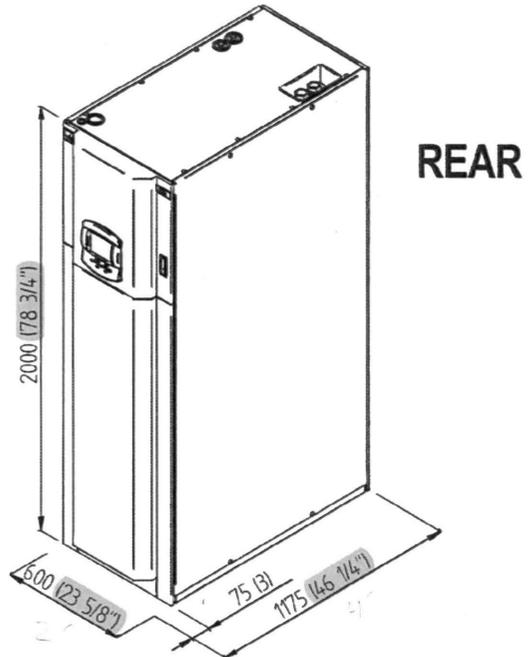
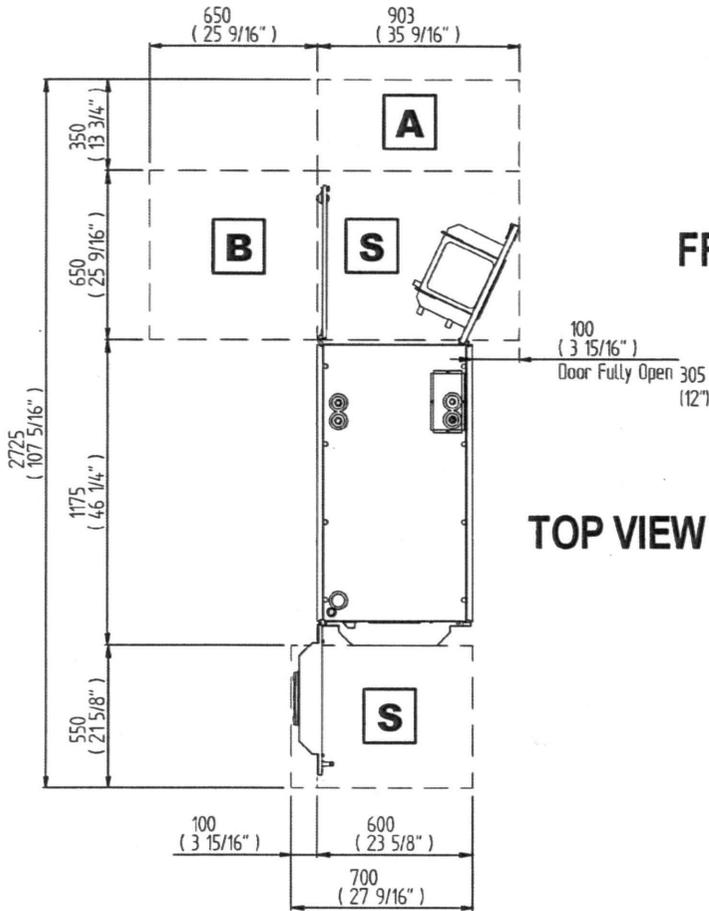
$$800\# / 62,320\# = .012$$

→ 1% ADDITIONAL
LOAD, NEGLECTABLE

CABINET AND FLOOR PLANNING DIMENSIONAL DATA

AIR COOLED (A) / WATER / GLYCOL COOLED (W) / CHILLED WATER (C)

ACCESS REQUIRED TO SERVICE WITHIN THE ROW
 REAR SERVICE AREA IS S+B OR S+A WHEN B IS NOT AVAILABLE



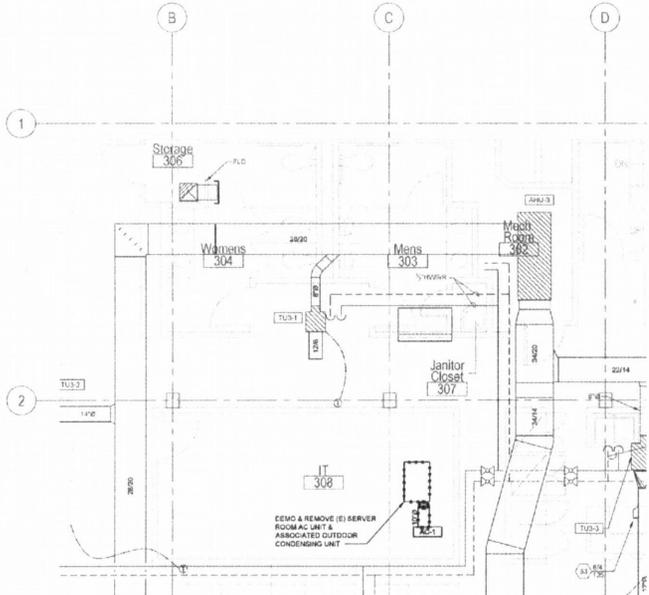
DRY WEIGHT ± 5% (lb / kg)		
Model No.	AIR COOLED	WATER/GLYCOL
CR020R	739 / 335	772 / 350
CR035R	805 / 365	849 / 385
CHILLED WATER		
CR040R	728 / 330	

Floor Plan

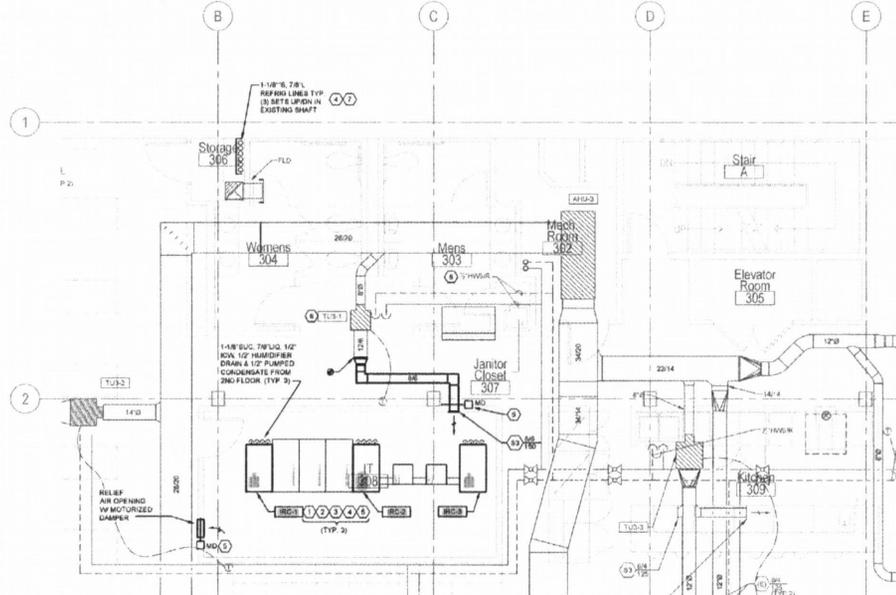
ECONOMIZER EXEMPTION
 NEW COOLING EQUIPMENT (2) PRIMARY UNITS W/ 110 MBH COOLING AND (1) RESIDUAL UNIT W/ 110 MBH COOLING ARE PROVIDED FOR EXPANDED CAPACITY AT EXISTING SERVER ROOM.
 AS MUCH THEY DO NOT REQUIRE ECONOMIZER PER DESIG EXEMPTION 503.4.1.8 WHICH ALLOWS INSTALLATION OF UP TO 600 MBH OF NEW NON-ECONOMIZER COOLING EQUIPMENT AT (E) SERVER ROOM.

HVAC GENERAL NOTES
 A NO ELECTRICAL GALVANIZED MATERIALS TO BE USED WITHIN THE IT SERVER ROOM TO PREVENT ZINC INFLUENCE CORROSION.
 B CONTRACTOR SHALL VISIT THE SITE AND BECOME THOROUGHLY FAMILIAR WITH SITE CONDITIONS AND NOTIFY ENGINEER OF ANY CONFLICT OR DIFFERENCE.

HVAC NOTES BY SYMBOL
 (NOT ALL NOTES USED ON EACH SHEET)
 ① ALL ELECTRICAL & PIPING CONNECTIONS ARE MADE THROUGH THE TOP OF THE UNIT. INSTALLATION MADE PER MANUFACTURER'S RECOMMENDATIONS.
 ② PROVIDE AN RPPB IN MECHANICAL ROOM FOR IN ROW COOLERS. HANG/DR SUPPLY P.P.P.E. RPPB TO BE SUPPLIED W/ DISCHARGE TO NEAREST SINK OR APPROVED DRAIN.
 ③ 1/2" PUMPED CONDENSATE TO DISCHARGE W/ AIR GAP AT MOP SINK ON SECOND FLOOR.
 ④ PER MANUFACTURER'S RECOMMENDATIONS, VERTICAL RISERS TO BE DOWNSIZED ONE TRADE SIZE (E: 1-1/8" TO 7/8" AND 7/8" TO 3/4").
 ⑤ RIG & MD CONTROLS TO INTERLOCK W/ FIRE SUPPRESSION SYSTEM CONTROLS TO STOP AIRFLOW UPON ALARM. COORDINATE REQUIREMENTS W/ FIRE SYSTEM CONTRACTOR.
 ⑥ NO REHEAT REQUIRED FOR EXISTING TERMINAL UNIT (E) (2). HYDROVIC VALVES TO BE PERMANENTLY CLOSED.
 ⑦ COORDINATE W/ GC TO REMOVE WALL AND PATCH/REPAIR TO ALLOW B/RAFT ACCESS.



1 MECHANICAL THIRD FLOOR HVAC DEMO PLAN
 1/8"=1'-0"
 0 2 4 8



2 MECHANICAL THIRD FLOOR HVAC PLAN
 1/8"=1'-0"
 0 2 4 8



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REVISIONS: DATE

KEEN SERVER ROOM

1313 NW GLISAN ST.
 PORTLAND, OR

DRAWING REVIEW

DEPT	INITIALS	DATE
CAD		
DESIGNER		
P.M.		
ENGINEER		
FIELD		

MECHANICAL THIRD FLOOR HVAC PLAN

DESIGNED: LSP MURRAY
 BY: E. STOYAN
 CHECKED: MURRAY
 DATE: 08/14/12

PROJECT NUMBER: C-0330-22074

PERMIT ISSUE
 08/14/12

M2.3

DATE PLOTTED: 08/14/12 10:58 AM